

**BRIDGETON LANDFILL, LLC.** 

PHASE 1 NORTH QUARRY EVOH COVER SYSTEM

CONSTRUCTION QUALITY ASSURANCE ACCEPTANCE REPORT

**BRIDGETON, ST. LOUIS COUNTY, MISSOURI** 

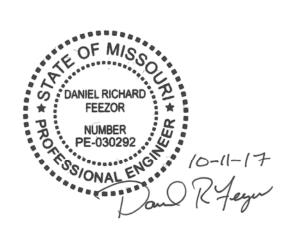
**Prepared For:** 

Bridgeton Landfill, LLC. 13570 St. Charles Rock Road Bridgeton, MO 63044

October 2017

**Prepared By:** 

Feezor Engineering, Inc. 3377 Hollenberg Drive Bridgeton, MO 63044



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Project No.: BT-125

# **CONTENTS**

| LIST ( | OF APPENDICES AND SUB-APPENDICES                 | . v |
|--------|--|-----|
| 1      | INTRODUCTION                                     | . 1 |
| 1.1    | Overview of Project                              | 1   |
| 1.2    | BACKGROUND                                       | 1   |
| 2      | SUBGRADE PREPARATION                             | .3  |
| 2.1    | SOIL FILL AND INFRASTRUCTURE MODIFICATIONS       | 2   |
| 2.1    | STRIP DRAINS                                     |     |
| 2.3    | GEOCOMPOSITE ROAD UNDERLAY                       |     |
| 2.4    | Non-Woven Cushion Fabric                         |     |
|        |  |     |
| 3      | FLEXIBLE MEMBRANE LINER INSTALLATION             | .5  |
| 3.1    | Pre - Installation Activities                    | 5   |
| 3.2    | FLEXIBLE MEMBRANE LINER PROPERTIES               | 5   |
| 3.2    | 2.1 Quality Control Testing                      | 5   |
| 3.3    | PRODUCT DELIVERY, STORAGE, AND HANDLING          |     |
| 3.4    | Installation Procedures                          | 5   |
| 3.4    |  |     |
| 3.4    | 4.2 Seaming Procedures                           |     |
|        | 3.4.2.1 Trial Welds                              |     |
|        | 3.4.2.2 Fusion Welding Procedures                |     |
|        | 3.4.2.3 Extrusion Welding Procedures             |     |
|        | 4.3 Defects and Repairs                          |     |
| 3.5    | CONSTRUCTION QUALITY ASSURANCE                   |     |
| 3.5    | 5.1 Oversight                                    | 7   |
| 3.5    | 5.2 Testing                                      |     |
|        | 3.5.2.1 Non-Destructive testing                  | 7   |
|        | 3.5.2.2 Destructive testing                      | 8   |
| 4      | ACCESS ROAD CONSTRUCTION                         | .9  |
| 4.1    | Access Road Construction Methods                 | 9   |
| 4.1    | 1.1 Geocomposite Cushion Layer                   |     |
| 4.1    | 1.2 Access Road Construction                     |     |
| 5      | LANDFILL GAS AND LIQUIDS RECOVERY INFRASTRUCTURE | 10  |
| 5.1    | LANDFILL GAS AND LIQUIDS RECOVERY INFRASTRUCTURE | 10  |
| 5.1    | 1.1 Landfill Gas Collection                      |     |
| _      | 1.2 Liquids Recovery and Conveyance              |     |
|        | Construction Quality Assurance                   |     |
|        | 2.1 Construction Oversight                       |     |
| _      | 2.2 Testing                                      |     |
| 6      | STORM WATER MANAGEMENT                           | 12  |
| 6.1    | STORM WATER DRAINAGE SYSTEMS                     | 12  |
| 7      | CERTIFICATION                                    | 13  |
| APPE   | NDICES AND SUB APPENDICES                        |     |

#### LIST OF APPENDICES AND SUB-APPENDICES

| A. Dail | y Field | l Summar | y Reports |
|---------|---------|----------|-----------|
|---------|---------|----------|-----------|

### B. Geosynthetic Conformance Testing

- **B.1** EVOH Geomembrane Manufacturer's Quality Control Data
- **B.2** Geotextile Manufacturer's Quality Control Data
- **B.3** Geocomposite Manufacturer's Quality Control Data

#### C. Geosynthetic Installation Data

- **C.1** Installer's Subgrade Acceptance Forms
- C.2 Panel Placement Forms
- **C.3** Field Tensiometer Calibration Certificate
- **C.4** Trial Weld Qualification Test Forms
- **C.5** Panel Seaming Forms
- **C.6** Non-Destructive Testing Results
- **C.7** Destructive Sampling
  - **C.7.1** Destructive Sample Log
  - **C.7.2** Destructive Sample Laboratory Testing Results
  - C.7.3 Memorandum Concerning Destructive Failure Tracking
- **C.8** Geomembrane Repair Log

#### D. Landfill Gas and Liquids Management Infrastructure

- **D.1** Pipe Information
- **D.2** Pressure Test Forms

#### E. Construction Photographs

#### F. Construction Certification Drawings (Reduced Set)

- **Drawing 001** Title Page
- **Drawing 002** Summary of Site Works
- **Drawing 003** Grading Plan View
- Drawing 004 EVOH Cover Undercap Plan View
- **Drawing 005** EVOH Cover Panel Layout Plan View
- **Drawing 006** EVOH Cover Overcap Plan View
- Drawing 007 Details 1
- Drawing 008 Details 2
- **Drawing 009** Details 3
- Drawing 010 Details 4
- Drawing 011 Details 5
- Drawing 012 Details 6
- Drawing 013 Details 7
- **Drawing 014** Details 8

#### 1 INTRODUCTION

#### 1.1 Overview of Project

During the late 2016 and 2017 construction season, Bridgeton Landfill, LLC (BLL) initiated and completed construction of Phase 1 North Quarry Ethylene Vinyl Alcohol (EVOH) Cover System. This report documents the construction of the EVOH Cover System Components, and provides the as-built record drawings, all sealed by a Missouri Registered Professional Engineer. Construction of the North Quarry EVOH Cover System was in general conformance with the October 2016 EVOH Cover System Work Plan developed by Cornerstone Environmental of Farmington Hills, MI.

Bridgeton Landfill, LLC retained Feezor Engineering, Inc. (FEI) of Bridgeton, MO to provide Construction Quality Assurance (CQA) services for the construction of the Phase 1 EVOH Cover System. Bridgeton Landfill, LLC also selected American Environmental Group, LTD (AEG) of Richfield, OH and Fusion Solutions, Inc. (FSI) of Carlinville, IL to construct / install the components of Phase 1 North Quarry EVOH Cover System including:

- General fill,
- Subsurface collection systems and cushioning geotextiles,
- EVOH liner installations,
- Cushion geocomposite road construction,
- Storm water drainage systems, and
- Landfill gas, leachate, and air supply piping.

### 1.2 Background

The North Quarry EVOH Work Plan was prepared in accordance with Section 35b of the Administrative Settlement Agreement and Order on Consent (AOC) between the U.S. Environmental Protection Agency (U.S. EPA) and Bridgeton Landfill, LLC, dated April 28, 2016. Section 35b of the AOC requires: Within 60 days of the Effective Date, Respondent shall submit to EPA and MDNR for review and approval a Work Plan for the placement of an EVOH Cover over the North Quarry. The Work Plan shall include the steps and associated timeframes necessary to install the EVOH Cover. Consistent with an EPA approved Work Plan, installation of the EVOH Cover shall proceed to be placed over the North Quarry, starting from the location of the existing EVOH Cover moving north such that the EVOH is continuous up to and covering a line of existing TMPs including TMP-16, 17, 18, 21, 22, 23, 25, 27, 28 and 29. The Work Plan shall also describe measures for operations and maintenance of the EVOH Cover.

The North Quarry EVOH Work Plan was approved by the U.S. EPA on October 19, 2016 and the final draft was submitted to the U.S. EPA on October 24, 2016. The U.S. EPA approved the final submitted North Quarry EVOH Work Plan on November 4, 2016.

1

The Phase 1 EVOH work completed the EVOH installation on a portion previously described as Phase 1A and Phase 1B (now considered one phase – i.e. Phase 1). The Phase 1A boundary was based on the AOC issued by U.S. EPA dated April 28, 2016. The Phase 1B EVOH cover boundary was based on the ridgeline of the North Quarry and captured the area on the south side of the ridgeline and outside of the area that could be affected by a potential thermal isolation barrier.

#### 2 SUBGRADE PREPARATION

#### 2.1 Soil Fill and Infrastructure Modifications

Before commencement of the installation of the geosynthetic portions of this project, subgrade amendments were made. Vertical landfill gas and liquid removal infrastructure heights were adjusted accordingly to accommodate proposed fill soils. This work was performed by FSI prior to the initiation of fill operations. Next vegetation was stripped from the proposed project area. Following the removal of vegetation, fill soil was placed in accordance with the proposed grades in the project work plan developed by Cornerstone. This fill was placed to allow for the proper shedding of storm water that came into contact with the project area to the storm water controls. Upon completion of the placement of fill soils, FSI removed any rocks or foreign debris that could potentially damage the geosynthetics. A representation of the final project contours can be found on **Drawing 003** in **Appendix F**.

## 2.2 Strip Drains

After preparation of the sub-base, a series of strip drains were installed in conformance to the locations specified in the project work plan. All strip drains were manufactured by American Wick (identified as model #6012). All drains were installed by AEG and joined using manufacturer's recommendations.

Strip drains that were installed uphill of the previously installed (by others) perimeter toe drain system terminated into the gravel backfill of the toe drain. This liquid will be managed through the perimeter toe drain sumps (PS sumps) already in place. Two separate sumps (CS-1 and CS-2) were installed at the toe of the slope to handle liquids that are collected by strip drains downhill of the perimeter toe drain. Four-inch risers were also installed at proposed locations if BLL decides in the future to utilize the strip drains as gas extraction locations. Locations of strip drains, strip drain risers and liquid extraction sumps CS-1 and CS-2 are depicted on **Drawing 004** in **Appendix F**.

# 2.3 Geocomposite Road Underlay

Prior to the installation of the non-woven geotextile cushion fabric, a surveyor laid out the proposed locations of the access roads that were proposed to be installed on top of the finished geosynthetic liner system in conformance with the Cornerstone work plan. AEG then installed a 220-mil double-sided geocomposite with 6-ounce per square yard non-woven geotextile backing in the locations of the proposed access roads. This material was joined together by affixing the inside geogrid using cable ties. After the geogrid of adjacent panels were joined, the geotextile on the edge of panels was continuously sewn together in accordance with the CQA Plan contained within the work plan. Following installation, a surveyor performed a record survey of the geocomposite to ensure that any slight

deviations were modified in the final roads on top of the geomembrane. Results of manufacturer's quality control testing for the double-sided geocomposite can be found in **Appendix B.3**.

#### 2.4 Non-Woven Cushion Fabric

A combination of 6-ounce per square yard and 8-ounce per square yard non-woven cushion geotextile material was acquired from SKAPS Industries. AEG deployed this material over the entirety of the project area to be covered with the EVOH geomembrane material. This material was deployed by a skid steer with a spreader bar. All adjacent panels of cushion geotextile were overlapped a minimum of six-inches. After the material was deployed and overlapped, it was seamed together by a heat tacking method with a Leister hot air tool. Results of manufacturer's quality control testing for the non-woven cushion geotextile can be found in **Appendix B.2**.

#### 3 FLEXIBLE MEMBRANE LINER INSTALLATION

#### 3.1 Pre - Installation Activities

Once the sub-base was prepared, strip drain system installed, cushion geotextile placed and the geocomposite road underlayment was installed, activities commenced to prepare for the installation of the 50-mil EVOH geomembrane. A subgrade acceptance form was jointly completed by FEI and AEG for the project area state the subgrade was suitable to the engineer and installer's representative for geomembrane placement. Subgrade Acceptance Forms may be found in **Appendix C.1**.

## 3.2 Flexible Membrane Liner Properties

The installed material consists of 50-mil Ethylene Vinyl Alcohol (EVOH) geomembrane. Raven Industries (Raven) provided manufacturer's certifications and test results for the 50-mil geomembrane which are included in **Appendix B.1**.

#### 3.2.1 Quality Control Testing

All rolls of EVOH geomembrane supplied for this project by Raven were CQA tested in the manufacturing facility. The rolls were evaluated for tensile characteristics that included stress at break and elongation at break. Additional testing performed included average thickness and asperity height along with tear and puncture resistance. Lastly, material was tested at a frequency of once per every 200,000 pounds for standard oxidative induction time. The reported values of each roll tested exceed the requirements of the CQA Plan. The test methods, minimum values and testing frequency conform with that established in the CQA Plan included within the project work plan.

# 3.3 Product Delivery, Storage, and Handling

Flexible membrane liner (FML) rolls were delivered on site by tractor-trailer. The rolls were stacked three high on a level dry surface west of the working area. Each roll's identification number, roll number, and dimensions were documented.

#### 3.4 Installation Procedures

#### 3.4.1 Deployment

AEG installed all FML panels. Rolls were supported by a spreader bar attached to skid steer and were deployed by AEG employees across the length of the closure area. Panels were placed in a manner that minimized seams. Unbound edges of the FML panels were temporarily loaded with sandbags prior to seaming.

As it was deployed, each panel was assigned a unique field identification number by FEI. The FML was continuously examined for damage and manufacturing defects beginning with placement on the subgrade through the completion of the project. Observed defects were marked by FEI and repaired by AEG. The panel placement diagram showing liner panels and repairs is included on the construction record drawings on **Drawing 005** in **Appendix F**.

#### 3.4.2 Seaming Procedures

#### 3.4.2.1 Trial Welds

Prior to field seaming, trial weld samples were prepared and tested in the field using a field tensiometer to qualify welders for seaming activities. The tensiometer calibration certificate is included in **Appendix C.3**. Trial weld samples were made from excess FML and were prepared using the same procedures and under the same conditions the welder expected during field welding. Three 1-inch samples were tested for peel and three 1-inch samples were tested for shear. FEI personnel observed the trial weld preparation and testing. The minimum strength criterion required for peel testing was 60 pounds per inch (ppi) for fusion and 52 ppi for extrusion welds. For shear testing, the minimum strength criterion was 80 ppi for both fusion and extrusion welds. The failure mode was required to be a film tear bond or a partial adhesion failure as described in section 6.1 and Table 1(a) of The Geosynthetics Research Institute specification GM-19 and the welds were to show no more than 25% delamination into the weld. A failure mode of Separation in Plane (SIP) is also deemed acceptable in accordance with literature from the Manufacturer and the CQA Plan contained within the work plan.

If all samples passed these criteria, the equipment and operator were allowed to proceed. If a sample failed, the reason for failure was investigated and a new sample was prepared and tested. This process was performed at the start of the day, after lunch, after extended delays without seaming and after any equipment shutdowns.

The various procedures associated with both fusion and extrusion seaming operations were observed by FEI. These observations included: seam preparation, weather conditions, general seaming procedures, overlap of geomembrane panels, and temporary bonding procedures. Seams were monitored throughout their length for quality and seam completion. Visually detected imperfections were marked by FEI and subsequently repaired by AEG. Panel placement and seaming records are presented in **Appendix C.2** and **Appendix C.5**, respectively. Results of trial weld testing are presented in **Appendix C.4**.

#### 3.4.2.2 Fusion Welding Procedures

Most production seams were made using a dual hot wedge fusion welder (commonly called a "mouse" or "wedge"). The unit heated the two overlapped panels above the geomembrane's melting point. The panels then passed through a set of preset pressure wheels that compress the two panels together to form a weld. This device created an air

channel between the fused seams that was pressurized with air and non-destructively tested throughout the welds entire length.

#### 3.4.2.3 Extrusion Welding Procedures

Repairs, patches and other necessary areas were performed with an extrusion welder. The unit introduced a bead of molten resin along the edge of the seam of the two FML sheets were welded. The top sheet was heat-tacked down to the bottom sheet and was ground with an abrasive disk immediately prior to the extrusion process. The continuity of the extrusion welds were non-destructively verified by vacuum testing at all locations except where the liner was welded to penetrations. At those locations, welds were inspected visually.

#### 3.4.3 Defects and Repairs

Flexible membrane liner panels were monitored for damage during deployment. Additionally, FEI personnel observed the FML panels and seams on an on-going basis throughout the installation process until the completion of the project.

Each repair was documented by FEI and repaired by AEG. Repairs were made by seaming a piece of geomembrane over the affected area with an extrusion-welding machine. All patches exceeded damaged areas by a minimum of 6 inches. Extrusion welded repairs were non-destructively tested using a vacuum box apparatus.

The vacuum box testing process consisted of placing a sealed box with a glass cover for viewing over a seam that had been bathed with a water / soap solution. The vacuum box was energized and created a vacuum of 5 psi for 10-15 seconds. If no air bubbles were observed coming from the seam, the test was considered to be a passing test. Documentation of FML repairs and testing is included in **Appendix C.8**.

#### 3.5 Construction Quality Assurance

#### 3.5.1 Oversight

All production and repair fusion and extrusion welds completed by AEG personnel were 100 percent non-destructively tested by either vacuum box or air channel testing in addition to regular destructive test samples along seams.

#### 3.5.2 Testing

#### 3.5.2.1 Non-Destructive testing

Non-destructive testing of geomembrane liner seams consisted of air channel pressure testing or vacuum testing. Extrusion welded repairs were vacuum tested and double wedge seams were air-pressure tested. Seams and repairs failing non-destructive testing were repaired and retested until passing results were obtained.

Air channel testing consisted of pressurizing the channels between the double wedge seams with air to a minimum pressure of 30 pounds per square inch (psi). The channels were kept pressurized for a minimum of 5 minutes. Passing tests were those with no more than a 3-psi drop over the 5-minute period. Results of non-destructive testing of FML seams are presented in **Appendix C.6**.

#### 3.5.2.2 Destructive testing

Destructive geomembrane seam samples were obtained at a minimum frequency of one per 500 linear feet of seam. Destructive seam testing was performed at TRI/Environmental Laboratory. The pass / fail criteria were as follows:

#### Peel Adhesion (ASTM D6392)

- Four out of the five-test specimens meet the strength requirements discussed in section 3.4.2.1.
- Failure mode is a film-tear bond or partial adhesion failure as described in section 6.1 and Table 1(a) of the GRI specification GM-19 and the welds were to show no more than 25% separation into the weld. A failure mode of Separation in Plane (SIP) is also deemed acceptable in accordance with literature from the Manufacturer and the CQA Plan contained within the work plan.

#### Shear Strength (ASTM D 6392)

- Four out of the five-test specimens meet the strength requirements discussed in section 3.4.2.1.
- Failure mode is a film-tear bond or partial adhesion failure as described in section 6.1 and Table 1(a) of the GRI specification GM-19 and the welds were to show no more than 25% separation into the weld.

Destructive samples were obtained and were labeled. A summary log of destructive samples is presented in **Appendix C.7.1**. Results of laboratory testing of destructive seam samples are included as **Appendix C.7.2**.

A memorandum concerning the bounding of failed destructive samples is presented in **Appendix C.7.3**.

#### 4 ACCESS ROAD CONSTRUCTION

#### 4.1 Access Road Construction Methods

#### 4.1.1 Geocomposite Cushion Layer

As described above in section 2.4, a 220-mil double sided geocomposite with 6-ounce per square yard non-woven geotextile back was installed below and above the EVOH geomembrane and the locations of proposed access roads. Prior to installation, a FEI surveyor laid out the locations of the previously installed road underlayment geocomposite that was installed below the EVOH geomembrane. Then material was installed with a 4-inch overlap along long seams and a 12-inch overlap on short seams. This material was joined together by affixing the inside geogrid using cable ties. After the geogrid of adjacent panels were jointed, the geotextile on the edge of panels was continuously sewn together. Results of manufacturer's quality control testing for the double-sided geocomposite can be found in **Appendix B.3**.

#### 4.1.2 Access Road Construction

Following installation of the geocomposite cushion layer, gravel access roads were installed in conformance to the approved work plan. AEG proceeded to install the aggregate for the access road. This consisted of placing an 18-inch layer of 2-inch to 4-inch of crushed limestone topped by a 6-inch layer of MODOT type V dense graded aggregate. Locations of installed access roads are depicted on **Drawing 006** of **Appendix F**.

#### 5 LANDFILL GAS AND LIQUIDS RECOVERY INFRASTRUCTURE

#### 5.1 Landfill Gas and Liquids Recovery Infrastructure

Following installation of the geosynthetic liner system, reconfiguration of the project area's landfill gas and liquids recovery infrastructure was performed by AEG.

#### 5.1.1 Landfill Gas Collection

Four header access risers were installed in the existing North Quarry perimeter landfill gas header to bring vacuum above ground. From these locations, landfill gas collection headers and laterals were installed above-ground to provide vacuum to the wells within the project area. This installation included:

- Approximately 410 feet of 4-inch diameter landfill gas collection piping,
- Approximately 1,870 feet of 6-inch diameter landfill gas collection piping,
- Approximately 230 feet of 8-inch diameter landfill gas collection piping,
- Approximately 1,870 feet of 12-inch diameter landfill gas collection piping, and
- Approximately 13 feet of 18-inch diameter landfill gas collection piping.

All gas collection piping was constructed of high density polyethylene (HDPE) pipe made from PE 3408 resin meeting ASTM D3350 requirements. All pipe materials were field inspected to verify conformance with design plans. HDPE pipe was joined by butt fusion methods according to standard procedures and manufacturer's recommendations. Gas collection piping was installed in the locations and to the required lines and grades as shown on **Drawing 006** of **Appendix F**.

#### **5.1.2** Liquids Recovery and Conveyance

In addition to the installation of landfill gas conveyance infrastructure, liquids (leachate and condensate) recovery piping infrastructure was also installed at the locations depicted on **Drawing 006** of **Appendix F**. A 3-inch by 6-inch dual-contained HDPE forcemain was constructed and installed to various liquid extraction points (wells, sumps, etc.) within the North Quarry. This infrastructure facilitates the removal of liquids and their conveyance to the onsite leachate pre-treatment system. In addition to the installation of the liquid forcemain, air supply piping was installed within the project footprint to provide compressed air to extraction pumps that are utilized throughout the project area. This installation included:

- Approximately 6,735 feet of 3-inch x 6-inch dual-contained forcemain, and
- Approximately 4,515 feet of 2-inch air supply piping.

All liquids recovery piping was constructed of HDPE pipe made from PE 3408 resin meeting ASTM D3350 requirements. All pipe materials were field inspected to verify conformance

with design plans. HDPE pipe was joined by butt fusion methods according to standard procedures and manufacturer's recommendations.

# **5.2 Construction Quality Assurance**

#### **5.2.1 Construction Oversight**

The CQA representative inspected all materials for the landfill gas collection and liquids recovery systems. This included piping, valves and fittings to ensure that these materials were acceptable and consistent with construction plans. The CQA representative inspected the materials to be constructed of HDPE pipe to determine if the materials met the following requirements:

- All HDPE pipe was new, or first quality, and was furnished at lengths as indicated on the approved design plans. All HDPE piping was straight throughout its length and free from imperfections.
- The HDPE pipe and fittings had a minimum Standard Dimension Ratio (SDR) as noted on the design plans.

During installation of the landfill gas collection and liquids recovery systems, the CQA representative ensured that the construction adhered to the plans and specifications. This included:

- Pipe and appurtenances were installed true to line, grade and location with the pipe supported and restrained against movement with all valve stems plumb.
- The pipe joints, except where flanged were butt fused as recommended by the pipe manufacturer. All shavings from the preparation of pipe ends for fusion were removed from the pipe prior to installation.

#### 5.2.2 Testing

Field-testing of the landfill gas collection and liquids recovery systems consisted of pressure testing system infrastructure in accordance with the Republic Services SOP. The pressure testing was performed by AEG and documented by FEI.

The pressure testing was performed after completion of a portion of the piping system. All pressure testing for landfill gas collection and liquid forcemain systems was conducted at a minimum of 10 psig as well as the containment piping for the liquid forcemain system. Carrier piping for the liquid forcemain system and air supply piping testing was conducted at a minimum of 100 psig. All pressure testing data is included in **Appendix D.2**.

#### **6 STORM WATER MANAGEMENT**

#### **6.1 Storm Water Drainage Systems**

Storm water management considerations were also included into the Phase 1 EVOH cover system construction. The portion of the project area with drainage to the west utilizes existing storm water management features in the South Quarry and ultimately drains to Outfall #003. A storm water terrace and culvert were constructed at the toe of the south slope of the project area. Drainage from this culvert flows to an existing culvert in the South Quarry which ultimately drains to Outfall #004.

The existing perimeter ditch at the toe of the east slope of the project area was re-graded and lined with EVOH geomembrane. This drainage area covers the vast majority of the project area and ultimately drains to the existing lined retention basin known as Outfall #006. Two culverts were installed to convey storm water from the ditch to the retention basin with gate valves installed to allow for control of the release of storm water if necessary.

A storm water letdown was installed at the northeast corner of the project area that receives runoff from two storm water terraces on the north slope of the North Quarry. Storm water from this letdown is ultimately discharged through Oufall #006.

# **7 CERTIFICATION**

I, Daniel R. Feezor, P.E., do hereby certify to my best knowledge and belief that the Phase 1 North Quarry EVOH Cover System was constructed in accordance with Cornerstone Environmental's approved EVOH Cover System Work Plan dated October 19, 2016 and the CQA Plan included within.

# APPENDIX A DAILY FIELD SUMMARY REPORTS

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



| Page:  | 1 | of | 1 |  |
|--------|---|----|---|--|
| . 466. | _ | ٠. | _ |  |

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |   |
|-------------------------------------|-------------|------------|---|
| Project: North Quarry Phase 1       | Task No.:   | -          |   |
| Location: Bridgeton, MO             | Date:       | 11/21/2016 |   |
| Contractor(s): Fusion Solution Inc. | Report No.: | 1          |   |
| Mosthory AM D.Cl. J. DM D.Cl. J.    |             |            | _ |

Weather: AM P. Cloudy PM P. Cloudy
Temperature: AM 26 PM 49

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0730 – I arrived on site.

0800 – Pre-Construction Meeting held with Nick Bauer (BLL EM), Mike Lambrich (BLL Site Manager), Matt Cunningham (Fusion PM), Arron Weber (FEI) and myself. We discussed project scope and schedule. After the initial discussion, we performed a walkthrough of the project area. Existing infrastructure needing to be relocated prior and during grading activaties were identified. BLL also requested FEI layout the project boundary and cut/fill stakes in preparation for grading activities to begin later this week or beginning of next depending on weather conditions.

1030 - Walkthrough Complete.

1045 – Arron Weber and I are performing initial project stake out.

1200 - Lunch

1230 – Layout work continues.

1400 – FEI completed initial stakeout.

FEI Representative:

# **Feezor Engineering, Inc.** 406 E. Walnut St.

Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bri                         | dgeton  | Landfill    | Job No.: | BT-125    |             |            |  |
|-------------------------------------|---------|-------------|----------|-----------|-------------|------------|--|
| Project: No                         | rth Qua | rry Phase 1 |          |           | Task No.:   | -          |  |
| Location: Bridgeton, MO             |         |             |          |           | Date:       | 11/29/2016 |  |
| Contractor(s): Fusion Solution Inc. |         |             |          |           | Report No.: | 2          |  |
| Weather:                            | AM      | P. Cloudy   | PM       | P. Cloudy |             |            |  |

**Temperature:** AM 44 PM 63

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0800 – Fusion arrives onsite and moves their trailer into the work area.

0900 – Fusion begins moving concrete blocks and other materials from the grading area.

1300 – Fusion leaves the site.

FEI Representative:

# Feezor Engineering, Inc. 406 E. Walnut St.

Chatham, IL 62629 (217) 483-3118



# **Daily Field Summary Report**

| Client: Bridgeton Landfill          | <b>Job No.:</b> BT-125 |  |
|-------------------------------------|------------------------|--|
| Project: North Quarry Phase 1       | Task No.:              |  |
| Location: Bridgeton, MO             | Date: 11/30/2016       |  |
| Contractor(s): Fusion Solution Inc. | Report No.: 3          |  |
| Weather: AM P. Cloudy PM P. (       | <br>Cloudy             |  |

46

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion arrives onsite and prepares to begin hauling in grading layer soil.

34

0745 - Fusion begins hauling and placement of grading layer soil in the Phase 1A cap area. Komatsu PC300 Excavator is loading a single Komatsu HM300 haul truck with soil material from stockpile north of the construction area. Material is being hauled and unloaded in the Phase 1A area. CAT D6N w/ GPS is grading placed material to subgrade elevations.

Existing landfill leachate forcemain and airline piping in the current work area are being removed this morning. Piping will be replaced after grading activities are completed for the day. All GCCS piping is remaining active during the project.

These processes are ongoing.

Temperature:

1200 - Lunch

1300 – Work Resumes with same process as morning

AM

1615 – Fusion begins reconnecting infrastructure removed this morning to allow for grading activities.

1700 – Fusion has reconnected all infrastructure items. Left site for day.

**FEI Representative:** 

Page: 1 of 1

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



| Page:  | 1 | of | 1 |  |
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#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          |         |             |    |           | Job No.:    | BT-125    |  |
|-------------------------------------|---------|-------------|----|-----------|-------------|-----------|--|
| Project: No                         | rth Qua | rry Phase 1 |    | _         | Task No.:   | -         |  |
| Location: Bridgeton, MO             |         |             |    |           | Date:       | 12/1/2016 |  |
| Contractor(s): Fusion Solution Inc. |         |             |    |           | Report No.: | 4         |  |
| Weather:                            | AM      | P. Cloudy   | PM | P. Cloudy |             |           |  |
| Temperature:                        | AM      | 31          | PM | 45        |             |           |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

0700 – Fusion continues hauling and placement of grading layer soil in the Phase 1A cap area. Komatsu PC300 Excavator is loading a single Komatsu HM300 haul truck with soil material from stockpile north of the construction area. Material is being hauled and unloaded in the Phase 1A area. CAT D6N w/ GPS is grading placed material to subgrade elevations.

Existing landfill leachate forcemain and airline piping in the current work area are being removed this morning. Piping will be replaced after grading activities are completed for the day. All GCCS piping is remaining active during the project.

These processes are ongoing.

1030 – KB electrician is on site to review the electrical and control connections to LCS-5A. Existing control building will be relocated just outside of the Phase 1A area until EVOH Cap is completed. Temporary power and control wire will be ran to allow LCS-5A to remain active throughout the construction project.

1200 - Lunch

1300 – Work Resumes with same process as morning

1615 – Fusion is reconnecting infrastructure removed this morning to allow for grading activities.

1700 – Fusion has reconnected all infrastructure items. Left site for day.

FEI Representative:

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#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          |         |             |    |           | Job No.:    | BT-125    |  |
|-------------------------------------|---------|-------------|----|-----------|-------------|-----------|--|
| Project: No                         | rth Qua | rry Phase 1 |    | _         | Task No.:   | -         |  |
| Location: Bridgeton, MO             |         |             |    |           | Date:       | 12/2/2016 |  |
| Contractor(s): Fusion Solution Inc. |         |             |    |           | Report No.: | 5         |  |
| Weather:                            | AM      | P. Cloudy   | PM | P. Cloudy |             |           |  |
| Temperature:                        | AM      | 27          | PM | 48        |             |           |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

0700 – Fusion continues hauling and placement of grading layer soil in the Phase 1A cap area. Komatsu PC300 Excavator is loading a single Komatsu HM300 haul truck with soil material from stockpile north of the construction area. Material is being hauled and unloaded in the Phase 1A area. CAT D6N w/ GPS is grading placed material to subgrade elevations.

Existing landfill leachate forcemain and airline piping in the current work area are being removed this morning. Piping will be replaced after grading activities are completed for the day. All GCCS piping is remaining active during the project.

These processes are ongoing.

0815 – KB electricians is onsite to remove the electrical and control connections to LCS-5A. Once power and control is disconnected, Fusion will relocate the existing control building just outside of the Phase 1A area.

0845 – Fusion has relocated the control building for LCS-5A. Temporary power and control wire is being ran inside separate PVC conduit.

1015 – KB Electric has reconnected the power and control to LCS-5A and it is back online.

1200 - Lunch

1300 – Work Resumes with same process as morning

1615 – Fusion is reconnecting infrastructure removed this morning to allow for grading activities.

1700 – Fusion has reconnected all infrastructure items. Left site for day.

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| Page: | 1 | of | 1 |
|-------|---|----|---|
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#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          |         |             |    |           | Job No.:    | BT-125    |  |
|-------------------------------------|---------|-------------|----|-----------|-------------|-----------|--|
| Project: No                         | rth Qua | rry Phase 1 |    | _         | Task No.:   | -         |  |
| Location: Bridgeton, MO             |         |             |    |           | Date:       | 12/3/2016 |  |
| Contractor(s): Fusion Solution Inc. |         |             |    |           | Report No.: | 6         |  |
| Weather:                            | AM      | P. Cloudy   | PM | P. Cloudy |             |           |  |
| Temperature:                        | AM      | 31          | PM | 44        |             |           |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

0700 - Fusion continues hauling and placement of grading layer soil in the Phase 1A cap area. Komatsu PC300 Excavator is loading a single Komatsu HM300 haul truck with soil material from stock

pile north of the construction area. Material is being hauled and unloaded in the Phase 1A area. CAT D6N w/ GPS is grading placed material to subgrade elevations.

Existing landfill leachate forcemain and airline piping in the current work area are being removed this morning. Piping will be replaced after grading activities are completed for the day. All GCCS piping is remaining active during the project.

These processes are ongoing.

1015 – FEI is performing survey layout of eastern ditch.

1200 - Lunch

1300 – Work Resumes with same process as morning

1515 – Fusion is reconnecting infrastructure removed this morning to allow for grading activities.

1600 – Fusion has reconnected all infrastructure items. Left site for day.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



| - 0 - | Page: | 1 | of | 1 |
|-------|-------|---|----|---|
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#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          |                               |           |             | Job No.:  | BT-125    |           |  |
|-------------------------------------|-------------------------------|-----------|-------------|-----------|-----------|-----------|--|
| Project: No                         | Project: North Quarry Phase 1 |           |             |           | Task No.: | -         |  |
| Location: Bri                       | dgeton,                       | MO        |             |           | Date:     | 12/6/2016 |  |
| Contractor(s): Fusion Solution Inc. |                               |           | Report No.: | 7         |           |           |  |
| Weather:                            | AM                            | P. Cloudy | PM          | P. Cloudy |           |           |  |
| Temperature:                        | AM                            | 32        | PM          | 43        |           |           |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

0700 – Fusion continues hauling and placement of grading layer soil in the Phase 1A cap area. Komatsu PC300 Excavator is loading a single Komatsu HM300 haul truck with soil material from stock pile north of the construction area. Material is being hauled and unloaded in the Phase 1A area. CAT D6N w/ GPS is grading placed material to subgrade elevations.

Existing landfill leachate forcemain and airline piping in the current work area are being removed this morning. Piping will be replaced after grading activities are completed for the day. All GCCS piping is remaining active during the project. Two workers from fusion begin adding extensions onto wells.

These processes are ongoing.

1200 - Lunch

1300 – Work Resumes with same process as morning. Paynecrest arrives onsite and examines a TMP to determine the best method for raising it above the proposed grade.

1400 – Fusion finished raising their second well and begins capping the underground air and force main lines at the PEWs.

1515 – Fusion begins reconnecting infrastructure removed this morning to allow for grading activities.

1600 – Fusion has reconnected all infrastructure items. Left site for day.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



| Page: | 1 | of | 1 |
|-------|---|----|---|
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#### **Daily Field Summary Report**

| <b>Client:</b> Bri | dgeton   | Landfill     |    |           | Job No.:    | BT-125    |  |
|--------------------|----------|--------------|----|-----------|-------------|-----------|--|
| Project: No        | rth Qua  | rry Phase 1A |    |           | Task No.:   | -         |  |
| Location: Bri      | dgeton,  | MO           |    |           | Date:       | 12/7/2016 |  |
| Contractor(s): Fus | sion Sol | ution Inc.   |    |           | Report No.: | 8         |  |
| Weather:           | AM       | P. Cloudy    | PM | P. Cloudy |             |           |  |

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

Temperature:

AM

0700 – Fusion continues hauling and placement of rock for the drainage trench.

32

1100 – Fusion continues hauling and placement of grading layer soil in the Phase 1A cap area. Komat su PC300 Excavator is loading a single Komatsu HM300 haul truck with soil material from stockpile north of the construction area. Material is being hauled and unloaded in the Phase 1A area. CAT D6N w/ GPS is grading placed material to subgrade elevations.

Existing landfill leachate forcemain and airline piping in the current work area are being removed this morning. Piping will be replaced after grading activities are completed for the day. All GCCS piping is remaining active during the project. Two workers from fusion begin adding extensions onto wells.

These processes are ongoing.

1200 - Lunch

1400 – I begin south ditch stakeout. Fusion has raised 3 wells and begins to cap more of the underground air and forcemain lines.

1600 - Fusion begins reconnecting infrastructure removed this morning to allow for grading activities 1700 – Left site for day.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1\_\_\_ of \_\_1\_\_

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 03/20/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 9          |
| Weather: AM P. Cloudy PM            | Sunny       |            |

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

Temperature:

0700 – Fusion is onsite with 6 workers, equipment onsite is a Cat 315D Excavator, a Komatsu HM300 Haul Truck, a Cat 330C Excavator, a Cat D6n GPS Dozer, a TakeuchiTL240 Skid steer, and various fusion welding equipment. They begin to strip the vegetation off of the Phase 1B area, and to cut and cap abandoned infrastructure below grade.

1200 - Lunch

1300 – Fusion resumes previous activities

AM

50

1700 – Left site for day.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 03/21/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 10         |
| Moothory AM D.Cl. J. DM D.C.        |             |            |

Weather: AM P. Cloudy PM P. Sunny
Temperature: AM 45 PM 66

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

0700 – Fusion is onsite with 6 workers, equipment onsite is a Cat 315D Excavator, a Komatsu HM300 Haul Truck, a Cat 330C Excavator, a Cat D6N GPS Dozer, a Takeuchi TL240 Skid steer, and various fusion welding equipment. They continue to strip and grade Phase 1B, using soil from the North Quarry stockpile, they also begin to remove the rock pads used for the TMP installations.

1200 - Lunch

1300 – Fusion resumes previous activities

1700 – Left site for day.

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| Page: | 1 | of | 1 |
|-------|---|----|---|
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#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 03/22/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 11         |
| Weather: AM P. Cloudy PM P. Sunny   |             |            |

52

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

Temperature:

0700 – Fusion is onsite with 6 workers, equipment onsite is a Cat 315D Excavator, a Komatsu HM300 Haul Truck, a Cat 330C Excavator, a Cat D6N GPS Dozer, a Takeuchi TL240 Skid steer, and various fusion welding equipment. They continue to grade Phase 1B, using soil from the North Quarry stock pile, they also continue to cut and cap abandoned infrastructure below the subgrade.

1200 - Lunch

1300 – Fusion resumes previous activities

AM

36

1430 – The North Quarry stockpile is depleted and Fusion begins to haul soil from the Borrow Area to continue grading.

1700 – Left site for day.

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| Page: | 1 | of | 1 |
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#### **Daily Field Summary Report**

| <b>Client:</b> Bri | dgeton   | Landfill    |    |         | Job No.:    | BT-125     |  |
|--------------------|----------|-------------|----|---------|-------------|------------|--|
| Project: No        | rth Qua  | rry Phase 1 |    | _       | Task No.:   | -          |  |
| Location: Bri      | dgeton,  | , MO        |    |         | Date:       | 03/23/2017 |  |
| Contractor(s): Fus | sion Sol | ution Inc.  |    |         | Report No.: | 12         |  |
| Weather:           | AM       | P. Cloudy   | PM | Showers |             |            |  |

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

Temperature:

AM

39

0700 – Fusion is onsite with 6 workers, equipment onsite is a Cat 315D Excavator, a Komatsu HM300 Haul Truck, a Cat 330C Excavator, a Cat D6N GPS Dozer, a Takeuchi TL240 Skid steer, and various fusion welding equipment. They continue to grade Phase 1B, using soil from the North Quarry stock pile, they also continue to cut and cap abandoned infrastructure below the subgrade. 1200 - Fusion Leaves the site due to rain.

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406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



| Page: | 1 | of | 1 |
|-------|---|----|---|
|       |   |    |   |

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill    |          |            | Job No.: | BT-125 |             |            |  |
|-------------------------------|----------|------------|----------|--------|-------------|------------|--|
| Project: North Quarry Phase 1 |          |            |          |        | Task No.:   | -          |  |
| Location: Bri                 | dgeton,  | , MO       |          |        | Date:       | 03/24/2017 |  |
| Contractor(s): Fus            | sion Sol | ution Inc. |          |        | Report No.: | 13         |  |
| Weather:                      | AM       | P. Cloudy  | PM       | Sunny  |             |            |  |

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – I arrived on site.

Temperature:

0700 – Fusion is onsite with 6 workers, equipment onsite is a Cat 315D Excavator, a Komatsu HM300 Haul Truck, a Cat 330C Excavator, a Cat D6N GPS Dozer, a Takeuchi TL240 Skid steer, and various fusion welding equipment. They continue to grade Phase 1B, using soil from the North Quarry stock pile, they also continue to cut and cap abandoned infrastructure below the subgrade.

1200 - Lunch

1300 – Fusion resumes previous activities

AM

1700 – Fusion leaves the site for day.

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| Page: 1 | of | 1 |
|---------|----|---|
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# **Daily Field Summary Report**

| <b>Client:</b> Bri | dgeton L  | andfill     |      |      | Job No.:    | BT-125     |  |
|--------------------|-----------|-------------|------|------|-------------|------------|--|
| Project: No        | rth Quar  | ry Phase 1B |      |      | Task No.:   | -          |  |
| Location: Bri      | dgeton, I | MO          |      |      | Date:       | 03/27/2017 |  |
| Contractor(s): Fus | sion Solu | tion Inc.   |      |      | Report No.: | 14         |  |
| Weather:           | AM        | Rain        | PM   | Rain |             |            |  |
| Temperature        | Λ N Λ     | Γĵ          | DIVI | го   | -           |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

No work from 3/27/17 thru 4/9/17 due to continuing rain.

FEI Representative:

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 04/10/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 15         |

Weather:AMShowersPMShowersTemperature:AM58PM81

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite with 2 workers, they begin to relocate pipe onto the PS trench so the surrounding area can be graded.

1200 - Lunch

1300 – Fusion begins to strip Phase 1B.

1600 – Fusion Left the site.

ArrenWeln

Copies To:Dan Feezor, Erin Fanning FEI Representative:

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 04/11/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 16         |
|                                     |             |            |

Weather: AM Cloudy PM Cloudy
Temperature: AM 48 PM 62

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite with 2 workers, they continue to strip Phase 1B

1100 – Fusion begins to add rock to the PS trench to bring it up to grade.

1200 – They begin to remove soil below the PS trench to bring it to grade and blend it in around the PS trench.

1500 – Fusion leaves the site for the day.

ArrenWeln

Temperature:

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1\_\_\_ of \_\_1\_\_

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | <b>Job No.:</b> BT-125 | )  |
|-------------------------------------|------------------------|----|
| Project: North Quarry Phase 1       | Task No.:              |    |
| Location: Bridgeton, MO             | Date: 04/12/20         | 17 |
| Contractor(s): Fusion Solution Inc. | Report No.: 17         |    |
| Weather: AM P Sunny PM P S          | unny                   |    |

73

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

PM

0700 – Fusion is onsite with 2 workers, they begin removal of the 3 culverts feeding into the retention pond from the Phase 1B ditch.

1200 - Lunch

1600 – Fusion leaves the site for the day, all 3 culverts were removed.

45

AM

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| Page:  | 1 | of | 1 |
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#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 04/13/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 18         |

Weather:AMP SunnyPMSunnyTemperature:AM54PM84

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite, they begin to cut out the east ditch for phase 1B.

1200 - Lunch

1400 – Fusion leaves the site for the day.

FEI Representative:

Copies To:Dan Feezor, Erin Fanning

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 04/14/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 19         |

Weather:AMP SunnyPMP SunnyTemperature:AM65PM85

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite, they continue to cut out the east ditch for phase 1B.

1200 - Lunch

1400 – Fusion leaves the site for the day.

# **Feezor Engineering, Inc.** 406 E. Walnut St.

Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:     | BT-125     |  |
|-------------------------------------|--------------|------------|--|
| Project: North Quarry Phase         | Task No.:    | -          |  |
| Location: Bridgeton, MO             | Date:        | 04/17/2017 |  |
| Contractor(s): Fusion Solution Inc. | Report No.:  | 20         |  |
| Weather: AM P Sunn                  | y PM P Sunny |            |  |

71

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

PM

0700 – Fusion is onsite with 3 workers, they continue excavation of the south ditch for phase 1B.

1200 - Lunch

1300 – Fusion begins to haul in dirt for the Phase 1B down chute from the borrow area.

1600 – Fusion leaves the site for the day.

AM

Temperature:

Representative: Aran VIII

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| Page: | 1 | of | 1 |
|-------|---|----|---|
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#### **Daily Field Summary Report**

| Client: Bridgeton Landfill    |          |            |    | Job No.:  | BT-125      |            |
|-------------------------------|----------|------------|----|-----------|-------------|------------|
| Project: North Quarry Phase 1 |          |            |    | Task No.: | -           |            |
| Location: Bridgeton, MO       |          |            |    |           | Date:       | 04/18/2017 |
| Contractor(s): Fus            | sion Sol | ution Inc. |    |           | Report No.: | 21         |
| Weather:                      | AM       | P Sunny    | PM | P Sunny   |             |            |
| Temperature:                  | AM       | 52         | PM | 79        |             |            |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite with 2 workers, they continue to bring in dirt for the down chute and construct it according to design.

1200 - Lunch

1600 – Fusion leaves the site for the day.

FEI Representative: Arran Waln

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Job No.:    | BT-125     |
|-------------|------------|
| Task No.:   | -          |
| Date:       | 04/19/2017 |
| Report No.: | 22         |
|             | Task No.:  |

Weather:AMP SunnyPMSunnyTemperature:AM65PM88

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite with 2 workers, they continue construction of the down chute.

0900 – Fusion begins construction of the berm below the down chute

1200 - Lunch

1300 – Fusion begins to fill in additional areas within the project footprint.

1600 – Fusion leaves the site for the day.

ArrenWeln

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |
|-------------------------------------|-------------|------------|
| Project: North Quarry Phase 1       | Task No.:   | -          |
| Location: Bridgeton, MO             | Date:       | 04/20/2017 |
| Contractor(s): Fusion Solution Inc. | Report No.: | 23         |
| Weather: AM P. Sunny PM Sunny       | <del></del> |            |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

PM

0700 – Fusion is onsite, they continue adding fill and grading within the project area with a CAT D6N w/ GPS.

1200 - Lunch

1600 – Fusion leaves the site for the day.

AM

58

Temperature:

El Representative: **Arranulu** 

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| Page: 1 | of | 1 |
|---------|----|---|
|---------|----|---|

# **Daily Field Summary Report**

| Client: Bridgeton Landfill    |           |            |    |      | Job No.:    | BT-125     |  |
|-------------------------------|-----------|------------|----|------|-------------|------------|--|
| Project: North Quarry Phase 1 |           |            |    |      | Task No.:   | -          |  |
| Location: Bridgeton, MO       |           |            |    |      | Date:       | 04/21/2017 |  |
| Contractor(s): Fus            | sion Solu | ition Inc. |    |      | Report No.: | 24         |  |
| Weather:                      | AM        | Rain       | PM | Rain |             |            |  |
| Temperature:                  | AM        | 52         | PM | 58   | -           |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

No work from today due to rain.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



| Page: | 1 | of | 1 |
|-------|---|----|---|
|       |   |    |   |

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill |          |             |    | Job No.: | BT-125      |    |  |
|----------------------------|----------|-------------|----|----------|-------------|----|--|
| Project: No                | rth Qua  | rry Phase 1 |    | _        | Task No.:   | -  |  |
| Location: Bridgeton, MO    |          |             |    | Date:    | 04/24/2017  |    |  |
| Contractor(s): Fus         | sion Sol | ution Inc.  |    |          | Report No.: | 25 |  |
| Weather:                   | AM       | P Sunny     | PM | P Sunny  |             |    |  |
| Temperature:               | AM       | 44          | PM | 77       |             |    |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite. They begin to clean up Phase 1A from the rain and begin to construct a catchall around the culvert at the southeast corner of phase 1A that was added to the design.

1200 - Lunch

1300 – Fusion begins remove the rock road through the fill area and haul in dirt

1700 – Fusion leaves the site for the day.

ArrenWeln

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill |           |             |    | Job No.: | BT-125      |    |  |
|----------------------------|-----------|-------------|----|----------|-------------|----|--|
| Project: No                | rth Quai  | rry Phase 1 |    |          | Task No.:   | -  |  |
| Location: Bridgeton, MO    |           |             |    | Date:    | 04/25/2017  |    |  |
| Contractor(s): Fus         | sion Solu | ition Inc.  |    |          | Report No.: | 26 |  |
| Weather:                   | AM        | Sunny       | PM | Sunny    |             |    |  |
| Temperature:               | AM        | 58          | PM | 82       |             |    |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite with 2 workers. They continue removing rock from the primary access road and replacing with fill soils and grade.

1200 - Lunch

1700 – Fusion leaves the site for the day.

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| Page: | 1 | of | 1 |  |
|-------|---|----|---|--|
|       |   | •  | _ |  |

#### **Daily Field Summary Report**

| <b>Client:</b> Bri | dgeton L  | andfill    |    |      | Job No.:    | BT-125     |  |
|--------------------|-----------|------------|----|------|-------------|------------|--|
| Project: No        | rth Quar  | ry Phase 1 |    |      | Task No.:   | -          |  |
| Location: Bri      | dgeton, I | MO         |    |      | Date:       | 04/26/2017 |  |
| Contractor(s): Fus | sion Solu | tion Inc.  |    |      | Report No.: | 27         |  |
| Weather:           | AM        | Rain       | PM | Rain |             |            |  |
| Temperature:       | AM        | 50         | PM | 72   | _           |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – Fusion is onsite. The continue the removal of rock from the primary access road over the top of the north quarry. They continue replacing the rock will fill soil and grading. They are also checking and re-establishing any necessary erosion control devices for the forecasted rain. 1200 – Lunch

1600 – Fusion leaves the site for the day.

ArrenWeln

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| Page: 1 | of | 1 |
|---------|----|---|
|---------|----|---|

#### **Daily Field Summary Report**

| <b>Client:</b> Bri | dgeton L  | andfill    |    |      | Job No.:     | BT-125     |  |
|--------------------|-----------|------------|----|------|--------------|------------|--|
| Project: No        | rth Quar  | ry Phase 1 |    |      | Task No.:    | -          |  |
| Location: Bri      | dgeton, N | MO         |    |      | Date:        | 04/27/2017 |  |
| Contractor(s): Fus | sion Solu | tion Inc.  |    |      | Report No.:  | 28         |  |
| Weather:           | AM        | Rain       | PM | Rain |              |            |  |
| Temperature:       | AM        | 52         | PM | 58   | <del>-</del> |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

No work from 4/27/17 thru 4/30/17 due to continuing rain.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          | Job No.:    | BT-125     |  |
|-------------------------------------|-------------|------------|--|
| Project: North Quarry Phase 1B      | Task No.:   | -          |  |
| Location: Bridgeton, MO             | Date:       | 05/01/2017 |  |
| Contractor(s): Fusion Solution Inc. | Report No.: | 29         |  |

Weather:AMRainPMRainTemperature:AM49PM58

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. They go through the site safety class.

0900 – AEG begins to setup their trailer and get their equipment ready.

1200 – AEG begins to weld together pipe strings.

1700 – AEG demobilizes and plans on returning the 15<sup>th</sup> after the upcoming forecasted rain.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill               | Job No.:    | BT-125     |
|--|-------------|------------|
| Project: North Quarry Phase 1B           | Task No.:   | -          |
| Location: Bridgeton, MO                  | Date:       | 05/15/2017 |
| Contractor(s): Fusion Solution Inc.; AEG | Report No.: | 30         |
|  |             |            |

Weather:AMSunnyPMSunnyTemperature:AM62PM90

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. They go through the site safety class. Fusion is onsite, the begin to groom the project area ahead of FML installation.

0900 – AEG begins to setup their trailer and get their equipment ready. They also fill sand bags.

1200 - Lunch

1300 - AEG begins to weld together pipe strings.

1700 - AEG and Fusion leave site.

tative: AranUela

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill    | Job No.:    | BT-125     |
|-------------------------------|-------------|------------|
| Project: North Quarry Phase 1 | Task No.:   | -          |
| Location: Bridgeton, MO       | Date:       | 05/16/2017 |
| Contractor(s): AEG            | Report No.: | 31         |
| Weather: AM Sunny PM Su       | unny        |            |

90

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

PM

0700 – AEG is onsite. They begin to clean dirt off the PS trench and stage materials in the work area.

1200 - Lunch

1400 – AEG begins to install strip drains at proposed locations and deploy cushion geotextile in the project area. They also install geocomposite at the locations where proposed roads are to be installed.

1800 – AEG leaves the site.

Temperature:

AM

71

ArronWelm

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill    | Job No.:    | BT-125     |
|-------------------------------|-------------|------------|
| Project: North Quarry Phase 1 | Task No.:   | -          |
| Location: Bridgeton, MO       | Date:       | 05/17/2017 |
| Contractor(s): AEG            | Report No.: | 32         |

Weather:AMCloudyPMShowersTemperature:AM74PM84

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. They begin to deploy liner over the west slope.

1200 - Lunch

1300 – AEG fills sandbags and brings more liner to the work area.

1700 – AEG leaves the site.

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Page: 1 of 1

BT-125

05/18/2017

33

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill |  |
|----------------------------|--|
|----------------------------|--|

Project: North Quarry Phase 1

Location: Bridgeton, MO

Contractor(s): AEG

Weather:

Temperature:

AM Sunny ΑM 72

PM PM

Sunny 91

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

Job No.:

Task No.:

**Report No.:** 

Date:

0700 – AEG is onsite. They continue to deploy liner over the west slope.

1200 - Lunch

1900 – AEG leaves the site.

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| Page: 1 of 1 |  |
|--------------|--|
|--------------|--|

#### **Daily Field Summary Report**

| Client: Bri        | dgeton L  | andfill       |    |      | Job No.:    | BT-125     |  |
|--------------------|-----------|---------------|----|------|-------------|------------|--|
| Project: No        | rth Quar  | ry Phase 1    |    |      | Task No.:   | -          |  |
| Location: Bri      | dgeton, I | MO            |    |      | Date:       | 05/19/2017 |  |
| Contractor(s): Fus | sion Solu | tion Inc.; AE | G  |      | Report No.: | 34         |  |
| Weather:           | AM        | Rain          | PM | Rain |             |            |  |

85

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

No work due to rain.

Temperature:

AM

58

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Page: 1 of 1

#### **Daily Field Summary Report**

| <b>Client:</b> Bri | dgeton L | .andfill    |    |       | Job No.:    | BT-125     |  |
|--------------------|----------|-------------|----|-------|-------------|------------|--|
| Project: No        | rth Quar | ry Phase 1B |    |       | Task No.:   | -          |  |
| Location: Bri      | dgeton,  | MO          |    |       | Date:       | 05/22/2017 |  |
| Contractor(s): AE  | G        |             |    |       | Report No.: | 35         |  |
| Weather:           | AM       | Sunny       | PM | Sunny |             |            |  |
| Temperature:       | AM       | 54          | PM | 79    |             |            |  |

79

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. They begin to install strip drains, cushion geotextile and road underlayment geocomposite on the next section of the cap. They also begin to deploy geocomposite on top of the previously installed EVOH liner so the main haul road can be put back in place.

1200 - Lunch

1400 – AEG resumes deployment of EVOH geomembrane.

54

1900 – AEG leaves the site.

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| Page: 1 of | 1 |
|------------|---|
|------------|---|

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill     |    |        |       |            | Job No.:    | BT-125     |  |
|--------------------------------|----|--------|-------|------------|-------------|------------|--|
| Project: North Quarry Phase 1B |    |        |       |            | Task No.:   | -          |  |
| Location: Bridgeton, MO        |    |        |       |            | Date:       | 05/23/2017 |  |
| Contractor(s): AE              | G  |        |       |            | Report No.: | 36         |  |
| Weather:                       | AM | Cloudy | PM Sh | nowRainers |             |            |  |
| Temperature:                   | ΔM | 50     | PM    | 72         |             |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. The continue to install strip drains, deploy cushion geotextile and install road road underlayment geocomposite where necessary. Afterwards, they resume the installation of EVOH geomembrane over the west slope. The pipe crew continues fabricating pipe sections. 1030 – AEG shuts due due to rain.

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| Page: | 1 | of | 1 |
|-------|---|----|---|
|       |   |    |   |

#### **Daily Field Summary Report**

| <b>Client:</b> Bri                                      | Client: Bridgeton Landfill |        |    |        |             | BT-125          |  |
|---|----------------------------|--------|----|--------|-------------|-----------------|--|
| Project: North Quarry Phase 1B  Location: Bridgeton, MO |                            |        |    |        | Task No.:   | -<br>05/24/2017 |  |
|   |                            |        |    |        | Date:       |                 |  |
| Contractor(s): AE                                       | G                          |        |    |        | Report No.: | 37              |  |
| Weather:  | AM                         | Cloudy | PM | Cloudy |             |                 |  |
| Temperature:  | AM                         | 53     | PM | 71     |             |                 |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. The continue installing geocomposite above previously installed liner where the proposed access road is to be installed. Then they begin to deploy liner while their pipe crew begins placing gravel for the construction of the main access road in accordance with the project design.

1200 - Lunch

1900 – AEG leaves the site.

FEI Representative: HranWell

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill    |       |        |     |        | Job No.:    | BT-125     |  |
|-------------------------------|-------|--------|-----|--------|-------------|------------|--|
| Project: North Quarry Phase 1 |       |        |     |        | Task No.:   | -          |  |
| Location: Bridgeton, MO       |       |        |     |        | Date:       | 05/25/2017 |  |
| Contractor(s): AE             | G     |        |     |        | Report No.: | 38         |  |
| Weather:                      | AM    | Cloudy | PM  | Cloudy |             |            |  |
| Townsustings                  | A N A |        | D14 | 70     |             |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. The pipe crew continues construction of the main access road including the installation of the proposed deflector pipes. The liner crew continues with the installation of EVOH geomembrane.

1200 - Lunch

1900 – AEG leaves the site.

ArrenWelm

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill  Project: North Quarry Phase 1  Location: Bridgeton, MO |       |       |    |       | Job No.:    | BT-125     |  |
|--|-------|-------|----|-------|-------------|------------|--|
|  |       |       |    |       | Task No.:   | -          |  |
|  |       |       |    |       | Date:       | 05/26/2017 |  |
| Contractor(s): AE  | G     |       |    |       | Report No.: | 39         |  |
| Weather:   | AM    | Sunny | PM | Sunny |             |            |  |
| Tomorosturos   | A B 4 | 60    | DM | 07    |             |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. The pipe crew continues cleanup of the PS trench, while the liner crew deploys more geocomposite above previously installed EVOH geomembrane then resume the installation of EVOH geomembrane.

1200 - Lunch

1900 – AEG leaves the site.

ArrenWelm

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| Page: | 1 | of | 1 |
|-------|---|----|---|
|       |   |    |   |

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill          |    |        |    |         | Job No.:    | BT-125     |  |
|-------------------------------------|----|--------|----|---------|-------------|------------|--|
| Project: North Quarry Phase 1B      |    |        |    |         | Task No.:   | -          |  |
| Location: Bridgeton, MO             |    |        |    |         | Date:       | 05/27/2017 |  |
| Contractor(s): Fusion Solution Inc. |    |        |    |         | Report No.: | 40         |  |
| Weather:                            | AM | Cloudy | PM | Showers |             |            |  |
| Temperature:                        | AM | 66     | PM | 84      |             |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. The pipe crew continues the construction of the main access road per design while the liner crew works on the west tie in.

1300 - AEG leaves the site due to rain.

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| <b>Client:</b> Bri                                    | Client: Bridgeton Landfill |       |    |       |             | BT-125     |  |
|---|----------------------------|-------|----|-------|-------------|------------|--|
| Project: North Quarry Phase 1 Location: Bridgeton, MO |                            |       |    |       | Task No.:   | -          |  |
|   |                            |       |    |       | Date:       | 05/30/2017 |  |
| Contractor(s): AE                                     | G                          |       |    |       | Report No.: | 41         |  |
| Weather:  | AM                         | Sunny | PM | Sunny |             |            |  |
| Temperature:  | AM                         | 60    | PM | 83    |             |            |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 - AEG is onsite. The pipe crew begins to excavate to install Header Access Riser 3, the liner crew continues work on the west tie in.

1200 - Lunch

1700 – AEG leaves the site.

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Page: 1\_\_\_ of \_\_1\_\_

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill  Project: North Quarry Phase 1  Location: Bridgeton, MO |    |       |    |       | Job No.:    | BT-125     |  |
|--|----|-------|----|-------|-------------|------------|--|
|  |    |       |    |       | Task No.:   | -          |  |
|  |    |       |    |       | Date:       | 05/31/2017 |  |
| Contractor(s): AE  | G  |       |    |       | Report No.: | 42         |  |
| Weather:   | AM | Sunny | PM | Sunny |             |            |  |

84

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 – AEG is onsite. The pipe crew continues building the main access road. The liner crew continues to install EVOH geomembrane.

1200 - Lunch

1800 – AEG leaves the site

Temperature:

AM

61

Temperature:

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| Page: | 1 | of | 1 |
|-------|---|----|---|
|       |   |    |   |

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill  Project: Phase 1 North Quarry EVOH Liner  Location: Bridgeton, MO |     |       |    |       | Job No.:    | BT-125   |
|---|-----|-------|----|-------|-------------|----------|
|   |     |       |    |       | Task No.:   | -        |
|   |     |       |    |       | Date:       | 6/1/2017 |
| Contractor(s): AEG  | j . |       |    |       | Report No.: | 43       |
| Weather:  | AM  | Sunny | PM | Sunny |             |          |

85

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – Meet Dan at Hollenburg Rd office. Mobilize to the landfill for job detail.

70

0800 – Complete Bridgeton Landfill safety orientation

AM

0830 – AEG crew is deploying EVOH geomembrane on the slope of the North Quarry to the existing PS trench. Data collection of panel placement, welding, destructs, and non-destructive testing is ongoing. Bridgeton Landfill personnel cut power to the area to allow AEG to work around components in the area.

1200 - Lunch

1230 – Work resumes in the same manner as the morning.

2000 – AEG stops for the day. Approximately 22,576 square feet of liner deployed.

359.755%

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client: Bridgeton Landfill  Project: Phase 1 North Quarry EVOH Liner  Location: Bridgeton, MO |    |       |    |       | Job No.:    | BT-125   |  |
|---|----|-------|----|-------|-------------|----------|--|
|   |    |       |    |       | Task No.:   | -        |  |
|   |    |       |    |       | Date:       | 6/2/2017 |  |
| Contractor(s): AEC  | ĵ  |       |    |       | Report No.: | 44       |  |
| Weather:  | AM | Sunny | PM | Sunny |             |          |  |

90

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – Arrive on site.

Temperature:

0700 – AEG crew is continuing liner work on the slope of the North Quarry to the existing PS trench. Extrusion welding to the PS trench is ongoing as well as repairs, air testing, and destructive sampling. 1200 - Lunch

1230 – Work resumes in the same manner as the morning.

AM

75

1400 - AEG begins to deploy strip drain, cushion geotextile and road underlayment geocomposite on the eastern side of the north quarry in preparation of EVOH liner deployment on 6/3/2017. 1800 – AEG stops for the day.

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| Page: | 1 | of | 1 |
|-------|---|----|---|
|       |   |    |   |

#### **Daily Field Summary Report**

| Client:Bridgeton Landfill                |           |       |    | Job No.: | BT-125      |          |
|--|-----------|-------|----|----------|-------------|----------|
| Project: Phase 1 North Quarry EVOH Liner |           |       |    |          | Task No.:   | -        |
| Location: Brid                           | dgeton, N | MO    |    |          | Date:       | 6/3/2017 |
| Contractor(s): AEC                       | j .       |       |    |          | Report No.: | 45       |
| Weather:                                 | AM        | Sunny | PM | Sunny    |             |          |
| Temperature:                             | AM        | 80    | PM | 92       |             |          |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0655 – Arrive on site.

0700 – AEG crew begins to deploy EVOH liner on the south side of the north quarry from the existing PS trench to the future anchor trench. AEG simultaneously commences seeming, and non-destructive testing. Data collection for all activities is ongoing. Marking destructive samples as they become necessary. 1200 – Lunch

1230 – Work resumes in the same manner as the morning.

1800 – AEG stops for the day. Approximately 29,218 square feet of EVOH liner deployed.

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Page: 1 of 1

#### **Daily Field Summary Report**

| <b>Client:</b> Brid                      | dgeton L | andfill |    |       | Job No.:    | BT-125   |  |
|--|----------|---------|----|-------|-------------|----------|--|
| Project: Phase 1 North Quarry EVOH Liner |          |         |    |       | Task No.:   | -        |  |
| Location: Bridgeton, MO                  |          |         |    |       | Date:       | 6/5/2017 |  |
| Contractor(s): AEG                       | j .      |         |    |       | Report No.: | 46       |  |
| Weather:                                 | AM       | Sunnv   | PM | Sunnv |             |          |  |

90

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

Temperature:

0700 – AEG foreman and personnel assess the condition of the work site after overnight rain in the area. AEG foreman determines that the condition of the work area is unsuitable for liner work.

0800 – AEG demobs to allow Site to dry.

0800 - Continue to collect data from previous liner deployment including seaming, non-destruct air tests, repairs, destructive testing.

1500 – Complete collecting liner data at the Site. Demobilize.

AM

70

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125   |
|--|-------------|----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -        |
| Location: Bridgeton, MO                  | Date:       | 6/6/2017 |
| Contractor(s):AEG                        | Report No.: | 47       |

Weather:AMSunnyPMSunnyTemperature:AM66PM82

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0655 – Arrive on site.

0700 – AEG works to deploy strip drains, cushion geotextile and road underlayment geocomposite along the cap of the north quarry.

1200 – AEG takes lunch.

1230 – AEG works to deploy EVOH liner on the cap of the north quarry. Deployment work includes seaming, non-destructive air tests, repairs, destructive sampling.

1800 – Work stops for the day. Approximately 20,102 square feet of liner placed.

350.0556

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Page: 1 of 1

#### **Daily Field Summary Report**

| <b>Client:</b> Brid                      | dgeton L  | andfill |       |             | Job No.:    | BT-125   |  |
|--|-----------|---------|-------|-------------|-------------|----------|--|
| Project: Phase 1 North Quarry EVOH Liner |           |         |       | Task No.:   | -           |          |  |
| Location:Brid                            | dgeton, I | MO      |       |             | Date:       | 6/7/2017 |  |
| Contractor(s): AEC                       | <u> </u>  |         |       |             | Report No.: | 48       |  |
| Weather:                                 | AM        | Sunny   | PM Pa | rtly Cloudy |             |          |  |
| Temperature:                             | AM        | 64      | PM    | 80          |             |          |  |

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG works to install strip drains, cushion geotextile and road underlayment geocomposite along the cap of the north quarry.

1200 - AEG takes lunch.

1230 – AEG works to deploy EVOH liner on the cap of the north quarry. Deployment work includes seaming, non-destructive air tests, repairs, destructive sampling.

1800 – Work stops for the day. Approximately 21,072 square feet of liner placed.

350.0556

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Page: 1 of 1

#### **Daily Field Summary Report**

| <b>Client:</b> Brid | dgeton I | Landfill       |          |           | Job No.:    | BT-125   |  |
|---------------------|----------|----------------|----------|-----------|-------------|----------|--|
| Project: Ph         | ase 1 N  | orth Quarry EV | /OH Line | r         | Task No.:   | -        |  |
| Location:Brid       | dgeton,  | МО             |          |           | Date:       | 6/8/2017 |  |
| Contractor(s): AEC  | ĵ        |                |          |           | Report No.: | 49       |  |
| Weather:            | AM       | P. Cloudy      | PM       | M. Cloudy |             |          |  |

83

PM Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0645 – Arrive on site.

Temperature:

ΑM

0700 – AEG works to install strip drains, cushion geotextile and road underlayment geocomposite along the cap of the north quarry.

1200 – AEG takes lunch.

1230 – AEG works to deploy EVOH liner on the cap of the north quarry. Deployment work includes seaming, non-destructive air tests, repairs, destructive sampling.

1800 – Work stops for the day. Approximately 25,672 square feet of liner placed.

61

406 E. Walnut St. Chatham, IL 62629 (217) 483-3118



Page: 1 of 1

#### **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125   |
|--|-------------|----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -        |
| Location: Bridgeton, MO                  | Date:       | 6/9/2017 |
| Contractor(s):AEG                        | Report No.: | 50       |
|  |             |          |

Weather:AMClearPMClearTemperature:AM68PM88

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0653 – Arrive on site.

0700 – AEG works to install strip drains, cushion geotextile and road underlayment geocomposite along the cap of the north quarry.

1220 – AEG takes lunch.

1250 – AEG works to deploy EVOH liner on the cap of the north quarry. Deployment work includes seaming, non-destructive air tests, repairs, destructive testing.

1830 – Work stops for the day. Approximately 39,592 square feet of liner placed.

ve: 359.7552

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Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill

Project: Phase 1 North Quarry EVOH Liner

Location: Bridgeton, MO

Contractor(s): AEG

Task No.:

Date: 6/10/2017

Report No.: 51

Weather:AMClearPMClearTemperature:AM71PM90

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0653 – Arrive on site.

0700 – AEG works to install strip drains, cushion geotextile and road underlayment geocomposite as well as EVOH liner along the cap of the north quarry.

1100 – High winds force AEG to stop deploying liner. The AEG crew works to complete detail work such as repairs and tie-ins across the entire North Quarry cap area.

1200 - AEG takes lunch.

1230 – AEG continues detail work in the same manner as before.

1700 – Work stops for the day. Approximately 12,448 square feet of liner placed.

350.055%

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125    |
|--|-------------|-----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -         |
| Location: Bridgeton, MO                  | Date:       | 6/12/2017 |
| tractor(s):AEG                           | Report No.: | 52        |

Weather:AMClearPMClearTemperature:AM72PM95

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0653 – Arrive on site.

0700 – AEG works to deploy cushion geotextile and EVOH liner along the cap of the north quarry.

0945 – AEG stops deploying liner to allow for PS trench grading. AEG crew works to complete detail work such as repairs and tie-ins across the entire North Quarry cap area.

1200 – AEG takes lunch.

1230 – AEG continues detail/tie-in work in the same manner as before.

1500 – AEG begins to prep a new area of the North Quarry cap for geotextile placement.

1800 – Work stops for the day.

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Page: 1 of 1

#### **Daily Field Summary Report**

Client:Bridgeton Landfill
Project: Phase 1 North Quarry EVOH Liner
Location:Bridgeton, MO
Date: 6/13/2017
Contractor(s):AEG
Report No.: 53

Weather:AMClearPMClearTemperature:AM80PM90

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0653 – Arrive on site.

0700 – AEG works to deploy EVOH liner along the cap of the north quarry to the anchor trench.

1200 - AEG takes lunch.

1230 – AEG continues work in the same manner as before.

1500 – AEG stops the deployment of EVOH and works to install strip drains, cushion geotextile and road underlayment geocomposite on all areas of the North Quarry cap that have exposed subgrade. Additional crew members are working on fusion/extrusion welding the panels placed in the morning and making repairs/air testing.

1800 – Work stops for the day.

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| Page: | 1 | of | 1 |
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|       |   |    |   |

#### **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125    |
|--|-------------|-----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -         |
| Location: Bridgeton, MO                  | Date:       | 6/14/2017 |
| Contractor(s):AEG                        | Report No.: | 54        |
|  |             |           |

Weather:AMP. CloudyPMRainTemperature:AM80PM90

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 - Arrive on site.

0700 – AEG works to deploy EVOH liner along the cap of the north quarry to the anchor trench. Additional crew members are working on fusion/extrusion welding the panels and making repairs/air testing.

1130 – AEG preps the work site for rain as storms are entering the area.

1205 – AEG takes lunch.

1315 – Significant rain accumulation has forced AEG to stop work for the day in an effort to allow the storm water to evacuate and evaporate from the work area.

1330 – Demobilize to Hollenberg Rd. office.

350.055%

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Page: 1 of 1

BT-125

#### **Daily Field Summary Report**

Client:Bridgeton Landfill

Project: Phase 1 North Quarry EVOH Liner

Location:Bridgeton, MO

Task No.: Date: 6/16/2017

Report No.: 55

Job No.:

Contractor(s):AEG

Weather:AMP. CloudyPMCloudyTemperature:AM74PM92

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG works on patches to the EVOH liner due to the subgrade being too muddy to deploy liner on. Additional crew members are working on fusion/extrusion welding the panels and making repairs/air testing.

1205 – AEG takes lunch.

1315 –AEG returns and continues repairs.

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1700 – AEG leaves the site for the day.

FEI Representative: Hreshill

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125    |
|--|-------------|-----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -         |
| Location: Bridgeton, MO                  | Date:       | 6/19/2017 |
| Contractor(s):AEG                        | Report No.: | 56        |

Weather:AMP. CloudyPMCloudyTemperature:AM67PM88

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG works fusion/extrusion welding the panels and making repairs/air testing of previously installed geomembrane.

1205 – AEG takes lunch.

1315 –AEG returns and continues performing detail work on EVOH geomembrane.

1700 – AEG leaves the site for the day.

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Page: 1 of 1

BT-125

6/20/2017

57

Date:

**Report No.:** 

#### **Daily Field Summary Report**

Client:Bridgeton Landfill Job No.: Project: Phase 1 North Quarry EVOH Liner Task No.: Location:Bridgeton, MO

Contractor(s):AEG Weather: ΑM PM P. Cloudy Sunny

AM PM Temperature: 92 66

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG is working on detail work for previously installed EVOH geomembrane due to the subgrade being too wet to deploy.

1205 – AEG takes lunch.

1315 –AEG returns and continues repairs.

1700 – AEG leaves the site for the day.

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Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill

Project: Phase 1 North Quarry EVOH Liner

Location: Bridgeton, MO

Task No.: Date: 6/21/2017

Report No.: 58

BT-125

Job No.:

Contractor(s):AEG

Weather:AMSunnyPMCloudyTemperature:AM76PM97

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 - Arrive on site.

0700 – AEG resumes installation of EVOH geomembrane. All strip drain, cushion geotextile and road underlay ment geocomposite has already been installed.

1205 – AEG takes lunch.

1315 –AEG returns and continues laying out liner.

1700 – AEG leaves the site for the day.

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Page: 1 of 1

BT-125

#### **Daily Field Summary Report**

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| _ |     | _  |        |         |         |  |

Project: Phase 1 North Quarry EVOH Liner Location: Bridgeton, MO

Contractor(s):AEG

Weather:

AM

ΑM Sunny 76

PM Sunny PM 87

Temperature:

Task No.: 6/22/2017 Date: **Report No.:** 59

Job No.:

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG continues installation of EVOH geomembrane.

1205 – AEG takes lunch.

1315 –AEG returns and continues installing geomembrane.

1900 – All geomembrane is deployed. AEG leaves the site for the day.

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Page: 1 of 1

# **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125    |
|--|-------------|-----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -         |
| Location: Bridgeton, MO                  | Date:       | 6/23/2017 |
| Contractor(s):AEG                        | Report No.: | 60        |

Weather: AM P. Sunny PM Cloudy
Temperature: AM 70 PM 88

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG works on extrusion welding repairs on previously installed EVOH geomembrane.

1205 – AEG takes lunch.

1315 –AEG returns and continues performing detail work on previously installed geomembrane.

1800 – AEG leaves the site for the day.

ArrenWelm

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Page: 1 of 1

BT-125

6/24/2017

61

Job No.:

Task No.:

**Report No.:** 

Date:

#### **Daily Field Summary Report**

**Client:**Bridgeton Landfill

Project: Phase 1 North Quarry EVOH Liner

Location: Bridgeton, MO

Contractor(s):AEG

Weather: Temperature:

ΑM P. Sunny ΑM 64

PM PM

Cloudy 81

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG works on repairs on previously installed EVOH geomembrane.

1205 – AEG takes lunch.

1315 –AEG returns and continues previous activities.

1700 – AEG leaves the site for the day.

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Page: 1 of 1

BT-125

6/26/2017

62

Job No.:

Task No.:

**Report No.:** 

Date:

#### **Daily Field Summary Report**

Client:Bridgeton Landfill Project: Phase 1 North Quarry EVOH Liner

Location:Bridgeton, MO

Contractor(s):AEG

Weather: Temperature:

AM

ΑM P. Sunny 58

PM Cloudy PM

81

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG continues working on repairs on previously installed geomembrane. AEG pipe crew begins the excavation of the anchor trench along the project boundary.

1205 – AEG takes lunch.

1315 –AEG returns and continues previous activities.

1700 – AEG leaves the site for the day.

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Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill
Project: Phase 1 North Quarry EVOH Liner
Location: Bridgeton, MO

Contractor(s): AEG

BT-125

Task No.:

6/27/2017

Report No.:
63

Weather: AM P. Sunny PM Cloudy
Temperature: AM 58 PM 83

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 - Arrive on site.

0700 – AEG continues working on repairs to previously installed geomembrane. AEG pipe crew continues the excavation of the anchor trench. After a portion of trench is excavated, EVOH geomembrane is placed in the trench and then it is backfilled.

1205 – AEG takes lunch.

1315 –AEG returns and continues previous activities.

1700 – AEG leaves the site for the day.

FEI Representative:

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Page: 1 of 1

#### **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125    |
|--|-------------|-----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -         |
| Location: Bridgeton, MO                  | Date:       | 6/28/2017 |
| Contractor(s):AEG                        | Report No.: | 64        |
| Moathor: AM D.C DM C                     |             |           |

Weather:AMP. SunnyPMSunnyTemperature:AM69PM90

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG continue making repairs to previously installed EVOH geomembrane along with installing the strip drain risers. They also continue excavation of the anchor trench along the east boundary and sealing pipe boots.

1205 – AEG takes lunch.

1315 –AEG returns and continues previous activities.

1700 – AEG leaves the site for the day.

FEI Representative:

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| Page:  | 1 | of | 1 |  |
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# **Daily Field Summary Report**

| Client:Bridgeton Landfill                | Job No.:    | BT-125    |
|--|-------------|-----------|
| Project: Phase 1 North Quarry EVOH Liner | Task No.:   | -         |
| Location: Bridgeton, MO                  | Date:       | 6/29/2017 |
| Contractor(s):AEG                        | Report No.: | 65        |

Weather:AMP. SunnyPMSunnyTemperature:AM74PM93

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 - Arrive on site.

0700 – AEG continues making repairs to previously installed EVOH geomembrane along with installing the strip drain risers. They also excavate the last of the anchor trench along the east boundary and seal pipe boots.

1205 – AEG takes lunch.

1315 –AEG returns and continues previous activities.

1800 – AEG leaves the site for the day.

ArronWelm

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Page: 1 of 1

BT-125

6/30/2017

66

Job No.:

Task No.:

**Report No.:** 

Date:

#### **Daily Field Summary Report**

**Client:**Bridgeton Landfill

Project: Phase 1 North Quarry EVOH Liner

Location: Bridgeton, MO

Contractor(s):AEG

Weather: Temperature:

ΑM P. Sunny ΑM 70

PM PM

Sunny 87

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG works on making repairs and sealing pipe boots.

1205 – AEG takes lunch.

1315 –AEG returns and continues previous activities.

1800 – AEG leaves the site for the day.

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Page: 1 of 1

BT-125

7/01/2017

67

Job No.:

Task No.:

**Report No.:** 

Date:

#### **Daily Field Summary Report**

**Client:**Bridgeton Landfill

Project: Phase 1 North Quarry EVOH Liner

Location:Bridgeton, MO

Contractor(s):AEG

Weather: Temperature:

ΑM

 $\mathsf{AM}$ P. Sunny 71

PM Sunny PM 90

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0650 – Arrive on site.

0700 – AEG finishes repairs and pipe boots.

1100 - AEG liner crew demobilizes.

FEI Representative:



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/10/2017

Contractor(s): AEG Report No.: 68

Weather: AM Sunny PM Sunny, windy

Temperature: AM 82 °F PM 97 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0900 – One AEG crew fusing 3x6 perimeter forcemain sections and cleanouts in NE corner of Phase 1B, another crew fusing sections/fittings of 12-in gas pipe near LCS-5B.

1524 – AEG crews continue fusion work on perimeter forcemain and begin road building/extension work in Phase 1A.

1659 – AEG crews continue road building/extension activities using excavator, small dump truck, and bulldozer.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location**: Bridgeton, MO **Date**: 7/11/2017

Contractor(s): AEG Report No.: 69

Weather: AM Sunny PM Sunny
Temperature: AM 83 °F PM 99 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0711 – AEG crews resume fusing 3x6 perimeter forcemain sections and cleanouts along east side of Phase 1B. McElroy 618 fusion machine being prepped to ship to Ohio for repair of hydraulic system.

0839 – Additional rock for road building/extension work being delivered.

1430 – AEG crew continues road building/extension activities using excavator, small dump truck, and bulldozer. Bulldozer has to pull dump truck up the hill occasionally due to steepness of slope.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/12/2017

Contractor(s): AEG Report No.: 70

Weather: AM Sunny PM Sunny
Temperature: AM 82 °F PM 99 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0708 – AEG setting up to fuse flanges onto 30-in and 36-in sections of HDPE culvert using large trailer-mounted fusion machine.

1422 – AEG crew continues road building/extension activities using excavator and bulldozer. Small dump truck replaced with Terramac crawler given previous issue (bulldozer had to pull dump truck up the hill due to steepness of slope).



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/13/2017

Contractor(s): AEG Report No.: 71

Weather: AM Sunny PM Cloudy, light rain

Temperature: AM 84 °F PM 88 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0708 – Discuss day's agenda with AEG. AEG to continue road building/extension activities in order to get Terramac crawler off-rent. Also plan to fabricate HDPE fittings since new McElroy 618 arrived.

1004 – AEG crew working in South Quarry.

1531 – Pop-up thunderstorm threatening. Everyone off the hill.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/14/2017

Contractor(s): AEG Report No.: 72

Weather: AM Cloudy PM Partly cloudy, humid

**Temperature: AM** 76 °F **PM** 90 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0734 – AEG to continue road building/extension activities using Terramac, excavator, and bulldozer.

1140 – AEG lunch.

1420 – AEG road building/extension efforts continue.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/17/2017

Contractor(s): AEG Report No.: 73

Weather: AM Mostly sunny PM Mostly sunny

**Temperature: AM** 76 °F **PM** 90 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1307 – AEG performing road building/extension activities at base of road above PEW-50 using small excavator. Fusing sections of perimeter forcemain together, installing valve box on forcemain.

1528 — Survey of perimeter forcemain indicates continuous run in place from PEW-46 in southeast corner of North Quarry to point above CT-8B and below GEW-9 in amphitheater. Cleanouts still need to be capped with blind flanges and wellhead/lateral connections need to be made. Pressure testing likely to start mid- to late-week next week.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/18/2017

Contractor(s): AEG Report No.: 74

Weather: AM Sunny PM Sunny
Temperature: AM 80 °F PM 98 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0727 – AEG performing road building/extension activities at base of road north of PEW-50 using small excavator. Butt fusing fittings onto forcemain connections at wellheads along northeast ditch.

1413 – AEG continues fusion work.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/19/2017

Contractor(s): AEG Report No.: 75

Weather: AM Sunny PM Partly cloudy

Temperature: AM 81 °F PM 96 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1303 – AEG installing valve boxes on connections near PEW-48, -49, and -50, continuing other fittings fusion work.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/20/2017

Contractor(s): AEG Report No.: 76

Weather: AM Sunny PM Partly cloudy

Temperature: AM 86 °F PM 92 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0820 – AEG crew working in South Quarry along south perimeter road. No activities taking place in North Quarry. Additional rock being delivered for road work.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/21/2017

Contractor(s): AEG Report No.: 77

Weather: AM Sunny PM Sunny
Temperature: AM 94 °F PM 98 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1015 – AEG working on road extensions in southeastern portion of North Quarry.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/24/2017

Contractor(s): AEG Report No.: 78

Weather: AM Sunny PM Sunny
Temperature: AM 79 °F PM 90 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0830 – AEG working on dual-contained Y fittings and 12-in HDPE sections.

1410 – AEG working on road extensions.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/25/2017

Contractor(s): AEG Report No.: 79

Weather: AM Partly cloudy PM Sunny Temperature: AM 78 °F PM 91 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0820 – AEG excavating across perimeter road to install 36-in culvert. To maintain grade they'll need to construct a hump in the road over the pipe instead of deepening the trench across the road.

1548 – AEG continuing culvert work.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/26/2017

Contractor(s): AEG Report No.: 80

Weather: AM Cloudy PM Mostly cloudy

**Temperature: AM** 85 °F **PM** 95 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0900 – AEG performing fusion work (clean-out fittings) on forcemain near LCS-5A. Also air/gas fittings on headers and laterals in the area near LCS-5A.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/27/2017

Contractor(s): AEG Report No.: 81

Weather: AM Light rain PM Cloudy
Temperature: AM 78 °F PM 85 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1200 – AEG crew begin road building/extension work for the day. Start delayed by rain. Jason Carter new AEG project supervisor starting today. Pressure testing to begin next week.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/28/2017

Contractor(s): AEG Report No.: 82

Weather: AM Partly sunny PM Mostly cloudy

**Temperature: AM** 75 °F **PM** 87 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0820 - AEG crew is working on culverts.

1610 – AEG crew is still working on the installation of storm water culverts.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 7/31/2017

Contractor(s): AEG Report No.: 83

Weather: AM Mostly cloudy PM Mostly cloudy

Temperature: AM 73 °F PM 86 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0810 – AEG crew continues working on storm water culverts between perimeter ditch and retention basing. Jason indicates limited crew today. Plan is to remove soil from perimeter road surface, place rock on road, then complete road work from bottom of slope using single-axle dump trucks. Ditch culverts ordered.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/1/2017

Contractor(s): AEG Report No.: 84

Weather: AM Mostly cloudy PM Mostly cloudy

Temperature: AM 76 °F PM 88 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0750 – AEG crew continues working on the installation of storm water culverts between the perimeter ditch and the retention basin.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location**: Bridgeton, MO **Date**: 8/2/2017

Contractor(s): AEG Report No.: 85

Weather: AM Partly cloudy PM Partly cloudy

**Temperature: AM** 76 °F **PM** 89 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0920 – AEG using dozer to backfill soil around culverts and scrape top layer of soil and rubble off of perimeter road. Also placing more rock on top of hill using single-axle dump truck (constructing pad for Layne pump removal work tomorrow).



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

Location: Bridgeton, MO Date: 8/3/2017

Contractor(s): AEG Report No.: 86

Weather: AM Sunny PM Mostly sunny

Temperature: AM 78 °F PM 92 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0820 – AEG crew working in South Quarry on raising/relocating infrastructure.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/4/2017

Contractor(s): AEG Report No.: 87

Weather: AM Partly cloudy PM Mostly sunny

**Temperature: AM** 65 °F **PM** 78 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0912 – AEG crew continues working in South Quarry on raising/relocating infrastructure.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/7/2017

Contractor(s): AEG Report No.: 88

Weather: AM Foggy PM Mostly cloudy

**Temperature: AM** 67 °F **PM** 79 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0733 – AEG crew continue working in South Quarry on raising/relocating infrastructure. Working on the last of the 18-in wells in the SQ, then will resume road work in NQ and work on 12-in pipe.



Page: 1 of 1

# **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/14/2017

Contractor(s): AEG Report No.: 89

Weather: AM Mostly cloudy PM Cloudy
Temperature: AM 71 °F PM 82 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0748 – AEG crew working on pipe fittings and line connections near north access road. Air testing to begin tomorrow.

1410 – FEI prepping to resume TMP installations. AEG crew continues pipe work on west side of north access road. Move fusion machine off TMP-28R drill pad.



Page: 1 of 1

#### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/15/2017

Contractor(s): AEG Report No.: 90

Weather: AM Mostly cloudy PM Partly cloudy

Temperature: AM 80 °F PM 89 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0930 - AEG performing air test on 12-in, 8-in, and 6-in lateral and header lines associated with gas extraction wells GEW-201, -40, -40R, -203, -202, -55, -55R, -204, -53, -53R, -207, -41R, -41R2, -43R, -43R2, -205, -206, -44, -51, -211, -214, -49, -212, -54, and -54R, and leachate collection sump LCS-5B. 10psi pressure applied to lines and maintained for 1 hour. Initial/ending ambient temps = 65 and 70 degrees F.

1053 – FEI passes air test.

1704 – AEG begins additional testing (6-in lateral lines associated with gas extraction wells GEW-42R and -200. 10psi pressure applied to lines and maintained for 1 hour. Initial/ending ambient temps = 81 and 81 degrees F.

1808 – FEI passes air test.



Page: 1 of 1

### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/16/2017

Contractor(s): AEG Report No.: 91

Weather: AM Mostly cloudy PM Mostly cloudy

Temperature: AM 80 °F PM 88 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1136 – AEG performing air test on 6-in laterals associated with gas extraction wells GEW-2, -3, -4, and -46R. 10psi pressure applied to lines and maintained for 1 hour. Initial/ending ambient temps = 79 and 81 degrees F.

1308 – FEI passes air test.



Page: 1 of 1

### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/17/2017

Contractor(s): AEG Report No.: 92

Weather: AM Mostly cloudy PM Mostly sunny

**Temperature: AM** 76 °F **PM** 87 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0712 – AEG performing air test on 3-in x 6-in dual containment forcemain around north side of North Quarry. Pressurized to 100psi but test failed due to cleanout gasket leak.

0943 – AEG performing air test on 12-in header and 6-in laterals associated with gas extraction wells GEW-45 and -47R. 10psi pressure applied to lines and maintained for 1 hour. Initial/ending ambient temps = 77 and 81 degrees F.

1107 – AEG has repaired gasket and restarts forcemain test.

1358 – FEI passes air test for GEW-45/-47R header & laterals.

1604 – AEG has repaired leaking valves on forcemain laterals and restarts the forcemain test again.

1752 – FEI fails forcemain test due to pressure loss. AEG to re-address tomorrow.



Page: 1 of 1

### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/18/2017

Contractor(s): AEG Report No.: 93

Weather: AM Partly cloudy PM Overcast Temperature: AM 75 °F PM 86 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1030: AEG performing air test on 3-inch inner diameter pipe of 3x6 forcemain beginning @ PZ-109-SS, running clockwise around north quarry, past CT-10, past GEW-2S, then splitting at tee located immediately downhill of GEW-2. One part of pipe extends from tee, past GEW-2, past GEW-3, and ends near GEW-4. Other part of pipe extends from tee and follows surface water trench to end near PZ-104R-SS. Initial pressure: 100 psi; ambient temp = 81 °F

1200: Final pressure: 100 psi; ambient temp = 81 °F. Section passes test.

1500: AEG begins air test on 3x6 forcemain beginning @ PZ-102R-SS, running along anchor trench to end adjacent to flare station. Initial pressure: 100 psi inner & 10 psi outer; ambient temp =  $89 \, ^{\circ}$ F

1605: Final pressure: 100 psi inner & 10 psi outer; ambient temp = 90 °F. Section passes test.

Copies to: Dan Feezor FEI Representative: Jonathan E Wilkinson, P.E.

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Page: 1 of 3

### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/19/2017

Contractor(s): AEG Report No.: 94

Weather: AM Mostly Sunny PM Mostly Sunny

Temperature: AM 72 °F PM 91 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700: AEG begins pressure test of 2-inch diameter pipe beginning @ GEW-47R to near LCS-6B, then splitting at tee near LCS-6B. One part of pipe extends from tee to GEW-4. Other part of pipe extends from tee to unlabeled CT near PEW-53 and PEW-52. Initial pressure: 100 psi; ambient temp = 71 °F

0800: Final pressure: 100 psi; ambient temp = 75 °F. Section passes test.

0830: AEG begins pressure test of 3x6 forcemain beginning at PEW-52 / PEW-53, then going uphill past GEW-49, past GEW-214, then to blind flange near TMP-44. From blind flange, the forcemain continues past GEW-211, past GEW-207, past GEW-54/54R, to anchor trench downhill of GEW-41/41R2, then uphill to GEW-40R, past GEW-55/55R, and terminating at GEW-53/53R. Initial pressure: 100 psi inner & 10 psi outer; ambient temp = 78 °F

0900: 3x6 forcemain test failed due to faulty gasket on cleanout near GEW-211. AEG replaces gasket and restarts test. Initial pressure: 100 psi inner & 10 psi outer; ambient temp = 78 °F

1000: Final pressure of 3x6 forcemain: 100 psi inner & 10 psi outer; ambient temp = 81 °F. Section passes test.

1045: AEG begins pressure test of 3x6 forcemain beginning at TMP-47 / TMP-48, runs past LCS-6B, splits into "y". One line from y terminates at GEW-47R. Other line from y terminates

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All

- at unlabeled CT near PEW-53 and PEW-52. Initial pressure: 100 psi inner & 10 psi outer; ambient temp = 82 °F
- 1115: AEG begins pressure test of 2-inch diameter air line beginning at GEW-4 and passes GEW-3, GEW-2, then proceeds downhill to perimeter access road. The line splits at a tee. The pipe from one side of the tee leads to CT-11. The other pipe from the tee splits into another tee a few feet away. One side of the pipe from the second tee leads to GEW-46R. The other pipe from the second tee leads clockwise around the perimeter access road to Road Crossing 4, near CT-12. Initial pressure: 100 psi inner; ambient temp = 86 °F
- 1215: Final pressure of 3x6 forcemain: 100 psi inner & 10 psi outer; ambient temp = 88 °F. 3x6 forcemain section passes test. Final pressure of 2-inch air line: 100 psi. 2-inch air line section passes test.
- 1309: AEG begins pressure test on 6-inch outer diameter pipe of 3x6 forcemain beginning @ PZ-109-SS, running clockwise around north quarry, past CT-10, past GEW-2S, then splitting at tee located immediately downhill of GEW-2. One part of pipe extends from tee, past GEW-2, past GEW-3, and ends near GEW-4. Other part of pipe extends from tee and follows surface water trench to end near PZ-104R-SS. The inner pipe was tested yesterday. For outer pipe, initial pressure: 10 psi; ambient temp = 81 °F
- 1325: AEG begins pressure test of 2-inch diameter air line beginning at PEW-48 and leading uphill to GEW-42R / 42R2: 100 psi; ambient temp = 89 °F
- 1410: Final pressure of 6-inch outer diameter pipe of 3x6 forcemain: 10 psi; ambient temp = 89 °F. Section passes test.
- 1415: Pressure of 2-inch diameter air line for test started @ 1325 is 96 psi and falling. AEG identifies and fixes leak in line.
- 1420: Restart pressure test of 2-inch diameter air line beginning at PEW-48 and leading to GEW-42R / 42R2: 100 psi; ambient temp = 89 °F
- 1420: AEG begins pressure test of 6-inch diameter outer pipe of 3x6 forcemain leading from GEW-42R to box near PEW-48. Starting pressure: 10 psi; ambient temp = 89 °F
- 1520: Pressure of 6-inch diameter outer pipe of 3x6 forcemain from GEW-42R to box: 9.5 psi. Section fails test.
- 1525: Final pressure of 2-inch diameter air line: 100 psi; ambient temp = 88 °F. Section passes test.
- 1536: Restart pressure test of 6-inch diameter outer pipe of 3x6 forcemain from GEW-42R to box. Initial pressure: 10.5 psi; ambient temp = 88 °F

1636: Pressure of 6-inch diameter outer pipe of 3x6 forcemain from GEW-42R to box: 10.25 psi.

Section fails test. AEG will retest tomorrow (8/21).



Page: 1 of 1

### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/21/2017

Contractor(s): AEG Report No.: 95

Weather: AM Partly cloudy PM Light rain
Temperature: AM 88 °F PM 87 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0700 — AEG performing air test on 6-in containment forcemain lateral associated with gas extraction wells GEW-42 and -200. 10psi pressure applied to lines and maintained for 1 hour. Initial/ending ambient temps = 82 and 82 degrees F.

0848 – FEI passes air test. Last air test for project.



Page: 1 of 1

### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/22/2017

Contractor(s): AEG Report No.: 96

Weather: AM Light rain PM Mostly cloudy

Temperature: AM 71 °F PM 81 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0746 – AEG reconnecting wellheads to new forcemain and gas extraction laterals. Remaining work includes abandoning old 2-in horizontal piping, abandoning old risers next to the extraction wells, and performing additional work on roads and the two culverts that flow into the northeast pond. Still waiting to install culverts in the perimeter ditch to allow for road crossings.



Page: 1 of 1

## **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/23/2017

Contractor(s): AEG Report No.: 97

Weather: AM Partly cloudy PM Partly cloudy

**Temperature: AM** 69 °F **PM** 78 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

0752 – AEG working on 2-in pipe abandonments and dressing up roads.



Page: 1 of 1

## **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 8/24/2017

Contractor(s): AEG Report No.: 98

Weather: AM Partly cloudy PM Mostly sunny

Temperature: AM 71 °F PM 81 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1243 – AEG continues working on road extensions/repairs, and installing perimeter ditch culverts and piping crossings.



Page: 1 of 1

### **Daily Field Summary Report**

Client: Bridgeton Landfill Job No.: BT-125

Project: Phase 1A/B North Quarry EVOH/LFG CQA Task No.: -

**Location:** Bridgeton, MO **Date:** 9/27/2017

Contractor(s): Report No.: 99

Weather: AM Mostly cloudy PM Mostly sunny

**Temperature: AM** 65 °F **PM** 74 °F

Description of field activities (include labor, equipment, site conditions, sampling, etc.)

1130 – I arrive onsite to perform survey of miscellaneous items for project record drawings and to evaluate the completion of the perimeter access road. All project work is complete. 1530 – I left the site.

Copies to: Dan Feezor FEI Representative. Grady 165

## **APPENDIX B**

## **GEOSYNTHETIC CONFORMANCE TESTING**

## **Sub-Appendices**

| <b>B.1</b> | EVOH Geomembrane Manufacturer's Quality Control Data |
|------------|--|
| <b>B.2</b> | Geotextile Manufacturer's Quality Control Data       |
| р э        | Consomposite Manufacturer's Quality Control Data     |

## Sub-Appendix B.1

## **EVOH Geomembrane Manufacturer's Quality Control Data**



Product Name: X60FC1 Sales Order # 201039 Size of product: 16 x 550

Absolute Barrier TM X-Series X60FC1 are a seven layer, co-extruded membrane consisting of high density polyethylene (HDPE) with an effective barrier core-layer to provide superior resistance to gas transmission. HDPE provides excellent chemical resistance and durability for long term applications.

| Roll #             | Thickness<br>ASTM<br>D5994 | Asperity<br>GM 12              | Tensile<br>(ppi)<br>ASTM<br>D 6693 | Elongation(%)        | Elongation(%)       | Tear (lbs.)  | Puncture<br>(lbs.)<br>ASTM D<br>4833 | OIT<br>Oxidative<br>Induction<br>Time<br>ASTM<br>D3895 |
|--------------------|----------------------------|--------------------------------|------------------------------------|----------------------|---------------------|--------------|--------------------------------------|--|
| Spe cification     | 50 mil<br>min. avg         | 10 mil min<br>avg.             | 75 lb/in.<br>min avg.              | MD 200 %<br>min avg. | TD 30 %<br>min avg. | 27 min. avg. | 55 min avg                           | 100 min.   |
| 7080198            | 57                         | G 18.9 B 22.2                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7080303            | 58                         | G 20.2 B 22.0                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7080358            | 57                         | G 19.2 B 20.4                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7080392            | 57                         | G 19.2 B 22.2                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7080474            | 56                         | G 17.0 B 21.1                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7080533            | 57                         | G 22.0 B 20.0                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7080628            | 56                         | G 17.6 B 23.0                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7080866            | 58                         | G 17.0 B 23.0                  | 155                                | 303%                 | 91%                 | 50           | 127                                  | 188  |
| 7081034            | 57                         | G 15.2 B 17.8                  | 155                                | 405%                 | 449%                | 49           | 127                                  | 188  |
|                    | 55                         | G 19.3 B 21.1                  | 155                                | 405%                 | 449%                | 49           | 125                                  | 188  |
| 7081252            | 55                         |                                |                                    |                      |                     | 49           |                                      | 188  |
| 7081551<br>7081930 | 58                         | G 16.1 B 18.5<br>G 27.4 B 20.0 | 155<br>155                         | 405%<br>405%         | 449%<br>449%        | 49           | 125<br>125                           | 188  |
|                    |                            |                                |                                    |                      | _                   | _            | _                                    |  |
| 7172029            | 51                         | G 20.5 B 26.8                  | 150                                | 334%                 | 309%                | 47           | 119                                  | 175  |
| 7172035            | 52                         | G 17.2 B 16.1                  | 150                                | 334%                 | 309%                | 47           | 119                                  | 175  |
| 7172216            | 54                         | G 20.3 B 21.3                  | 150                                | 334%                 | 309%                | 47           | 119                                  | 175  |

Note: Any resins used to make this product have met suppliers' certifications.

Customer: Republic Services Date: November 15, 2013

Pamela Weiler

Quality Assurance Technician II

Pamela Wieder

Raven Industries – Engineered Films Division

Raven Industries, Inc. • Engineered Films Division • 821 W Algonquin St. • Sioux Falls, SD 57104



Product Name: X60FC1 Sales Order # 201040 Size of product: 16 x 550

Absolute Barrier <sup>TM</sup> X-Series X60FC1 are a seven layer, co-extruded membrane consisting of high density polyethylene (HDPE) with an effective barrier core-layer to provide superior resistance to gas transmission. HDPE provides excellent chemical resistance and durability for long term applications.

| Roll #        | Thickness<br>ASTM<br>D5994 | Asperity<br>GM 12  | Tensile<br>(ppi)<br>ASTM<br>D 6693 | Elongation(%)        | Elongation(%)       | Tear (lbs.)  | Puncture<br>(lbs.)<br>ASTM D<br>4833 | OIT<br>Oxidative<br>Induction<br>Time<br>ASTM<br>D3895 |
|---------------|----------------------------|--------------------|------------------------------------|----------------------|---------------------|--------------|--------------------------------------|--|
| Specification | 50 mil<br>min. avg         | 10 mil min<br>avg. | 75 lb/in.<br>min avg.              | MD 200 %<br>min avg. | TD 30 %<br>min avg. | 27 min. avg. | 55 min avg                           | 100 min.   |
| 7172809       | 54.42                      | G 18.7 B 16.8      | 150                                | 334%                 | 284%                | 47           | 119                                  | 175  |
| 7174542       | 53.07                      | G 17.8 B 16.8      | 163                                | 456%                 | 359%                | 48           | 125                                  | 175  |
| 7174569       | 53.49                      | G 18.3 B 16.4      | 163                                | 456%                 | 359%                | 48           | 125                                  | 175  |
| 7174621       | 54.43                      | G 18.0 B 15.4      | 163                                | 456%                 | 359%                | 48           | 125                                  | 175  |
| 7175851       | 53.72                      | G 17.0 B 19.2      | 160                                | 506%                 | 473%                | 48           | 125                                  | 175  |
| 7175973       | 53.90                      | G 16.1 B 15.3      | 160                                | 506%                 | 473%                | 48           | 125                                  | 175  |
| 7176122       | 53.90                      | G 16.8 B 14.8      | 160                                | 506%                 | 473%                | 48           | 125                                  | 175  |
| 7176173       | 55.35                      | G 17.8 B 15.4      | 160                                | 506%                 | 473%                | 48           | 125                                  | 175  |
| 7176218       | 59.80                      | G 15.6 B 16.1      | 160                                | 506%                 | 473%                | 48           | 125                                  | 175  |
| 7176308       | 53.86                      | G 16.6 B 15.2      | 163                                | 486%                 | 391%                | 47           | 126                                  | 175  |
| 7176326       | 51.45                      | G 18.9 B 18.5      | 163                                | 486%                 | 391%                | 47           | 126                                  | 175  |
| 7176347       | 53.27                      | G 18.3 B 15.7      | 163                                | 486%                 | 391%                | 47           | 126                                  | 175  |
| 7176368       | 53.58                      | G 19.3 B 15.6      | 163                                | 486%                 | 391%                | 47           | 126                                  | 175  |
| 7176384       | 53.95                      | G 17.7 B 17.5      | 163                                | 486%                 | 391%                | 47           | 126                                  | 175  |
| 7176434       | 55.06                      | G 17.3 B 16.1      | 163                                | 486%                 | 391%                | 47           | 126                                  | 175  |

Note: Any resins used to make this product have met suppliers' certifications.

Customer: Republic Services Date: November 20, 2013

Pamela Weiler

Quality Assurance Technician II

Pamela Wieder

Raven Industries – Engineered Films Division

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Product Name: X60FC1 Sales Order # 201041 Size of product: 16 x 550

Absolute Barrier TM X-Series X60FC1 are a seven layer, co-extruded membrane consisting of high density polyethylene (HDPE) with an effective barrier core-layer to provide superior resistance to gas transmission. HDPE provides excellent chemical resistance and durability for long term applications.

| Roll#         | Thickness<br>ASTM<br>D5994 | Asperity<br>GM 12  | Tensile<br>(ppi)<br>ASTM<br>D 6693 | Elongation(%)        | Elongation(%)       | Tear (lbs.)  | Puncture<br>(lbs.)<br>ASTM D<br>4833 | OIT Oxidative Induction Time ASTM D3895 |
|---------------|----------------------------|--------------------|------------------------------------|----------------------|---------------------|--------------|--------------------------------------|---|
| Specification | 50 mil<br>min. avg         | 10 mil min<br>avg. | 75 lb/in.<br>min avg.              | MD 200 %<br>min avg. | TD 30 %<br>min avg. | 27 min. avg. | 55 min avg                           | 100 min.                                |
| 7171890       | 51.8                       | G 20.5 B 26.8      | 155                                | 334%                 | 309%                | 50           | 127                                  | 188                                     |
| 7173331       | 54.4                       | G 16.3 B 16.1      | 150                                | 599%                 | 536%                | 47           | 119                                  | 175                                     |
| 7173374       | 53.9                       | G 15.4 B 15.3      | 150                                | 599%                 | 536%                | 47           | 119                                  | 175                                     |
| 7175501       | 56.1                       | G 15.9 B 13.1      | 160                                | 505%                 | 472%                | 47           | 119                                  | 175                                     |
| 7176598       | 54.7                       | G 14.5 B 14.1      | 163                                | 486%                 | 296%                | 47           | 126                                  | 175                                     |
| 7177308       | 55.6                       | G 14.5 B 14.3      | 154                                | 322%                 | 265%                | 47           | 127                                  | 175                                     |
| 7177336       | 56.0                       | G 15.4 B 17.5      | 154                                | 322%                 | 265%                | 47           | 127                                  | 175                                     |
| 7177661       | 55.8                       | G 18.1 B 12.0      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |
| 7177758       | 54.2                       | G 16.6 B 14.2      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |
| 7177955       | 55.7                       | G 15.4 B 14.8      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |
| 7178175       | 56.6                       | G 16.3 B 14.1      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |
| 7178363       | 54.0                       | G 13.3 B 13.8      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |
| 7178638       | 55.5                       | G 17.4 B 15.7      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |
| 7178776       | 56.0                       | G 17.7 B 14.5      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |
| 7178843       | 54.3                       | G 17.0 B 13.7      | 163                                | 517%                 | 381%                | 48           | 123                                  | 175                                     |

Note: Any resins used to make this product have met suppliers' certifications.

Customer: Republic Services Date: November 21, 2013

Clint Boerhave Quality Manager

Quality Ivialiagei

Raven Industries – Engineered Films Division

Raven Industries, Inc. • Engineered Films Division • 821 W Algonquin St. • Sioux Falls, SD 57104



Product Name: X60FC1 Sales Order # 201042 Size of product: 16 x 550

Absolute Barrier <sup>TM</sup> X-Series X60FC1 are a seven layer, co-extruded membrane consisting of high density polyethylene (HDPE) with an effective barrier core-layer to provide superior resistance to gas transmission. HDPE provides excellent chemical resistance and durability for long term applications.

| Roll #        | Thickness<br>ASTM<br>D5994 | Asperity<br>GM 12     | Tensile<br>(ppi)<br>ASTM<br>D 6693 | Elongation(%)        | Elongation(%)       | Tear (lbs.) ASTM D1004 | Puncture<br>(lbs.)<br>ASTM D<br>4833 | OIT Oxidative Induction Time ASTM D3895 |
|---------------|----------------------------|-----------------------|------------------------------------|----------------------|---------------------|------------------------|--------------------------------------|---|
| Specification | 50 mil<br>min. avg         | 10 mil min            | 75 lb/in.<br>min avg.              | MD 200 %<br>min avg. | TD 30 %<br>min avg. | 27 min. avg.           | 55 min avg                           | 100 min.                                |
| 7175605       | 54.8                       | avg.<br>G 15.9 B 15.5 | 160                                | 505%                 | 472%                | 47                     | 119                                  | 175                                     |
| 7177361       | 56.3                       | G 15.8 B 14.8         | 154                                | 322%                 | 265%                | 47                     | 127                                  | 175                                     |
| 7177400       | 55.5                       | G 15.7 B 15.3         | 154                                | 322%                 | 265%                | 47                     | 127                                  | 175                                     |
| 7177406       | 55.3                       | G 16.9 B 15.8         | 154                                | 322%                 | 265%                | 47                     | 127                                  | 175                                     |
| 7177460       | 55.8                       | G 15.9 B 16.3         | 154                                | 322%                 | 265%                | 47                     | 127                                  | 175                                     |
| 7177494       | 55.7                       | G 16.3 B 22.3         | 154                                | 322%                 | 265%                | 47                     | 127                                  | 175                                     |
| 7177524       | 55.3                       | G 18.7 B 15.7         | 154                                | 322%                 | 265%                | 47                     | 127                                  | 175                                     |
| 7177602       | 55.7                       | G 15.8 B 16.0         | 163                                | 517%                 | 381%                | 48                     | 123                                  | 175                                     |
| 7178492       | 53.9                       | G 16.5 B 13.7         | 163                                | 517%                 | 381%                | 48                     | 123                                  | 175                                     |
| 7178919       | 55.2                       | G 20.9 B 17.2         | 163                                | 482%                 | 467%                | 48                     | 123                                  | 175                                     |
| 7179003       | 58.1                       | G 16.1 B 17.8         | 163                                | 482%                 | 467%                | 48                     | 123                                  | 175                                     |
| 7179075       | 54.4                       | G 17.9 B 16.7         | 163                                | 482%                 | 467%                | 48                     | 123                                  | 175                                     |
| 7179145       | 56.4                       | G 17.5 B 16.1         | 163                                | 482%                 | 467%                | 48                     | 123                                  | 175                                     |
| 7179173       | 54.5                       | G 17.3 B 15.2         | 163                                | 482%                 | 467%                | 48                     | 123                                  | 175                                     |
| 7179242       | 55.5                       | G 19.2 B 17.4         | 163                                | 482%                 | 467%                | 48                     | 123                                  | 175                                     |

Note: Any resins used to make this product have met suppliers' certifications.

Customer: Republic Services Date: November 21, 2013

Clint Boerhave Quality Manager

Raven Industries – Engineered Films Division

Raven Industries, Inc. • Engineered Films Division • 821 W Algonquin St. • Sioux Falls, SD 57104



Product Name: X60FC1 Sales Order # 201044 Size of product: 16 x 550

Absolute Barrier TM X-Series X60FC1 are a seven layer, co-extruded membrane consisting of high density polyethylene (HDPE) with an effective barrier core-layer to provide superior resistance to gas transmission. HDPE provides excellent chemical resistance and durability for long term applications.

| Roll#         | Thickness<br>ASTM<br>D5994 | Asperity<br>GM 12  | Tensile<br>(ppi)<br>ASTM<br>D 6693 | Elongation(%)        | Elongation(%)       | Tear (lbs.)<br>ASTM D1004 | Puncture<br>(lbs.)<br>ASTM D<br>4833 | OIT<br>Oxidative<br>Induction<br>Time<br>ASTM<br>D3895 |
|---------------|----------------------------|--------------------|------------------------------------|----------------------|---------------------|---------------------------|--------------------------------------|--|
| Specification | 50 mil<br>min. avg         | 10 mil min<br>avg. | 75 lb/in.<br>min avg.              | MD 200 %<br>min avg. | TD 30 %<br>min avg. | 27 min. avg.              | 55 min avg                           | 100 min.   |
| 7171929       | 51.1                       | G 24.1 B 19.4      | 150                                | 309%                 | 118%                | 47                        | 119                                  | 175  |
| 7173290       | 54.7                       | G 15.2 B 15.7      | 178                                | 529%                 | 536%                | 47                        | 119                                  | 175  |
| 7173504       | 54.0                       | G 13.9 B 12.6      | 178                                | 529%                 | 536%                | 47                        | 119                                  | 175  |
| 7173687       | 55.1                       | G 14.7 B 13.7      | 178                                | 529%                 | 536%                | 47                        | 119                                  | 175  |
| 7174446       | 54.7                       | G 15.9 B 15.8      | 163                                | 456%                 | 359%                | 48                        | 125                                  | 175  |
| 7188820       | 55.5                       | G 15.3 B 14.4      | 155                                | 463%                 | 484%                | 49                        | 124                                  | 175  |
| 7188997       | 60.0                       | G 11.3 B 11.9      | 155                                | 463%                 | 484%                | 49                        | 124                                  | 175  |
| 7189137       | 53.9                       | G 14.6 B 16.2      | 155                                | 463%                 | 484%                | 49                        | 124                                  | 175  |
| 7189388       | 54.9                       | G 15.5 B 13.9      | 155                                | 463%                 | 484%                | 49                        | 124                                  | 175  |
| 7189562       | 53.1                       | G 13.8 B 11.6      | 155                                | 463%                 | 484%                | 49                        | 124                                  | 175  |
| 7189739       | 54.7                       | G 14.6 B 14.4      | 155                                | 463%                 | 484%                | 49                        | 124                                  | 175  |
| 7189991       | 53.1                       | G 14.8 B 14.7      | 155                                | 463%                 | 484%                | 49                        | 124                                  | 175  |
| 7190194       | 54.5                       | G17.1 B 13.6       | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175  |
| 7190775       | 55.8                       | G 15.1 B 13.6      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175  |
| 7190889       | 55.7                       | G 14.9 B 13.8      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175  |

Note: Any resins used to make this product have met suppliers' certifications.

Customer: Republic Services Date: November 30, 2013

Pamela Weiler

Quality Assurance Technician II

Raven Industries – Engineered Films Division

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Raven Industries, Inc. • Engineered Films Division • 821 W Algonquin St. • Sioux Falls, SD 57104



Product Name: X60FC1 Sales Order # 201045 Size of product: 16 x 550

Absolute Barrier ™ X-Series X60FC1 are a seven layer, co-extruded membrane consisting of high density polyethylene (HDPE) with an effective barrier core-layer to provide superior resistance to gas transmission. HDPE provides excellent chemical resistance and durability for long term applications.

| Roll#         | Thickness<br>ASTM<br>D5994 | Asperity<br>GM 12  | Tensile<br>(ppi)<br>ASTM<br>D 6693 | Elongation(%)        | Elongation(%)       | Tear (lbs.)<br>ASTM D1004 | Puncture<br>(lbs.)<br>ASTM D<br>4833 | OIT Oxidative Induction Time ASTM D3895 |
|---------------|----------------------------|--------------------|------------------------------------|----------------------|---------------------|---------------------------|--------------------------------------|---|
| Specification | 50 mil<br>min. avg         | 10 mil min<br>avg. | 75 lb/in.<br>min avg.              | MD 200 %<br>min avg. | TD 30 %<br>min avg. | 27 min. avg.              | 55 min avg                           | 100 min.                                |
| 7174686       | 55.6                       | G 16.3 B 16.1      | 163                                | 456%                 | 359%                | 48                        | 125                                  | 175                                     |
| 7179682       | 56.9                       | G 18.0 B 15.0      | 160                                | 506%                 | 472%                | 48                        | 125                                  | 175                                     |
| 7190290       | 54.5                       | G 13.4 B 14.1      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175                                     |
| 7190332       | 55.6                       | G 13.7 B 13.8      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175                                     |
| 7190412       | 54.1                       | G 14.7 B 13.8      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175                                     |
| 7190496       | 55.2                       | G 13.6 B 15.5      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175                                     |
| 7190540       | 55.6                       | G 15.2 B 14.3      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175                                     |
| 7190619       | 55.1                       | G 18.1 B 15.5      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175                                     |
| 7190734       | 54.4                       | G 16.8 B 14.4      | 168                                | 447%                 | 451%                | 49                        | 127                                  | 175                                     |
| 7191049       | 54.8                       | G 16.6 B 15.4      | 169                                | 508%                 | 466%                | 49                        | 127                                  | 175                                     |
| 7191181       | 55.0                       | G 14.7 B 14.7      | 169                                | 508%                 | 466%                | 49                        | 127                                  | 175                                     |
| 7191358       | 53.7                       | G 16.6 B 13.1      | 169                                | 508%                 | 466%                | 49                        | 127                                  | 175                                     |
| 7191477       | 55.8                       | G 15.6 B 17.2      | 169                                | 508%                 | 466%                | 49                        | 127                                  | 175                                     |
| 7191661       | 54.4                       | G 14.2 B 12.7      | 169                                | 508%                 | 466%                | 49                        | 127                                  | 175                                     |
| 7191859       | 54.9                       | G 16.5 B 13.8      | 168                                | 514%                 | 515%                | 50                        | 129                                  | 175                                     |

Note: Any resins used to make this product have met suppliers' certifications.

Customer: Republic Services Date: November 30, 2013

Pamela Weiler

Quality Assurance Technician II

Raven Industries – Engineered Films Division

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Raven Industries, Inc. • Engineered Films Division • 821 W Algonquin St. • Sioux Falls, SD 57104

## Sub-Appendix B.2

## **Geotextile Manufacturer's Quality Control Data**



SKAPS Industries (Nonwoven Division) 335, Athena Drive Athens, GA 30601 (U.S.A.) Phone (706) 354-3700 Fax (706) 354-3737

E-mail: contact@skaps.com

Sales Office:

Engineered Synthetic Product Inc.

Phone: (770)564-1857 Fax: (770)564-1818

December 27, 2016 Republic Waste Services

Ref : Bridgeton LF **PO : Bridgeton** 

Dear Sir/Madam:

This is to certify that SKAPS GE160 is a high quality needle-punched nonwoven geotextile made of 100% polypropylene staple fibers, randomly networked to form a high strength dimensionally stable fabric. SKAPS GE160 resists ultraviolet deterioration, rotting, biological degradation. The fabric is inert to commonly encountered soil chemicals. Polypropylene is stable within a pH range of 2 to 13. SKAPS GE160 conforms to the property values listed below:

| PROPERTY      | TEST METHOD | UNITS             | M.A.R.V.<br>Minimum Average Roll Value |
|---------------|-------------|-------------------|--|
| Weight        | ASTM D 5261 | oz/sy (g/m²)      | 6.00 (203)                             |
| Grab Tensile  | ASTM D 4632 | lbs (kN)          | 160 (0.71)                             |
| CBR Puncture  | ASTM D 6241 | lbs (kN)          | 450 (2.00)                             |
| Permittivity* | ASTM D 4491 | sec <sup>-1</sup> | 1.63                                   |
| AOS*          | ASTM D 4751 | US Sieve (mm)     | 70 (0.21)                              |
| UV Resistance | ASTM D 4355 | %/hrs             | 70/500                                 |

#### **Notes:**

## **KOUROSH SABZEVARI**

QUALITY CONTROL MANAGER

www.skaps.com

www.espgeosynthetics.com

<sup>\*</sup> At the time of manufacturing. Handling may change these properties.

**Product : GE160-180** 

| ROLL #<br>ASTM METHOD | WEIGHT<br>D5261 | MD TENSILE<br>D4632 | XMD TENSILE<br>D4632 | CBR PUNCTURE<br>D6241 | AOS<br>D4751 | PERMITTIVITY<br>D4491 |
|-----------------------|-----------------|---------------------|----------------------|-----------------------|--------------|-----------------------|
| UNITS                 | oz/sq yd        | lbs.                | lbs                  | lbs.                  | US Sieve     | sec <sup>-1</sup>     |
| TARGET                | 6.00            | 160                 | 160                  | 450                   | 70           | 1.63                  |
| 45619.1               | 6.59            | 166                 | 177                  | 498                   | 70           | 1.77                  |
| 45619.2               | 6.59            | 166                 | 177                  | 498                   | 70           | 1.77                  |
| 45619.3               | 6.59            | 166                 | 177                  | 498                   | 70           | 1.77                  |
| 45619.4               | 6.59            | 166                 | 177                  | 498                   | 70           | 1.77                  |
| 45619.5               | 6.35            | 161                 | 173                  | 498                   | 70           | 1.77                  |
| 45619.6               | 6.35            | 161                 | 173                  | 498                   | 70           | 1.77                  |
| 45619.7               | 6.35            | 161                 | 173                  | 498                   | 70           | 1.77                  |
| 45619.8               | 6.35            | 161                 | 173                  | 498                   | 70           | 1.77                  |
| 45619.9               | 6.35            | 161                 | 173                  | 498                   | 70           | 1.77                  |
| 45619.10              | 6.68            | 169                 | 180                  | 482                   | 70           | 1.77                  |
| 45619.11              | 6.68            | 169                 | 180                  | 482                   | 70           | 1.77                  |
| 45619.12              | 6.68            | 169                 | 180                  | 482                   | 70           | 1.77                  |
| 45619.13              | 6.68            | 169                 | 180                  | 482                   | 70           | 1.77                  |
| 45619.14              | 6.68            | 169                 | 180                  | 482                   | 70           | 1.77                  |
| 45619.15              | 6.24            | 164                 | 170                  | 482                   | 70           | 1.77                  |
| 45619.16              | 6.24            | 164                 | 170                  | 482                   | 70           | 1.77                  |
| 45619.17              | 6.24            | 164                 | 170                  | 482                   | 70           | 1.77                  |
| 45619.18              | 6.24            | 164                 | 170                  | 482                   | 70           | 1.77                  |
| 45619.19              | 6.24            | 164                 | 170                  | 482                   | 70           | 1.77                  |
| 45619.20              | 6.42            | 167                 | 176                  | 487                   | 70           | 1.77                  |
| 45619.21              | 6.42            | 167                 | 176                  | 487                   | 70           | 1.77                  |
| 45619.22              | 6.42            | 167                 | 176                  | 487                   | 70           | 1.77                  |
| 45619.23              | 6.42            | 167                 | 176                  | 487                   | 70           | 1.77                  |
| 45619.24              | 6.42            | 167                 | 176                  | 487                   | 70           | 1.77                  |
| 45619.25              | 6.39            | 160                 | 174                  | 487                   | 70           | 1.77                  |
| 45619.26              | 6.39            | 160                 | 174                  | 487                   | 70           | 1.77                  |
| 45619.27              | 6.39            | 160                 | 174                  | 487                   | 70           | 1.77                  |
| 45619.28              | 6.39            | 160                 | 174                  | 487                   | 70           | 1.77                  |



SKAPS Industries (Nonwoven Division) 335, Athena Drive Athens, GA 30601 (U.S.A.) Phone (706) 354-3700 Fax (706) 354-3737

E-mail: info@skaps.com

Sales Office:

Engineered Synthetic Product Inc.

Phone: (770)564-1857 Fax: (770)564-1818

October 29, 2013 Republic Waste Services, Inc.

Ref: RWS Bridgeton Landfill

PO: Phase 2

Dear Sir/Madam:

This is to certify that SKAPS GE180 is a high quality needle-punched nonwoven geotextile made of 100% polypropylene staple fibers, randomly networked to form a high strength dimensionally stable fabric.SKAPS GE180 resists ultraviolet deterioration, rotting, biological degradation. The fabric is inert to commonly encountered soil chemicals. Polypropylene is stable within a pH range of 2 to 13. SKAPS GE180 conforms to the property values listed below:

| PROPERTY              | TEST METHOD | UNITS                                       | M.A.R.V.<br>Minimum Average Roll Value |
|-----------------------|-------------|---|--|
| Weight                | ASTM D 5261 | oz/sy (g/m²)                                | 8.00 (271)                             |
| Thickness*            | ASTM D 5199 | mils (mm)                                   | 100 (2.54)                             |
| Grab Tensile          | ASTM D 4632 | lbs (kN)                                    | 225 (1.00)                             |
| Grab Elongation       | ASTM D 4632 | %   | 50                                     |
| Trapezoidal Tear      | ASTM D 4533 | lbs (kN)                                    | 90 (0.40)                              |
| Puncture Resistance   | ASTM D 4833 | lbs (kN)                                    | 130 (0.58)                             |
| Mullen Burst Strength | ASTM D 3786 | psi (kPa)                                   | 425 (2930)                             |
| Permittivity*         | ASTM D 4491 | sec <sup>-1</sup>                           | 1.26                                   |
| Permeability*         | ASTM D 4491 | cm/sec                                      | 0.30                                   |
| Water Flow*           | ASTM D 4491 | gpm/ft <sup>2</sup> (l/min/m <sup>2</sup> ) | 100 (4074)                             |
| AOS*                  | ASTM D 4751 | US Sieve (mm)                               | 80 (0.18)                              |
| UV Resistance         | ASTM D 4355 | %/hrs                                       | 70/500                                 |

### Notes:

## **PALAK PATEL**

QUALITY CONTROL MANAGER

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<sup>\*</sup> At the time of manufacturing. Handling may change these properties.

### Product : GE180-180

| ROLL#       | WEIGHT   | THICKNESS | MD TENSILE | MD ELONG | XMD TENSILE | XMD ELONG | MD TRAP | XMD TRAP | PUNCTURE | MULLEN | AOS             |                     | PERMEABILITY | PERMITTIVITY      |
|-------------|----------|-----------|------------|----------|-------------|-----------|---------|----------|----------|--------|-----------------|---------------------|--------------|-------------------|
| ASTM METHOD | D5261    | D5199     | D4632      | D4632    | D4632       | D4632     | D4533   | D4533    | D4833    | D3786  | D4751           | D4491               | D4491        | D4491             |
| UNITS       | oz/sq yd | (mils)    | lbs.       | %        | lbs         | %         | lbs.    | lbs      | lbs.     | psi    | <b>US Sieve</b> | gpm/ft <sup>2</sup> | cm/sec       | sec <sup>-1</sup> |
| TARGET      | 8.00     | 100       | 225        | 50       | 225         | 50        | 90      | 90       | 130      | 425    | 80              | 100                 | 0.30         | 1.26              |
| 31966.001   | 8.54     | 123       | 234        | 74       | 244         | 85        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.002   | 8.54     | 123       | 234        | 74       | 244         | 85        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.003   | 8.54     | 123       | 234        | 74       | 244         | 85        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.004   | 8.54     | 123       | 234        | 74       | 244         | 85        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.005   | 8.13     | 120       | 229        | 68       | 233         | 76        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.006   | 8.13     | 120       | 229        | 68       | 233         | 76        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.007   | 8.13     | 120       | 229        | 68       | 233         | 76        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.008   | 8.13     | 120       | 229        | 68       | 233         | 76        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.009   | 8.13     | 120       | 229        | 68       | 233         | 76        | 104     | 118      | 139      | 434    | 80              | 104                 | 0.43         | 1.39              |
| 31966.010   | 8.36     | 125       | 231        | 71       | 240         | 82        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.011   | 8.36     | 125       | 231        | 71       | 240         | 82        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.012   | 8.36     | 125       | 231        | 71       | 240         | 82        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.013   | 8.36     | 125       | 231        | 71       | 240         | 82        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.014   | 8.36     | 125       | 231        | 71       | 240         | 82        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.015   | 8.10     | 122       | 226        | 65       | 230         | 79        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.016   | 8.10     | 122       | 226        | 65       | 230         | 79        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.017   | 8.10     | 122       | 226        | 65       | 230         | 79        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.018   | 8.10     | 122       | 226        | 65       | 230         | 79        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.019   | 8.10     | 122       | 226        | 65       | 230         | 79        | 96      | 107      | 135      | 429    | 80              | 104                 | 0.43         | 1.39              |
| 31966.020   | 8.42     | 124       | 235        | 73       | 242         | 84        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.021   | 8.42     | 124       | 235        | 73       | 242         | 84        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.022   | 8.42     | 124       | 235        | 73       | 242         | 84        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.023   | 8.42     | 124       | 235        | 73       | 242         | 84        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.024   | 8.42     | 124       | 235        | 73       | 242         | 84        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.025   | 8.21     | 120       | 228        | 67       | 236         | 75        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.026   | 8.21     | 120       | 228        | 67       | 236         | 75        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.027   | 8.21     | 120       | 228        | 67       | 236         | 75        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.028   | 8.21     | 120       | 228        | 67       | 236         | 75        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.029   | 8.21     | 120       | 228        | 67       | 236         | 75        | 101     | 110      | 137      | 431    | 80              | 104                 | 0.43         | 1.39              |
| 31966.030   | 8.40     | 123       | 233        | 75       | 238         | 81        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.031   | 8.40     | 123       | 233        | 75       | 238         | 81        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.032   | 8.40     | 123       | 233        | 75       | 238         | 81        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.033   | 8.40     | 123       | 233        | 75       | 238         | 81        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.034   | 8.40     | 123       | 233        | 75       | 238         | 81        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.035   | 8.17     | 121       | 225        | 69       | 231         | 77        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.036   | 8.17     | 121       | 225        | 69       | 231         | 77        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.037   | 8.17     | 121       | 225        | 69       | 231         | 77        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.038   | 8.17     | 121       | 225        | 69       | 231         | 77        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.039   | 8.17     | 121       | 225        | 69       | 231         | 77        | 99      | 104      | 132      | 426    | 80              | 104                 | 0.43         | 1.39              |
| 31966.040   | 8.56     | 125       | 231        | 72       | 243         | 83        | 103     | 114      | 140      | 433    | 80              | 104                 | 0.43         | 1.39              |

<sup>\*</sup>All Values are MARV.

**Product : GE180-180** 

| ROLL#       | WEIGHT   | THICKNESS | MD TENSILE | MD ELONG | XMD TENSILE | XMD ELONG | MD TRAP | XMD TRAP | PUNCTURE | MULLEN | AOS      | _                   | PERMEABILITY | PERMITTIVITY      |
|-------------|----------|-----------|------------|----------|-------------|-----------|---------|----------|----------|--------|----------|---------------------|--------------|-------------------|
| ASTM METHOD | D5261    | D5199     | D4632      | D4632    | D4632       | D4632     | D4533   | D4533    | D4833    | D3786  | D4751    | D4491               | D4491        | D4491             |
| UNITS       | oz/sq yd | (mils)    | lbs.       | %        | lbs         | %         | lbs.    | lbs      | lbs.     | psi    | US Sieve | gpm/ft <sup>2</sup> | cm/sec       | sec <sup>-1</sup> |
| TARGET      | 8.00     | 100       | 225        | 50       | 225         | 50        | 90      | 90       | 130      | 425    | 80       | 100                 | 0.30         | 1.26              |
| 31966.041   | 8.56     | 125       | 231        | 72       | 243         | 83        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.042   | 8.56     | 125       | 231        | 72       | 243         | 83        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.043   | 8.56     | 125       | 231        | 72       | 243         | 83        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.044   | 8.56     | 125       | 231        | 72       | 243         | 83        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.045   | 8.34     | 120       | 229        | 66       | 235         | 79        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.046   | 8.34     | 120       | 229        | 66       | 235         | 79        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.047   | 8.34     | 120       | 229        | 66       | 235         | 79        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.048   | 8.34     | 120       | 229        | 66       | 235         | 79        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.049   | 8.34     | 120       | 229        | 66       | 235         | 79        | 103     | 114      | 140      | 433    | 80       | 104                 | 0.43         | 1.39              |
| 31966.050   | 8.44     | 124       | 234        | 74       | 239         | 85        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.051   | 8.44     | 124       | 234        | 74       | 239         | 85        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.052   | 8.44     | 124       | 234        | 74       | 239         | 85        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.053   | 8.44     | 124       | 234        | 74       | 239         | 85        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.054   | 8.44     | 124       | 234        | 74       | 239         | 85        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.055   | 8.11     | 121       | 227        | 68       | 237         | 76        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.056   | 8.11     | 121       | 227        | 68       | 237         | 76        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.057   | 8.11     | 121       | 227        | 68       | 237         | 76        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.058   | 8.11     | 121       | 227        | 68       | 237         | 76        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.059   | 8.11     | 121       | 227        | 68       | 237         | 76        | 97      | 102      | 130      | 428    | 80       | 100                 | 0.42         | 1.33              |
| 31966.060   | 8.51     | 125       | 232        | 71       | 241         | 82        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.061   | 8.51     | 125       | 232        | 71       | 241         | 82        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.062   | 8.51     | 125       | 232        | 71       | 241         | 82        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.063   | 8.51     | 125       | 232        | 71       | 241         | 82        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.064   | 8.51     | 125       | 232        | 71       | 241         | 82        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.065   | 8.35     | 122       | 230        | 65       | 233         | 78        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.066   | 8.35     | 122       | 230        | 65       | 233         | 78        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.067   | 8.35     | 122       | 230        | 65       | 233         | 78        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.068   | 8.35     | 122       | 230        | 65       | 233         | 78        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.069   | 8.35     | 122       | 230        | 65       | 233         | 78        | 105     | 112      | 138      | 435    | 80       | 100                 | 0.42         | 1.33              |
| 31966.070   | 8.38     | 124       | 235        | 73       | 244         | 84        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.071   | 8.38     | 124       | 235        | 73       | 244         | 84        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.072   | 8.38     | 124       | 235        | 73       | 244         | 84        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.073   | 8.38     | 124       | 235        | 73       | 244         | 84        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.074   | 8.38     | 124       | 235        | 73       | 244         | 84        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.075   | 8.27     | 121       | 226        | 70       | 230         | 76        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.076   | 8.27     | 121       | 226        | 70       | 230         | 76        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.077   | 8.27     | 121       | 226        | 70       | 230         | 76        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.078   | 8.27     | 121       | 226        | 70       | 230         | 76        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.079   | 8.27     | 121       | 226        | 70       | 230         | 76        | 95      | 106      | 133      | 430    | 80       | 100                 | 0.42         | 1.33              |
| 31966.080   | 8.59     | 123       | 230        | 75       | 240         | 81        | 102     | 115      | 136      | 432    | 80       | 100                 | 0.42         | 1.33              |

<sup>\*</sup>All Values are MARV.

**Product : GE180-180** 

| ROLL#                  | WEIGHT       | THICKNESS  | MD TENSILE | MD ELONG | XMD TENSILE | XMD ELONG | MD TRAP    | XMD TRAP   | PUNCTURE   | MULLEN     | AOS             | WATER FLOW          | PERMEABILITY | PERMITTIVITY      |
|------------------------|--------------|------------|------------|----------|-------------|-----------|------------|------------|------------|------------|-----------------|---------------------|--------------|-------------------|
| ASTM METHOD            | D5261        | D5199      | D4632      | D4632    | D4632       | D4632     | D4533      | D4533      | D4833      | D3786      | D4751           | D4491               | D4491        | D4491             |
| UNITS                  | oz/sq yd     | (mils)     | lbs.       | %        | lbs         | %         | lbs.       | lbs        | lbs.       | psi        | <b>US Sieve</b> | gpm/ft <sup>2</sup> | cm/sec       | sec <sup>-1</sup> |
| TARGET                 | 8.00         | 100        | 225        | 50       | 225         | 50        | 90         | 90         | 130        | 425        | 80              | 100                 | 0.30         | 1.26              |
| 31966.081              | 8.59         | 123        | 230        | 75       | 240         | 81        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.082              | 8.59         | 123        | 230        | 75       | 240         | 81        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.083              | 8.59         | 123        | 230        | 75       | 240         | 81        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.084              | 8.59         | 123        | 230        | 75       | 240         | 81        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.085              | 8.13         | 120        | 228        | 67       | 232         | 79        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.086              | 8.13         | 120        | 228        | 67       | 232         | 79        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.087              | 8.13         | 120        | 228        | 67       | 232         | 79        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.088              | 8.13         | 120        | 228        | 67       | 232         | 79        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.089              | 8.13         | 120        | 228        | 67       | 232         | 79        | 102        | 115        | 136        | 432        | 80              | 100                 | 0.42         | 1.33              |
| 31966.090              | 8.45         | 125        | 233        | 72       | 242         | 83        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.091              | 8.45         | 125        | 233        | 72       | 242         | 83        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.092              | 8.45         | 125        | 233        | 72       | 242         | 83        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.093              | 8.45         | 125        | 233        | 72       | 242         | 83        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.094              | 8.45         | 125        | 233        | 72       | 242         | 83        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.095              | 8.30         | 122        | 225        | 69       | 234         | 77        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.096              | 8.30         | 122        | 225        | 69       | 234         | 77        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.097              | 8.30         | 122        | 225        | 69       | 234         | 77        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.098              | 8.30         | 122        | 225        | 69       | 234         | 77        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.099              | 8.30         | 122        | 225        | 69       | 234         | 77        | 98         | 103        | 131        | 427        | 80              | 100                 | 0.42         | 1.33              |
| 31966.100              | 8.36         | 124        | 231        | 74       | 238         | 80        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.101              | 8.36         | 124        | 231        | 74       | 238         | 80        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.102              | 8.36         | 124        | 231        | 74       | 238         | 80        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.103              | 8.36         | 124        | 231        | 74       | 238         | 80        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.104              | 8.36         | 124        | 231        | 74       | 238         | 80        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.105              | 8.26         | 121        | 229        | 66       | 231         | 75        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.106              | 8.26         | 121        | 229        | 66       | 231         | 75        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.107              | 8.26         | 121        | 229        | 66       | 231         | 75        | 100        | 113        | 140        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.108<br>31966.109 | 8.26<br>8.26 | 121<br>121 | 229<br>229 | 66<br>66 | 231<br>231  | 75<br>75  | 100<br>100 | 113<br>113 | 140<br>140 | 434<br>434 | 80<br>80        | 102<br>102          | 0.43<br>0.43 | 1.36<br>1.36      |
| 31966.110              | 8.52         | 121        | 234        | 71       | 243         | 75<br>82  | 96         | 105        | 134        | 434        | 80              | 102                 | 0.43         | 1.36              |
| 31966.110              | 8.52         | 123        | 234        | 71       | 243         | 82<br>82  | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.111              | 8.52         | 123        | 234        | 71       | 243         | 82        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.113              | 8.52         | 123        | 234        | 71       | 243         | 82        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.114              | 8.52         | 123        | 234        | 71       | 243         | 82        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.115              | 8.15         | 120        | 226        | 68       | 237         | 78        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.116              | 8.15         | 120        | 226        | 68       | 237         | 78        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.117              | 8.15         | 120        | 226        | 68       | 237         | 78        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.118              | 8.15         | 120        | 226        | 68       | 237         | 78        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.119              | 8.15         | 120        | 226        | 68       | 237         | 78        | 96         | 105        | 134        | 429        | 80              | 102                 | 0.43         | 1.36              |
| 31966.120              | 8.46         | 125        | 230        | 73       | 239         | 84        | 103        | 111        | 137        | 431        | 80              | 102                 | 0.43         | 1.36              |

<sup>\*</sup>All Values are MARV.



Sales Office: Engineered Synthetics Products Inc. Phone: (770) 564-1857

Fax: (770) 564-1818

Date: May 1<sup>st</sup>, 2017

Republic Waste Services Bridgeton Landfill - Phase 1A and 1B Cover

PO#: PO6472936

**SUBJECT: Annual UV Resistance Testing for SKAPS Industries Products** 

To whom it may concern,

This letter is to inform that SKAPS Industries certifies UV Resistance based on third party testing annually. SKAPS Industries certifies its products to retain at least 70% of its strength after being exposed to direct UV for five-hundred (500) hours (ASTM D 4355). SKAPS Industries nonwoven geotextiles are composed of one-hundred percent virgin raw polypropylene material. Therefore, all GT and GE products are composed of identical raw polypropylene fibers.

Attached to this document is the third party annual testing result for UV Resistance performed in 2017 for SKAPS Industries' GT131. SKAPS Industries' GE160 and GE180 supplied are heavier and thicker fabrics, therefore, will retain a greater amount of strength after exposed in the UV Resistance chamber in comparison to SKAPS GT131. SKAPS Industries certifies that the GE160 and GE180 supplied to this project will meet or exceed the requirements of UV Resistance.

Please feel free to contact SKAPS Industries if you have any questions.

Regards,

Kourosh Sabzevari

**Quality Control Manager** 

<= Same

2/15/2017

Mail To: Bill To:

Kourosh R. Sabzevari SKAPS Industries

335 Athena Drive Athens, Georgia 30601

email: kourosh@skaps.com email: anurag@skaps.com

Dear Mr. Sabzevari:

Thank you for consulting TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report of the laboratory testing for the sample(s) listed below.

Project: Third Party Testing - GT131 UV Resistance

TRI Job Reference Number: 26543

Material(s) Tested: One, Skaps GT 131 Geotextile

Test(s) Requested: UV Resistance (ASTM D 4355)

If you have any questions or require any additional information, please call us at 1-800-880-8378

Sincerely,

Mansukh Patel Laboratory Manager Geosynthetic Services Division www.GeosyntheticTesting.com

\*Signature is on file

# GEOTEXTILE TEST RESULTS TRI Client: SKAPS Industries Project: Third Party Testing - GT131 UV Resistance

Material: Skaps GT 131 Geotextile Sample Identification: GT131

TRI Log #: 26543

| PARAMETER                            | TEST RE       | PLICATE I | NUMBER |     |      |   |   |   |   |    | MEAN | STD.<br>DEV. | PROJ.<br>SPEC. |
|--------------------------------------|---------------|-----------|--------|-----|------|---|---|---|---|----|------|--------------|----------------|
|                                      | 1             | 2         | 3      | 4   | 5    | 6 | 7 | 8 | 9 | 10 |      |              |                |
| JV Resistance (ASTM D 4355)          |               |           |        |     |      |   |   |   |   |    |      |              |                |
| Strength Retained measured via strip | tensile (ASTN | 1 D 5035) |        |     |      |   |   |   |   |    |      |              | PERCEN'        |
|                                      |               |           |        |     |      |   |   |   |   |    |      |              | RETAINE        |
| MD - Tensile Strength (lbs) - B      | 80            | 97        | 101    | 97  | 101  |   |   |   |   |    | 95   | 9            | 9.15           |
| MD - Tensile Strength (ppi) - B      | 40            | 49        | 51     | 49  | 51   |   |   |   |   |    | 48   | 4            |                |
| MD - Tensile Strength (N) - B        | 356           | 432       | 449    | 432 | 449  |   |   |   |   |    | 424  | 39           |                |
| MD - Tensile Strength (kN/m) - B     | 7.0           | 8.5       | 8.8    | 8.5 | 8.8  |   |   |   |   |    | 8.3  | 8.0          |                |
| MD - Tensile Strength (lbs) - E      | 80            | 69        | 95     | 95  | 72   |   |   |   |   |    | 82   | 12           | 15.03          |
| MD - Tensile Strength (ppi) - E      | 40            | 35        | 48     | 48  | 36   |   |   |   |   |    | 41   | 6            |                |
| MD - Tensile Strength (N) - E        | 356           | 307       | 423    | 423 | 320  |   |   |   |   |    | 366  | 55           |                |
| MD - Tensile Strength (kN/m) - E     | 7.0           | 6.0       | 8.3    | 8.3 | 6.3  |   |   |   |   |    | 7.2  | 1.1          | 86             |
| D - Tensile Strength (lbs) - B       | 105           | 123       | 100    | 113 | 116  |   |   |   |   |    | 111  | 9            | 8.14           |
| ΓD - Tensile Strength (ppi) - B      | 53            | 62        | 50     | 57  | 58   |   |   |   |   |    | 56   | 5            |                |
| TD - Tensile Strength (N) - B        | 467           | 547       | 445    | 503 | 516  |   |   |   |   |    | 496  | 40           |                |
| TD - Tensile Strength (kN/m) - B     | 9.2           | 10.8      | 8.8    | 9.9 | 10.2 |   |   |   |   |    | 9.8  | 8.0          |                |
| ΓD - Tensile Strength (lbs) - E      | 104           | 88        | 101    | 100 | 86   |   |   |   |   |    | 96   | 8            | 8.56           |
| D - Tensile Strength (ppi) - E       | 52            | 44        | 51     | 50  | 43   |   |   |   |   |    | 48   | 4            |                |
| ΓD - Tensile Strength (N) - E        | 463           | 392       | 449    | 445 | 383  |   |   |   |   |    | 426  | 36           |                |
| ΓD - Tensile Strength (kN/m) - E     | 9.1           | 7.7       | 8.8    | 8.8 | 7.5  |   |   |   |   |    | 8.4  | 0.7          | 86             |
| MD - Elong. @ Max. Load (%) - B      | 69            | 72        | 69     | 69  | 74   |   |   |   |   |    | 71   | 2            |                |
| MD - Elong. @ Max. Load (%) - E      | 63            | 43        | 67     | 62  | 57   |   |   |   |   |    | 58   | 9            | 83             |
| TD - Elong. @ Max. Load (%) - B      | 86            | 91        | 85     | 87  | 89   |   |   |   |   |    | 88   | 2            |                |
| FD - Elong. @ Max. Load (%) - E      | 72            | 65        | 77     | 73  | 65   |   |   |   |   |    | 70   | 5            | 80             |
| 3 - Baseline Unexposed               |               |           |        |     |      |   |   |   |   |    |      |              |                |
| E - Exposed for 500 hours of ASTM D  | 4355 Cycle    |           |        |     |      |   |   |   |   |    |      |              |                |

MD Machine Direction

TD Transverse Direction

<= Same (P.O. # BT-125)

May 15, 2017

Mail To: Bill To:

Brad Vits Feezor Engineering Inc.

406 East Walnut Chatham, IL 62258

email: bvits@feezorengineering.com

Dear Mr. Vits:

Thank you for consulting TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report of the laboratory testing for the sample(s) listed below.

Project: North Quarry Phase 1 EVOH Cover

TRI Job Reference Number: 28750

Material(s) Tested: One, SKAPS 6 oz Nonwoven Geotextile(s)

Test(s) Requested: CBR Puncture Strength (ASTM D 6241)

If you have any questions or require any additional information, please call us at 1-800-880-8378

Sincerely,

Mansukh Patel Laboratory Manager

Geosynthetic Services Division www.GeosyntheticTesting.com

\*Signature is on file

# GEOTEXTILE TEST RESULTS TRI Client: Feezor Engineering Inc. Project: North Quarry Phase 1 EVOH Cover

Material: SKAPS 6 oz Nonwoven Geotextile

Sample Identification: 45619.28

TRI Log #: 28750

| D4D445TED                     | TEAT DE                             |     |     |     |     |     |     |     |     |     |      | STD. |
|-------------------------------|-------------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|
| PARAMETER                     | TEST REPLICATE NUMBER               |     |     |     |     |     |     |     |     |     | MEAN | DEV. |
|                               | 1                                   | 2   | 3   | 4   | 5   | 6   | 7   | 8   | 9   | 10  |      |      |
| CBR Puncture Strength (ASTM I | CBR Puncture Strength (ASTM D 6241) |     |     |     |     |     |     |     |     |     |      |      |
| Puncture Resistance (lbs)     | 587                                 | 476 | 560 | 561 | 377 | 521 | 575 | 595 | 542 | 611 | 541  | 69   |

## **Sub-Appendix B.3**

## **Geocomposite Manufacturer's Quality Control Data**



December 27, 2016 Republic Waste Services

Ref.: RWS Bridgeton Landfill, MO

Customer P.O. # Product : TN 220-2-6

We hereby certify that the TN 220-2-6 drainage geocomposite, meets or exceeds the project requirements as stated in the specifications. The properties listed in this section are:

| Property                        | Test Method              | Unit                | Value                  | Qualifier         |
|---------------------------------|--------------------------|---------------------|------------------------|-------------------|
| Geonet <sup>3</sup>             |                          |                     |                        |                   |
| Thickness                       | ASTM D 5199              | mil                 | 200                    | MAV <sup>6</sup>  |
| Carbon Black                    | ASTM D 4218              | %                   | 2.0                    | MAV               |
| Tensile Strength                | ASTM D 7179              | lbs/in              | 45                     | MAV               |
| Melt Flow                       | ASTM D 1238 <sup>2</sup> | g/10 min            | 1.0                    | Maximum           |
| Density                         | ASTM D 1505              | g/cm <sup>3</sup>   | 0.94                   | MAV               |
| Transmissivity <sup>1a</sup>    | ASTM D 4716              | m²/sec              | 2.0 x 10 <sup>-3</sup> | MAV               |
| Composite                       |                          |                     |                        |                   |
| Ply Adhesion                    | ASTM D 7005              | lb/in               | 1.0                    | MAV               |
| Transmissivity <sup>1b</sup>    | ASTM D 4716              | m <sup>2</sup> /sec | 1.0 x 10 <sup>-4</sup> | MAV               |
| Geotextile <sup>3 &amp; 4</sup> |                          |                     |                        |                   |
| Fabric Weight                   | ASTM D 5261              | oz/yd <sup>2</sup>  | 6.0                    | MARV <sup>5</sup> |
| Grab Strength                   | ASTM D 4632              | lbs                 | 160                    | MARV              |
| Grab Elongation                 | ASTM D 4632              | %                   | 50                     | MARV              |
| Trap Tear Strength              | ASTM D 4533              | lbs                 | 65                     | MARV              |
| CBR Puncture                    | ASTM D 6241              | lbs                 | 450                    | MARV              |
| Permittivity                    | ASTM D 4491              | sec <sup>-1</sup>   | 1.63                   | MARV              |
| Permeability                    | ASTM D 4491              | cm/sec              | 0.30                   | MARV              |
| AOS                             | ASTM D 4751              | US Sieve            | 70                     | MaxARV            |
| UV Resistance                   | ASTM D 4355              | %/hrs               | 70/500                 | MARV              |

### **Notes:**

- 1a. Transmissivity measured using water at  $21 \pm 2$  °C (70  $\pm 4$  °F) with a gradient of 0.1 and a confining pressure of 10,000 psf between steel plates after 15 minutes.
- 1b. Transmissivity measured using water at  $21 \pm 2$  °C ( $70 \pm 4$  °F) with a gradient of 0.1 and a confining pressure of 10,000 psf between steel plates after 15 minutes.
- 2. Condition 190/2.16
- 3. Geotextile and Geonet properties are prior to lamination.
- 4. Geotextile data is provided by the supplier.
- 5. MARV is statistically defined as mean minus two standard deviations and it is the value which is exceeded by 97.5% of all the test data.
- 6. Minium average value

Sincerely,
Rajesh Patel

Rajesh Patel QA Manager



**Product: TN 220-2-6** 

**Project:** RWS Bridgeton Landfill, MO

We hereby certify the following test results for the above referenced product/project :

|             | Geoco                   | mposite  |                         | Geonet              |                    |                     |                 |                           |                         |  |  |
|-------------|-------------------------|----------|-------------------------|---------------------|--------------------|---------------------|-----------------|---------------------------|-------------------------|--|--|
| Roll Number | Ply Adhesion<br>(lb/in) |          | Transmissivity (m²/sec) | Resin Lot<br>Number | Density<br>(g/cm³) | Thickness<br>(mils) | Carbon<br>Black | Tensile<br>Strength<br>MD | Transmissivity (m²/sec) |  |  |
|             | Side "A"                | Side "B" |                         |                     |                    |                     | (%)             | (lb/in)                   |                         |  |  |
| 73681010001 | 1.86                    | 2.33     | 3.03 x 10 <sup>-4</sup> | SHOX 004234         | 0.9531             | 224                 | 2.28            | 59                        | 3.31 x 10 <sup>-3</sup> |  |  |
| 73681010002 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010003 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010004 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010005 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010006 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010007 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010008 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010009 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010010 | 2.21                    | 1.67     |                         | SHOX 004234         | 0.9531             | 227                 | 2.22            | 52                        |                         |  |  |
| 73681010011 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010012 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010013 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010014 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010015 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010016 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010017 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010018 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010019 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010020 | 1.50                    | 1.84     |                         | SHOX 004234         | 0.9531             | 223                 | 2.51            | 56                        |                         |  |  |
| 73681010021 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010022 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010023 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |
| 73681010024 |                         |          |                         | SHOX 004234         | 0.9531             |                     |                 |                           |                         |  |  |



**Product: TN 220-2-6** 

**Project: RWS Bridgeton Landfill, MO** 

We hereby certify the following test results for the above referenced product/project :

|             | Geoco                                   | mposite |             | Geonet      |                            |                     |                    |                     |                 |                           |                                      |
|-------------|---|---------|-------------|-------------|----------------------------|---------------------|--------------------|---------------------|-----------------|---------------------------|--------------------------------------|
| Roll Number | Ply Adhesion (lb/in)  Side "A" Side "B" |         | -           |             | Transmissivity<br>(m²/sec) | Resin Lot<br>Number | Density<br>(g/cm³) | Thickness<br>(mils) | Carbon<br>Black | Tensile<br>Strength<br>MD | Transmissivity (m <sup>2</sup> /sec) |
|             |   |         | (III / Sec) | ramber      | (g/ciii )                  | (111113)            | (%)                | (lb/in)             | (III / Sec)     |                           |                                      |
| 73681010025 |   |         |             | SHOX 004234 | 0.9531                     |                     |                    |                     |                 |                           |                                      |
| 73681010026 |   |         | SHOX 004234 | 0.9531      |                            |                     |                    |                     |                 |                           |                                      |
| 73681010027 |   |         |             | SHOX 004234 | 0.9531                     |                     |                    |                     |                 |                           |                                      |



## POLYETHYLENE RESIN CERTIFICATION

Customer Name :Republic Waste ServicesProject Name :RWS Bridgeton Landfill, MO

**Geocomposite Manufacturer :** SKAPS Industries **Geocomposite Production Plant :** Commerce, GA **Geocomposite Brand Name :** TN 220-2-6

We hereby certify the following test results for the above referenced product/project:

| Resin<br>Manufacturer | Resin<br>Lot Number | Property        | Test<br>Method            | Units             | Resin<br>Manufacturer<br>Value | Tested<br>Value* |
|-----------------------|---------------------|-----------------|---------------------------|-------------------|--------------------------------|------------------|
| Osterman and Company  | SHOX 004234         | Density         | ASTM D1505                | g/cm <sup>3</sup> | 0.9480                         | 0.9482           |
| Osterman and Company  | 31107 004234        | Melt flow Index | ASTM D1238 <sup>(a)</sup> | g/10 min          | 0.11                           | 0.14             |

(a) Condition 190/2.16

<sup>\*</sup> Data from SKAPS Quality Control



## **Geotextile Certification**

**Product: TN 220-2-6** 

Project: RWS Bridgeton Landfill, MO

We hereby certify the following test results for the above referenced product/project :

| GEOCOMP<br>ROLL# | FABRIC<br>SIDE | WEIGHT oz/yd² | GRAB<br>lbs.<br>(MD) | GRAB<br>ELG %<br>(MD) | GRAB<br>lbs.<br>(XMD) | GRAB<br>ELG %<br>(XMD) | TRAP<br>lbs.<br>(MD) | TRAP<br>lbs.<br>(XMD) | CBR<br>PUNCTURE<br>Ibs | AOS<br>us sieve | PERM-ABL<br>cm/sec | PERM-ITY<br>sec <sup>-1</sup> |
|------------------|----------------|---------------|----------------------|-----------------------|-----------------------|------------------------|----------------------|-----------------------|------------------------|-----------------|--------------------|-------------------------------|
| 73681010001      | Side A         | 6.31          | 160                  | 74                    | 173                   | 84                     | 71                   | 87                    | 465                    | 70              | 0.52               | 1.82                          |
| 73081010001      | Side B         | 6.60          | 162                  | 69                    | 179                   | 82                     | 80                   | 84                    | 462                    | 70              | 0.52               | 1.82                          |
| 73681010020      | Side A         | 6.31          | 160                  | 74                    | 173                   | 84                     | 71                   | 87                    | 465                    | 70              | 0.52               | 1.82                          |
| 75001010020      | Side B         | 6.67          | 168                  | 72                    | 177                   | 80                     | 75                   | 80                    | 477                    | 70              | 0.52               | 1.82                          |

Product GE 160 Project: RWS Bridgeton Landfill, MO

| GT ROLL#<br>ASTM METHOD | WEIGHT*<br>D5261 | MD GRAB<br>D4632 | MD ELONG<br>D4632 | XMD GRAB<br>D4632 | XMD ELONG<br>D4632 | MD TRAP<br>D4533 | XMD TRAP<br>D4533 | CBR PUNCTURE<br>D6241 | AOS<br>D4751 | PERMEABILITY<br>D4491 | PERMITTIVITY<br>D4491 |
|-------------------------|------------------|------------------|-------------------|-------------------|--------------------|------------------|-------------------|-----------------------|--------------|-----------------------|-----------------------|
| UNITS                   | oz/sq yd         | lbs.             | %                 | lbs               | %                  | lbs.             | lbs               | lbs.                  | US Sieve     | cm/sec                | sec <sup>-1</sup>     |
| 7368.001                | 6.31             | 160              | 74                | 173               | 84                 | 71               | 87                | 465                   | 70           | 0.52                  | 1.82                  |
| 7368.002                | 6.31             | 160              | 74                | 173               | 84                 | 71               | 87                | 465                   | 70           | 0.52                  | 1.82                  |
| ু 7368.003              | 6.31             | 160              | 74                | 173               | 84                 | 71               | 87                | 465                   | 70           | 0.52                  | 1.82                  |
| 7368.004                | 6.60             | 162              | 69                | 179               | 82                 | 80               | 84                | 462                   | 70           | 0.52                  | 1.82                  |
| 7368.005                | 6.60             | 162              | 69                | 179               | 82                 | 80               | 84                | 462                   | 70           | 0.52                  | 1.82                  |
| 7368.006                | 6.60             | 162              | 69                | 179               | 82                 | 80               | 84                | 462                   | 70           | 0.52                  | 1.82                  |
| 7368.007                | 6.60             | 162              | 69                | 179               | 82                 | 80               | 84                | 462                   | 70           | 0.52                  | 1.82                  |
| 7368.008                | 6.67             | 168              | 72                | 177               | 80                 | 75               | 80                | 477                   | 70           | 0.52                  | 1.82                  |
| 7368.009                | 6.67             | 168              | 72                | 177               | 80                 | 75               | 80                | 477                   | 70           | 0.52                  | 1.82                  |
| 7368.010                | 6.67             | 168              | 72                | 177               | 80                 | 75               | 80                | 477                   | 70           | 0.52                  | 1.82                  |

| Geocomposite - Side A | Geotextile - Side A | Geocomposite - Side B | Geotextile - Side B |
|-----------------------|---------------------|-----------------------|---------------------|
| 73681010001           | 7368.003            | 73681010001           | 7368.006            |
| 73681010007           | 7368.008            | 73681010007           | 7368.002            |
| 73681010013           | 7368.005            | 73681010013           | 7368.004            |
| 73681010019           | 7368.001            | 73681010019           | 7368.009            |
| 73681010025           | 7368.010            | 73681010025           | 7368.007            |



March 29, 2017 Republic Waste Services

Ref.: RWS Bridgeton Landfill, MO Customer P.O. # PO6472936

**Product: TN 220-2-6** 

We hereby certify that the TN 220-2-6 drainage geocomposite, meets or exceeds the project requirements as stated in the specifications. The properties listed in this section are:

| Property                        | Test Method              | Unit                | Value                  | Qualifier         |
|---------------------------------|--------------------------|---------------------|------------------------|-------------------|
| Geonet <sup>3</sup>             |                          |                     |                        |                   |
| Thickness                       | ASTM D 5199              | mil                 | 200                    | MAV <sup>6</sup>  |
| Carbon Black                    | ASTM D 4218              | %                   | 2.0                    | MAV               |
| Tensile Strength                | ASTM D 7179              | lbs/in              | 45                     | MAV               |
| Melt Flow                       | ASTM D 1238 <sup>2</sup> | g/10 min            | 1.0                    | Maximum           |
| Density                         | ASTM D 1505              | g/cm <sup>3</sup>   | 0.94                   | MAV               |
| Transmissivity <sup>1a</sup>    | ASTM D 4716              | m <sup>2</sup> /sec | 2.0 x 10 <sup>-3</sup> | MAV               |
| Composite                       |                          |                     |                        |                   |
| Ply Adhesion                    | ASTM D 7005              | lb/in               | 1.0                    | MAV               |
| Transmissivity <sup>1b</sup>    | ASTM D 4716              | m <sup>2</sup> /sec | 1.0 x 10 <sup>-4</sup> | MAV               |
| Geotextile <sup>3 &amp; 4</sup> |                          |                     |                        |                   |
| Fabric Weight                   | ASTM D 5261              | oz/yd <sup>2</sup>  | 6.0                    | MARV <sup>5</sup> |
| Grab Strength                   | ASTM D 4632              | lbs                 | 160                    | MARV              |
| Grab Elongation                 | ASTM D 4632              | %                   | 50                     | MARV              |
| Trap Tear Strength              | ASTM D 4533              | lbs                 | 65                     | MARV              |
| CBR Puncture                    | ASTM D 6241              | lbs                 | 450                    | MARV              |
| Permittivity                    | ASTM D 4491              | sec <sup>-1</sup>   | 1.63                   | MARV              |
| Permeability                    | ASTM D 4491              | cm/sec              | 0.30                   | MARV              |
| AOS                             | ASTM D 4751              | US Sieve            | 70                     | MaxARV            |
| UV Resistance                   | ASTM D 4355              | %/hrs               | 70/500                 | MARV              |

#### **Notes:**

- 1a. Transmissivity measured using water at  $21 \pm 2$  °C (70  $\pm 4$  °F) with a gradient of 0.1 and a confining pressure of 10,000 psf between steel plates after 15 minutes.
- 1b. Transmissivity measured using water at  $21 \pm 2$  °C ( $70 \pm 4$  °F) with a gradient of 0.1 and a confining pressure of 10,000 psf between steel plates after 15 minutes.
- 2. Condition 190/2.16
- 3. Geotextile and Geonet properties are prior to lamination.
- 4. Geotextile data is provided by the supplier.
- 5. MARV is statistically defined as mean minus two standard deviations and it is the value which is exceeded by 97.5% of all the test data.
- 6. Minium average value

Sincerely,
Rajesh Patel

Rajesh Patel QA Manager



**Product: TN 220-2-6** 

**Project:** RWS Bridgeton Landfill, MO

We hereby certify the following test results for the above referenced product/project :

|             | Geoco                   | mposite  |                         | Geonet              |                    |                     |                 |                           |                                      |  |  |  |
|-------------|-------------------------|----------|-------------------------|---------------------|--------------------|---------------------|-----------------|---------------------------|--------------------------------------|--|--|--|
| Roll Number | Ply Adhesion<br>(lb/in) |          | Transmissivity (m²/sec) | Resin Lot<br>Number | Density<br>(g/cm³) | Thickness<br>(mils) | Carbon<br>Black | Tensile<br>Strength<br>MD | Transmissivity (m <sup>2</sup> /sec) |  |  |  |
|             | Side "A"                | Side "B" | (III / Sec)             | Number              | (g/cm/)            | (111113)            | (%)             | (lb/in)                   | (III / Sec)                          |  |  |  |
| 74881010001 | 1.49                    | 1.96     | 3.02 x 10 <sup>-4</sup> | NAHX 610271         | 0.9511             | 228                 | 2.27            | 59                        | 3.07 x 10 <sup>-3</sup>              |  |  |  |
| 74881010002 |                         |          |                         | NAHX 610271         | 0.9511             |                     |                 |                           |                                      |  |  |  |
| 74881010003 |                         |          |                         | NAHX 610271         | 0.9511             |                     |                 |                           |                                      |  |  |  |



#### POLYETHYLENE RESIN CERTIFICATION

Customer Name :Republic Waste ServicesProject Name :RWS Bridgeton Landfill, MO

**Geocomposite Manufacturer :** SKAPS Industries **Geocomposite Production Plant :** Commerce, GA **Geocomposite Brand Name :** TN 220-2-6

We hereby certify the following test results for the above referenced product/project:

| Resin<br>Manufacturer | Resin<br>Lot Number | Property        | Test<br>Method            | Units             | Resin<br>Manufacturer<br>Value | Tested<br>Value* |
|-----------------------|---------------------|-----------------|---------------------------|-------------------|--------------------------------|------------------|
| Chevron Phillips      | NAHX 610271         | Density         | ASTM D1505                | g/cm <sup>3</sup> | 0.9460                         | 0.9463           |
| Chemical Company      | NALIA 0102/1        | Melt flow Index | ASTM D1238 <sup>(a)</sup> | g/10 min          | 0.16                           | 0.17             |

(a) Condition 190/2.16

<sup>\*</sup> Data from SKAPS Quality Control



## **Geotextile Certification**

**Product:** TN 220-2-6

Project: RWS Bridgeton Landfill, MO

We hereby certify the following test results for the above referenced product/project :

| GEOCOMP<br>ROLL# | FABRIC<br>SIDE | WEIGHT oz/yd <sup>2</sup> | GRAB<br>Ibs.<br>(MD) | GRAB<br>ELG %<br>(MD) | GRAB<br>Ibs.<br>(XMD) | GRAB<br>ELG %<br>(XMD) | TRAP<br>lbs.<br>(MD) | TRAP<br>lbs.<br>(XMD) | CBR<br>PUNCTURE<br>Ibs | AOS<br>us sieve | PERM-ABL<br>cm/sec | PERM-ITY<br>sec <sup>-1</sup> |
|------------------|----------------|---------------------------|----------------------|-----------------------|-----------------------|------------------------|----------------------|-----------------------|------------------------|-----------------|--------------------|-------------------------------|
| 74881010001      | Side A         | 6.62                      | 169                  | 65                    | 177                   | 84                     | 77                   | 81                    | 496                    | 70              | 0.50               | 1.79                          |
| 74001010001      | Side B         | 6.62                      | 169                  | 65                    | 177                   | 84                     | 77                   | 81                    | 496                    | 70              | 0.50               | 1.79                          |



June 29, 2017 Republic Waste Services

Ref.: RWS Bridgeton Landfill, MO Customer P.O. # PO6666316

**Product: TN 220-2-6** 

We hereby certify that the TN 220-2-6 drainage geocomposite, meets or exceeds the project requirements as stated in the specifications. The properties listed in this section are:

| Property                        | Test Method              | Unit                | Value                  | Qualifier         |
|---------------------------------|--------------------------|---------------------|------------------------|-------------------|
| Geonet <sup>3</sup>             |                          |                     |                        |                   |
| Thickness                       | ASTM D 5199              | mil                 | 200                    | MAV <sup>6</sup>  |
| Carbon Black                    | ASTM D 4218              | %                   | 2.0                    | MAV               |
| Tensile Strength                | ASTM D 7179              | lbs/in              | 45                     | MAV               |
| Melt Flow                       | ASTM D 1238 <sup>2</sup> | g/10 min            | 1.0                    | Maximum           |
| Density                         | ASTM D 1505              | g/cm <sup>3</sup>   | 0.94                   | MAV               |
| Transmissivity <sup>1a</sup>    | ASTM D 4716              | m <sup>2</sup> /sec | 2.0 x 10 <sup>-3</sup> | MAV               |
| Composite                       |                          |                     |                        |                   |
| Ply Adhesion                    | ASTM D 7005              | lb/in               | 1.0                    | MAV               |
| Transmissivity <sup>1b</sup>    | ASTM D 4716              | m <sup>2</sup> /sec | 1.0 x 10 <sup>-4</sup> | MAV               |
| Geotextile <sup>3 &amp; 4</sup> |                          |                     |                        |                   |
| Fabric Weight                   | ASTM D 5261              | oz/yd <sup>2</sup>  | 6.0                    | MARV <sup>5</sup> |
| Grab Strength                   | ASTM D 4632              | lbs                 | 160                    | MARV              |
| Grab Elongation                 | ASTM D 4632              | %                   | 50                     | MARV              |
| Trap Tear Strength              | ASTM D 4533              | lbs                 | 65                     | MARV              |
| CBR Puncture                    | ASTM D 6241              | lbs                 | 450                    | MARV              |
| Permittivity                    | ASTM D 4491              | sec <sup>-1</sup>   | 1.63                   | MARV              |
| Permeability                    | ASTM D 4491              | cm/sec              | 0.30                   | MARV              |
| AOS                             | ASTM D 4751              | US Sieve            | 70                     | MaxARV            |
| UV Resistance                   | ASTM D 4355              | %/hrs               | 70/500                 | MARV              |

#### **Notes:**

- 1a. Transmissivity measured using water at  $21 \pm 2$  °C ( $70 \pm 4$  °F) with a gradient of 0.1 and a confining pressure of 10,000 psf between steel plates after 15 minutes.
- 1b. Transmissivity measured using water at  $21 \pm 2$  °C ( $70 \pm 4$  °F) with a gradient of 0.1 and a confining pressure of 10,000 psf between steel plates after 15 minutes.
- 2. Condition 190/2.16
- 3. Geotextile and Geonet properties are prior to lamination.
- 4. Geotextile data is provided by the supplier.
- 5. MARV is statistically defined as mean minus two standard deviations and it is the value which is exceeded by 97.5% of all the test data.
- 6. Minium average value

Sincerely,
Rajesh Patel

Rajesh Patel QA Manager



**Product: TN 220-2-6** 

Project: RWS Bridgeton Landfill, MO

We hereby certify the following test results for the above referenced product/project :

|             | Geoco    | mposite        |                         |                     |                    | Geo                 | net             |                           |                                      |
|-------------|----------|----------------|-------------------------|---------------------|--------------------|---------------------|-----------------|---------------------------|--------------------------------------|
| Roll Number | _        | hesion<br>/in) | Transmissivity (m²/sec) | Resin Lot<br>Number | Density<br>(g/cm³) | Thickness<br>(mils) | Carbon<br>Black | Tensile<br>Strength<br>MD | Transmissivity (m <sup>2</sup> /sec) |
|             | Side "A" | Side "B"       | (iii /see)              |                     | (g/ciii /          | ()                  | (%)             | (lb/in)                   | (iii / see)                          |
| 76911010001 | 1.64     | 1.97           | 2.78 x 10 <sup>-4</sup> | AMCX 004619         | 0.9526             | 222                 | 2.65            | 54                        | 2.65 x 10 <sup>-3</sup>              |
| 76911010002 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010003 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010004 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010005 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010006 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010007 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010008 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010009 |          |                |                         | AMCX 004619         | 0.9526             |                     |                 |                           |                                      |
| 76911010010 | 2.14     | 1.76           |                         | AMCX 004619         | 0.9526             | 221                 | 2.63            | 58                        |                                      |



#### POLYETHYLENE RESIN CERTIFICATION

Customer Name :Republic Waste ServicesProject Name :RWS Bridgeton Landfill, MO

**Geocomposite Manufacturer :** SKAPS Industries **Geocomposite Production Plant :** Commerce, GA **Geocomposite Brand Name :** TN 220-2-6

We hereby certify the following test results for the above referenced product/project:

| Resin<br>Manufacturer | Resin<br>Lot Number | Property        | Test<br>Method            | Units             | Resin<br>Manufacturer<br>Value | Tested<br>Value* |
|-----------------------|---------------------|-----------------|---------------------------|-------------------|--------------------------------|------------------|
| INEOS USA             | AMCX 004619         | Density         | ASTM D1505                | g/cm <sup>3</sup> | 0.9480                         | 0.9478           |
| INLOS OSA             | AMCX 004019         | Melt flow Index | ASTM D1238 <sup>(a)</sup> | g/10 min          | 0.27                           | 0.29             |

(a) Condition 190/2.16

<sup>\*</sup> Data from SKAPS Quality Control



## **Geotextile Certification**

**Product:** TN 220-2-6

Project: RWS Bridgeton Landfill, MO

We hereby certify the following test results for the above referenced product/project :

| GEOCOMP<br>ROLL# | FABRIC<br>SIDE | WEIGHT oz/yd² | GRAB<br>lbs.<br>(MD) | GRAB<br>ELG %<br>(MD) | GRAB<br>Ibs.<br>(XMD) | GRAB<br>ELG %<br>(XMD) | TRAP<br>lbs.<br>(MD) | TRAP<br>lbs.<br>(XMD) | CBR<br>PUNCTURE<br>Ibs | AOS<br>us sieve | PERM-ABL<br>cm/sec | PERM-ITY<br>sec <sup>-1</sup> |
|------------------|----------------|---------------|----------------------|-----------------------|-----------------------|------------------------|----------------------|-----------------------|------------------------|-----------------|--------------------|-------------------------------|
| 76911010001      | Side A         | 6.27          | 162                  | 75                    | 174                   | 80                     | 71                   | 84                    | 488                    | 70              | 0.51               | 1.81                          |
| 70911010001      | Side B         | 6.39          | 163                  | 67                    | 172                   | 77                     | 78                   | 81                    | 499                    | 70              | 0.51               | 1.81                          |



Sales Office: Engineered Synthetics Products Inc. Phone: (770) 564-1857

Fax: (770) 564-1818

Date: May 1<sup>st</sup>, 2017

Republic Waste Services Bridgeton Landfill - Phase 1A and 1B Cover

PO#: PO6472936

**SUBJECT: Annual UV Resistance Testing for SKAPS Industries Products** 

To whom it may concern,

This letter is to inform that SKAPS Industries certifies UV Resistance based on third party testing annually. SKAPS Industries certifies its products to retain at least 70% of its strength after being exposed to direct UV for five-hundred (500) hours (ASTM D 4355). SKAPS Industries nonwoven geotextiles are composed of one-hundred percent virgin raw polypropylene material. Therefore, all GT and GE products are composed of identical raw polypropylene fibers.

Attached to this document is the third party annual testing result for UV Resistance performed in 2017 for SKAPS Industries' GT131. SKAPS Industries' GE160 and GE180 supplied are heavier and thicker fabrics, therefore, will retain a greater amount of strength after exposed in the UV Resistance chamber in comparison to SKAPS GT131. SKAPS Industries certifies that the GE160 and GE180 supplied to this project will meet or exceed the requirements of UV Resistance.

Please feel free to contact SKAPS Industries if you have any questions.

Regards,

Kourosh Sabzevari

**Quality Control Manager** 

<= Same

2/15/2017

Mail To: Bill To:

Kourosh R. Sabzevari SKAPS Industries 335 Athena Drive

Athens, Georgia 30601

email: kourosh@skaps.com email: anurag@skaps.com

Dear Mr. Sabzevari:

Thank you for consulting TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report of the laboratory testing for the sample(s) listed below.

Project: Third Party Testing - GT131 UV Resistance

TRI Job Reference Number: 26543

Material(s) Tested: One, Skaps GT 131 Geotextile

Test(s) Requested: UV Resistance (ASTM D 4355)

If you have any questions or require any additional information, please call us at 1-800-880-8378

Sincerely,

Mansukh Patel Laboratory Manager Geosynthetic Services Division www.GeosyntheticTesting.com

\*Signature is on file

# GEOTEXTILE TEST RESULTS TRI Client: SKAPS Industries Project: Third Party Testing - GT131 UV Resistance

Material: Skaps GT 131 Geotextile Sample Identification: GT131

TRI Log #: 26543

| PARAMETER                            | TEST RE       | PLICATE N | NUMBER |     |      |   |   |   |   |    | MEAN | STD.<br>DEV. | PROJ.<br>SPEC. |
|--------------------------------------|---------------|-----------|--------|-----|------|---|---|---|---|----|------|--------------|----------------|
|                                      | 1             | 2         | 3      | 4   | 5    | 6 | 7 | 8 | 9 | 10 |      |              |                |
| JV Resistance (ASTM D 4355)          |               |           |        |     |      |   |   |   |   |    |      |              |                |
| Strength Retained measured via strip | tensile (ASTN | 1 D 5035) |        |     |      |   |   |   |   |    |      |              | PERCEN'        |
|                                      |               |           |        |     |      |   |   |   |   |    |      |              | RETAINE        |
| MD - Tensile Strength (lbs) - B      | 80            | 97        | 101    | 97  | 101  |   |   |   |   |    | 95   | 9            | 9.15           |
| MD - Tensile Strength (ppi) - B      | 40            | 49        | 51     | 49  | 51   |   |   |   |   |    | 48   | 4            |                |
| MD - Tensile Strength (N) - B        | 356           | 432       | 449    | 432 | 449  |   |   |   |   |    | 424  | 39           |                |
| MD - Tensile Strength (kN/m) - B     | 7.0           | 8.5       | 8.8    | 8.5 | 8.8  |   |   |   |   |    | 8.3  | 8.0          |                |
| MD - Tensile Strength (lbs) - E      | 80            | 69        | 95     | 95  | 72   |   |   |   |   |    | 82   | 12           | 15.03          |
| MD - Tensile Strength (ppi) - E      | 40            | 35        | 48     | 48  | 36   |   |   |   |   |    | 41   | 6            |                |
| MD - Tensile Strength (N) - E        | 356           | 307       | 423    | 423 | 320  |   |   |   |   |    | 366  | 55           |                |
| MD - Tensile Strength (kN/m) - E     | 7.0           | 6.0       | 8.3    | 8.3 | 6.3  |   |   |   |   |    | 7.2  | 1.1          | 86             |
| D - Tensile Strength (lbs) - B       | 105           | 123       | 100    | 113 | 116  |   |   |   |   |    | 111  | 9            | 8.14           |
| ΓD - Tensile Strength (ppi) - B      | 53            | 62        | 50     | 57  | 58   |   |   |   |   |    | 56   | 5            |                |
| TD - Tensile Strength (N) - B        | 467           | 547       | 445    | 503 | 516  |   |   |   |   |    | 496  | 40           |                |
| TD - Tensile Strength (kN/m) - B     | 9.2           | 10.8      | 8.8    | 9.9 | 10.2 |   |   |   |   |    | 9.8  | 8.0          |                |
| ΓD - Tensile Strength (lbs) - E      | 104           | 88        | 101    | 100 | 86   |   |   |   |   |    | 96   | 8            | 8.56           |
| D - Tensile Strength (ppi) - E       | 52            | 44        | 51     | 50  | 43   |   |   |   |   |    | 48   | 4            |                |
| ΓD - Tensile Strength (N) - E        | 463           | 392       | 449    | 445 | 383  |   |   |   |   |    | 426  | 36           |                |
| ΓD - Tensile Strength (kN/m) - E     | 9.1           | 7.7       | 8.8    | 8.8 | 7.5  |   |   |   |   |    | 8.4  | 0.7          | 86             |
| MD - Elong. @ Max. Load (%) - B      | 69            | 72        | 69     | 69  | 74   |   |   |   |   |    | 71   | 2            |                |
| MD - Elong. @ Max. Load (%) - E      | 63            | 43        | 67     | 62  | 57   |   |   |   |   |    | 58   | 9            | 83             |
| D - Elong. @ Max. Load (%) - B       | 86            | 91        | 85     | 87  | 89   |   |   |   |   |    | 88   | 2            |                |
| TD - Elong. @ Max. Load (%) - E      | 72            | 65        | 77     | 73  | 65   |   |   |   |   |    | 70   | 5            | 80             |
| 3 - Baseline Unexposed               |               |           |        |     |      |   |   |   |   |    |      |              |                |
| E - Exposed for 500 hours of ASTM D  | 4355 Cycle    |           |        |     |      |   |   |   |   |    |      |              |                |

MD Machine Direction

TD Transverse Direction

#### **APPENDIX C**

#### **GEOSYNTHETIC INSTALLATION DATA**

#### **Sub-Appendices**

| <b>C.1</b> | Installer's Subgrade Acceptance Forms                    |
|------------|--|
| <b>C.2</b> | Panel Placement Forms                                    |
| <b>C.3</b> | Field Tensiometer Calibration Certificates               |
| <b>C.4</b> | Trial Weld Qualification Test Forms                      |
| <b>C.5</b> | Panel Seaming Forms                                      |
| <b>C.6</b> | Non-Destructive Testing Results                          |
| <b>C.7</b> | Destructive Sampling                                     |
|            | C.7.1 Destructive Sample Log                             |
|            | C.7.2 Destructive Sample Laboratory Testing Results      |
|            | C.7.3 Memorandum Concerning Destructive Failure Tracking |
| CR         | Geomembrane Renair Log                                   |

#### Sub-Appendix C.1

#### **Installer's Subgrade Acceptance Forms**



Panels 1-285

## CERTIFICATE OF SOIL SURFACE ACCEPTANCE

|   |                              |                  | /                |                      |                       |
|---|------------------------------|------------------|------------------|----------------------|-----------------------|
| GEOS                                    | SYNTHETIC INSTALL            | ER               |                  | PROJEC               | Т                     |
| COMPANY:                                | American Environmental       | Group, Ltd.      | OWNER:           | Repub                | lic Services          |
| ADDRESS:                                | 3600 Brecksville Rd, S       | Suite 100        | PROJECT:         | Bridge               | ton Closure           |
|   | Richfield, OH 44             | 286              | LOCATION:        | Bridgeto             | n, MO 63044           |
|   |                              |                  | PROJECT #:       |                      | 317130                |
|   |                              |                  |                  |                      |                       |
| Lthall                                  | Indonaiseand a duly authoris | and annuannesti  | us of American   | Faultanan antal Can  | um I fal ala bassalas |
| 1 the C                                 | Indersigned, a duly authoriz | zed representati | ve of American   | Environmental Gro    | up, Lta., do nereby   |
| accept t                                | he area of soil surface bour | nded by the sec  | ondary geomen    | nbrane liner as an a | cceptable surface to  |
|   |                              | install geosy    | nthetic material | S.                   |                       |
| 1                                       | 1                            |                  |                  | C 0 1                | . / /                 |
| Hrran                                   | Weber Ho                     | ton Well         | 4                | CQH                  | 6/08/17               |
| 11101                                   | NAME                         | SIGNATURI        | =                | TITLE                | DATE                  |
|   | 147 1171                     | 01014/11011      | -                | 1 1 1 See See        | DATE                  |
| CF                                      | RTIFICATE OF ACCE            | PTANCE RE        | CEIVED BY        | COA RESIDEN          | TMANAGER              |
|   | KIII IOATE OF AGGE           | TANGENE          | OLIVED DI        | OGARLOIDER           | IMANAOLI              |
|   | 10-11-11                     | A                |                  | <i>2</i> 2 A         | 4 04 17               |
|   | TRON PHONG                   | CICNI TUD        | -                | <u>QA</u>            | 6.29.17               |
|   | NAME                         | SIGNATURI        | =                | IIILE                | DATE                  |
|   | CERTIFICATE                  | - ACCEDTAR       | ICE DECEN        | IED DY THE OV        | MED                   |
| *************************************** | CERTIFICATE O                | ACCEPTAN         | ACE RECEIV       | ED BY THE OV         | VNER                  |
|   |                              |                  |                  |                      |                       |
|   |                              |                  |                  |                      |                       |
|   | NAME                         | SIGNATUR         |                  | TITLE                | DATE                  |
|   |                              |                  |                  |                      |                       |
|   |                              |                  |                  |                      |                       |
| <i>-</i> .                              | - 15 1 1                     | / -              | . 17             |                      |                       |
| 5-1                                     | 7-17 through                 | n 6-2            | 2-11             |                      |                       |
| ,                                       | $\sigma$                     |                  |                  |                      |                       |
|   |                              |                  |                  |                      |                       |
|   |                              |                  |                  |                      |                       |

#### **Sub-Appendix C.2**

#### **Panel Placement Forms**

| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|----------|
| 1     | 5/17/2017        | 7174686        | 7:15 AM        | SLOPE    | 85     | 16    | 1,360      | AAW   |          |
| 2     | 5/17/2017        | 7174686        | 7:40 AM        | SLOPE    | 89     | 16    | 1,424      | AAW   |          |
| 3     | 5/17/2017        | 7174686        | 7:55 AM        | SLOPE    | 91     | 16    | 1,456      | AAW   |          |
| 4     | 5/17/2017        | 7174686        | 8:10 AM        | SLOPE    | 92     | 16    | 1,472      | AAW   |          |
| 5     | 5/17/2017        | 7174686        | 8:15 AM        | SLOPE    | 96     | 16    | 1,536      | AAW   |          |
| 6     | 5/17/2017        | 7174686        | 8:25 AM        | SLOPE    | 98     | 16    | 1,568      | AAW   |          |
| 7     | 5/18/2017        | 7191049        | 7:20 AM        | SLOPE    | 103    | 16    | 1,648      | AAW   |          |
| 8     | 5/18/2017        | 7191049        | 7:35 AM        | SLOPE    | 109    | 16    | 1,744      | AAW   |          |
| 9     | 5/18/2017        | 7191049        | 7:42 AM        | SLOPE    | 103    | 16    | 1,648      | AAW   |          |
| 10    | 5/18/2017        | 7191049        | 7:50 AM        | SLOPE    | 108    | 16    | 1,728      | AAW   |          |
| 11    | 5/18/2017        | 7191049        | 8:00 AM        | SLOPE    | 113    | 16    | 1,808      | AAW   |          |
| 12    | 5/18/2017        | 7191049        | 8:10 AM        | SLOPE    | 32     | 16    | 512        | AAW   |          |
| 13    | 5/18/2017        | 7177494        | 8:20 AM        | SLOPE    | 79     | 16    | 1,264      | AAW   |          |
| 14    | 5/18/2017        | 7177494        | 8:30 AM        | SLOPE    | 109    | 16    | 1,744      | AAW   |          |
| 15    | 5/18/2017        | 7177494        | 8:40 AM        | SLOPE    | 108    | 16    | 1,728      | AAW   |          |
| 16    | 5/18/2017        | 7177494        | 11:15 AM       | SLOPE    | 108    | 16    | 1,728      | AAW   |          |
| 17    | 5/18/2017        | 7177494        | 11:20 AM       | SLOPE    | 107    | 16    | 1,712      | AAW   |          |
| 18    | 5/18/2017        | 7177494        | 12:50 PM       | SLOPE    | 60     | 16    | 960        | AAW   |          |
| 19    | 5/18/2017        | 7178919        | 1:00 PM        | SLOPE    | 23     | 16    | 368        | AAW   |          |
| 20    | 5/18/2017        | 7178919        | 1:10 PM        | SLOPE    | 107    | 16    | 1,712      | AAW   |          |
| 21    | 5/18/2017        | 7178919        | 1:20 PM        | SLOPE    | 107    | 16    | 1,712      | AAW   |          |
| 22    | 5/18/2017        | 7178919        | 1:30 PM        | SLOPE    | 106    | 16    | 1,696      | AAW   |          |
| 23    | 5/18/2017        | 7178919        | 1:40 PM        | SLOPE    | 103    | 16    | 1,648      | AAW   |          |
| 24    | 5/18/2017        | 7178919        | 1:50 PM        | SLOPE    | 99     | 16    | 1,584      | AAW   |          |
| 25    | 5/18/2017        | 7189137        | 2:15 PM        | SLOPE    | 100    | 16    | 1,600      | AAW   |          |
| 26    | 5/18/2017        | 7189137        | 3:15 PM        | SLOPE    | 45     | 15    | 675        | AAW   |          |
| 27    | 5/18/2017        | 7189137        | 3:20 PM        | SLOPE    | 103    | 16    | 1,648      | AAW   |          |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments                     |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|------------------------------|
| 28    | 5/22/2017        | 7189137        | 2:55 PM        | SLOPE    | 55     | 16    | 440        | AAW   | Triangle /2                  |
| 29    | 5/22/2017        | 7189137        | 3:10 PM        | SLOPE    | 117    | 16    | 1,872      | AAW   |                              |
| 30    | 5/22/2017        | 7189137        | 3:30 PM        | SLOPE    | 132    | 16    | 2,112      | AAW   |                              |
| 31    | 5/22/2017        | 7173687        | 3:50 PM        | SLOPE    | 13     | 16    | 208        | AAW   |                              |
| 32    | 5/22/2017        | 7173687        | 4:10 PM        | SLOPE    | 29     | 16    | 232        | AAW   | Triangle /2                  |
| 33    | 5/22/2017        | 7173687        | 4:30 PM        | SLOPE    | 135    | 16    | 2,160      | AAW   |                              |
| 34    | 5/22/2017        | 7173687        | 4:40 PM        | SLOPE    | 86     | 16    | 1,376      | AAW   |                              |
| 35    | 5/22/2017        | 7173687        | 4:50 PM        | SLOPE    | 56     | 16    | 896        | AAW   |                              |
| 36    | 5/22/2017        | 7173687        | 5:25 PM        | SLOPE    | 154    | 16    | 2,464      | AAW   |                              |
| 37    | 5/23/2017        | 7173687        | 9:20 AM        | SLOPE    | 75     | 16    | 1,200      | AAW   |                              |
| 38    | 5/23/2017        | 7175605        | 9:30 AM        | SLOPE    | 81     | 16    | 1,296      | AAW   |                              |
| 39    | 5/23/2017        | 7175605        | 9:40 AM        | SLOPE    | 151    | 16    | 2,416      | AAW   |                              |
| 40    | 5/24/2017        | 7175605        | 8:40 AM        | SLOPE    | 157    | 16    | 2,512      | AAW   |                              |
| 41    | 5/24/2017        | 7175605        | 9:10 AM        | SLOPE    | 157    | 16    | 2,512      | AAW   |                              |
| 42    | 5/24/2017        | 7177400        | 9:20 AM        | SLOPE    | 130    | 16    | 2,080      | AAW   |                              |
| 43    | 5/24/2017        | 7177400        | 9:50 AM        | SLOPE    | 26     | 16    | 416        | AAW   |                              |
| 44    | 5/24/2017        | 7177400        | 10:15 AM       | SLOPE    | 73     | 16    | 1,168      | AAW   |                              |
| 45    | 5/24/2017        | 7177400        | 10:30 AM       | SLOPE    | 57     | 16    | 456        | AAW   | Triangle /2                  |
| 46    | 5/24/2017        | 7177400        | 10:40 AM       | SLOPE    | 25     | 16    | 400        | AAW   |                              |
| 47    | 5/24/2017        | 7177400        | 10:50 AM       | SLOPE    | 130    | 16    | 2,080      | AAW   |                              |
| 48    | 5/24/2017        | 7177400        | 11:05 AM       | SLOPE    | 103    | 16    | 1,648      | AAW   |                              |
| 49    | 5/24/2017        | 7177400        | 11:15 AM       | SLOPE    | 52     | 16    | 832        | AAW   |                              |
| 50    | 5/24/2017        | 7190332        | 12:35 PM       | SLOPE    | 23     | 16    | 368        | AAW   |                              |
| 51    | 5/24/2017        | 7190332        | 12:40 PM       | SLOPE    | 38     | 16    | 608        | AAW   |                              |
| 52    | 5/25/2017        | 7190332        | 6:40 AM        | SLOPE    | 30     | 14    | 210        | AAW   | Triangle /2                  |
| 53    | 5/25/2017        | 7190332        | 6:50 AM        | SLOPE    | 51.5   | 16    | 824        | AAW   | Length is avg. of both sides |
| 54    | 5/25/2017        | 7190332        | 7:00 AM        | SLOPE    | 107    | 16    | 1,712      | AAW   |                              |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments                     |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|------------------------------|
| 55    | 5/25/2017        | 7190332        | 7:20 AM        | SLOPE    | 113    | 16    | 1,808      | AAW   |                              |
| 56    | 5/25/2017        | 7190332        | 7:30 AM        | SLOPE    | 116    | 16    | 1,856      | AAW   |                              |
| 57    | 5/25/2017        | 7190332        | 7:40 AM        | SLOPE    | 59     | 16    | 944        | AAW   |                              |
| 58    | 5/25/2017        | 7189739        | 7:50 AM        | SLOPE    | 59     | 16    | 944        | AAW   |                              |
| 59    | 5/25/2017        | 7189739        | 8:00 AM        | SLOPE    | 68     | 16    | 1,088      | AAW   |                              |
| 60    | 5/25/2017        | 7189739        | 8:15 AM        | SLOPE    | 126    | 16    | 2,016      | AAW   |                              |
| 61    | 5/25/2017        | 7189739        | 8:25 AM        | SLOPE    | 130    | 16    | 2,080      | AAW   |                              |
| 62    | 5/25/2017        | 7189739        | 8:50 AM        | SLOPE    | 125    | 16    | 2,000      | AAW   |                              |
| 63    | 5/25/2017        | 7190194        | 9:00 AM        | SLOPE    | 142    | 16    | 2,272      | AAW   |                              |
| 64    | 5/25/2017        | 7190194        | 9:15 AM        | SLOPE    | 138    | 16    | 2,208      | AAW   |                              |
| 65    | 5/25/2017        | 7190194        | 9:25 AM        | SLOPE    | 10     | 14    | 70         | AAW   | Triangle /2                  |
| 66    | 5/25/2017        | 7190194        | 9:35 AM        | SLOPE    | 138    | 16    | 2,208      | AAW   |                              |
| 67    | 5/25/2017        | 7190194        | 9:50 AM        | SLOPE    | 136    | 16    | 2,176      | AAW   |                              |
| 68    | 5/25/2017        | 7190889        | 2:05 PM        | SLOPE    | 35     | 16    | 560        | AAW   |                              |
| 69    | 5/25/2017        | 7190889        | 2:20 PM        | SLOPE    | 50     | 16    | 800        | AAW   |                              |
| 70    | 5/25/2017        | 7190889        | 2:30 PM        | SLOPE    | 54     | 16    | 864        | AAW   |                              |
| 71    | 5/25/2017        | 7190889        | 2:40 PM        | SLOPE    | 140    | 16    | 2,240      | AAW   |                              |
| 72    | 5/25/2017        | 7190889        | 2:50 PM        | SLOPE    | 52     | 16    | 832        | AAW   |                              |
| 73    | 5/25/2017        | 7190889        | 3:00 PM        | SLOPE    | 170    | 16    | 2,720      | AAW   |                              |
| 74    | 5/25/2017        | 7190889        | 3:10 PM        | SLOPE    | 63     | 16    | 1,008      | AAW   |                              |
| 75    | 5/25/2017        | 7171929        | 3:20 PM        | SLOPE    | 86     | 16    | 1,376      | AAW   |                              |
| 76    | 5/25/2017        | 7171929        | 3:35 PM        | SLOPE    | 124    | 16    | 1,984      | AAW   |                              |
| 77    | 5/25/2017        | 7171929        | 3:50 PM        | SLOPE    | 100    | 16    | 1,600      | AAW   |                              |
| 78    | 5/26/2017        | 7190775        | 8:55 AM        | SLOPE    | 77     | 16    | 1,232      | AAW   |                              |
| 79    | 5/26/2017        | 7190775        | 9:15 AM        | SLOPE    | 50     | 16    | 800        | AAW   |                              |
| 80    | 5/26/2017        | 7190775        | 9:25 AM        | SLOPE    | 15.5   | 16    | 248        | AAW   | Length is avg. of both sides |
| 81    | 5/31/2017        | 7190775        | 9:45 AM        | SLOPE    | 17     | 13    | 221        | AAW   |                              |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|----------|
| 82    | 5/31/2017        | 7190775        | 9:50 AM        | SLOPE    | 38     | 16    | 608        | AAW   |          |
| 83    | 5/31/2017        | 7190775        | 9:55 AM        | SLOPE    | 49     | 16    | 784        | AAW   |          |
| 84    | 5/31/2017        | 7190775        | 10:05 AM       | SLOPE    | 59     | 16    | 944        | AAW   |          |
| 85    | 5/31/2017        | 7190775        | 10:15 AM       | SLOPE    | 65     | 16    | 1,040      | AAW   |          |
| 86    | 5/31/2017        | 7190775        | 10:25 AM       | SLOPE    | 79     | 16    | 1,264      | AAW   |          |
| 87    | 5/31/2017        | 7190775        | 10:35 AM       | SLOPE    | 87     | 16    | 1,392      | AAW   |          |
| 88    | 5/31/2017        | 7179682        | 10:45 AM       | SLOPE    | 99     | 16    | 1,584      | AAW   |          |
| 89    | 5/31/2017        | 7179682        | 1:20 PM        | SLOPE    | 113    | 16    | 1,808      | AAW   |          |
| 90    | 5/31/2017        | 7179682        | 1:35 PM        | SLOPE    | 124    | 16    | 1,984      | AAW   |          |
| 91    | 5/31/2017        | 7179682        | 1:47 PM        | SLOPE    | 132    | 16    | 2,112      | AAW   |          |
| 92    | 5/31/2017        | 7179682        | 2:30 PM        | SLOPE    | 83     | 16    | 1,328      | AAW   |          |
| 93    | 5/31/2017        | 7171929        | 2:40 PM        | SLOPE    | 62     | 16    | 992        | AAW   |          |
| 94    | 5/31/2017        | 7171929        | 2:50 PM        | SLOPE    | 172    | 16    | 2,752      | AAW   |          |
| 95    | 5/31/2017        | 7173374        | 3:00 PM        | SLOPE    | 172    | 16    | 2,752      | AAW   |          |
| 96    | 5/31/2017        | 7173374        | 3:10 PM        | SLOPE    | 173    | 16    | 2,768      | AAW   |          |
| 97    | 6/1/2017         | 7173374        | 11:32 AM       | SLOPE    | 170    | 16    | 2,720      | BJD   |          |
| 98    | 6/1/2017         | 7173374        | 11:40 AM       | SLOPE    | 45     | 16    | 720        | BJD   |          |
| 99    | 6/1/2017         | 7176308        | 12:35 PM       | SLOPE    | 126    | 16    | 2,016      | BJD   |          |
| 100   | 6/1/2017         | 7176308        | 3:15 PM        | SLOPE    | 173    | 16    | 2,768      | BJD   |          |
| 101   | 6/1/2017         | 7176308        | 3:35 PM        | SLOPE    | 174    | 16    | 2,784      | BJD   |          |
| 102   | 6/1/2017         | 7176308        | 3:45 PM        | SLOPE    | 47     | 16    | 752        | BJD   |          |
| 103   | 6/1/2017         | 7176308        | 3:55 PM        | SLOPE    | 43     | 16    | 688        | BJD   |          |
| 104   | 6/1/2017         | 7188997        | 4:30 PM        | SLOPE    | 132    | 16    | 2,112      | BJD   |          |
| 105   | 6/1/2017         | 7188997        | 4:45 PM        | SLOPE    | 140    | 16    | 2,240      | BJD   |          |
| 106   | 6/1/2017         | 7188997        | 4:50 PM        | SLOPE    | 52     | 16    | 832        | BJD   |          |
| 107   | 6/1/2017         | 7188997        | 4:56 PM        | SLOPE    | 52     | 16    | 832        | BJD   |          |
| 108   | 6/1/2017         | 7188997        | 5:04 PM        | SLOPE    | 128    | 16    | 2,048      | BJD   |          |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments    |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|-------------|
| 109   | 6/1/2017         | 7176368        | 5:25 PM        | SLOPE    | 129    | 16    | 2,064      | BJD   |             |
| 110   | 6/3/2017         | 7189388        | 7:35 AM        | SLOPE    | 83     | 16    | 1,328      | BJD   |             |
| 111   | 6/3/2017         | 7189388        | 7:42 AM        | SLOPE    | 75     | 16    | 1,200      | BJD   |             |
| 112   | 6/3/2017         | 7189388        | 7:52 AM        | SLOPE    | 66     | 16    | 1,056      | BJD   |             |
| 113   | 6/3/2017         | 7189388        | 8:04 AM        | SLOPE    | 66     | 16    | 1,056      | BJD   |             |
| 114   | 6/3/2017         | 7189388        | 8:12 AM        | SLOPE    | 64     | 16    | 1,024      | BJD   |             |
| 115   | 6/3/2017         | 7189388        | 8:15 AM        | SLOPE    | 66     | 16    | 1,056      | BJD   |             |
| 116   | 6/3/2017         | 7189388        | 8:21 AM        | SLOPE    | 67     | 16    | 1,072      | BJD   |             |
| 117   | 6/3/2017         | 7189388        | 8:27 AM        | SLOPE    | 60     | 16    | 960        | BJD   |             |
| 118   | 6/3/2017         | 7173290        | 8:35 AM        | SLOPE    | 7      | 16    | 112        | BJD   |             |
| 119   | 6/3/2017         | 7173290        | 8:42 AM        | SLOPE    | 69     | 16    | 1,104      | BJD   |             |
| 120   | 6/3/2017         | 7173290        | 9:00 AM        | SLOPE    | 69     | 16    | 1,104      | BJD   |             |
| 121   | 6/3/2017         | 7173290        | 9:10 AM        | SLOPE    | 66     | 16    | 1,056      | BJD   |             |
| 122   | 6/3/2017         | 7173290        | 9:19 AM        | SLOPE    | 66     | 16    | 1,056      | BJD   |             |
| 123   | 6/3/2017         | 7173290        | 9:27 AM        | SLOPE    | 67     | 16    | 1,072      | BJD   |             |
| 124   | 6/3/2017         | 7173290        | 9:35 AM        | SLOPE    | 64     | 16    | 1,024      | BJD   |             |
| 125   | 6/3/2017         | 7173290        | 9:45 AM        | SLOPE    | 63     | 16    | 1,008      | BJD   |             |
| 126   | 6/3/2017         | 7173290        | 9:50 AM        | SLOPE    | 58.19  | 16    | 931        | BJD   |             |
| 127   | 6/3/2017         | 7175973        | 10:18 AM       | SLOPE    | 57     | 16    | 912        | BJD   |             |
| 128   | 6/3/2017         | 7173290        | 10:20 AM       | SLOPE    | 22     | 6     | 66         | BJD   | Triangle /2 |
| 129   | 6/3/2017         | 7175973        | 10:25 AM       | SLOPE    | 53     | 16    | 848        | BJD   |             |
| 130   | 6/3/2017         | 7175973        | 10:31 AM       | SLOPE    | 56     | 16    | 896        | BJD   |             |
| 131   | 6/3/2017         | 7175973        | 10:44 AM       | SLOPE    | 54     | 16    | 864        | BJD   |             |
| 132   | 6/3/2017         | 7175973        | 10:52 AM       | SLOPE    | 51.88  | 16    | 830        | BJD   |             |
| 133   | 6/3/2017         | 7175973        | 10:56 AM       | SLOPE    | 27     | 7     | 95         | BJD   | Triangle /2 |
| 134   | 6/3/2017         | 7175973        | 11:05 AM       | SLOPE    | 34     | 16    | 544        | BJD   |             |
| 135   | 6/3/2017         | 7175973        | 11:15 AM       | SLOPE    | 35     | 16    | 560        | BJD   |             |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments    |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|-------------|
| 136   | 6/3/2017         | 7175973        | 1:00 PM        | SLOPE    | 83     | 16    | 1,328      | BJD   |             |
| 137   | 6/3/2017         | 7175973        | 1:15 PM        | SLOPE    | 86     | 16    | 1,376      | BJD   |             |
| 138   | 6/3/2017         | 7176326        | 1:25 PM        | SLOPE    | 47     | 16    | 752        | BJD   |             |
| 139   | 6/3/2017         | 7176326        | 1:33 PM        | SLOPE    | 46     | 16    | 736        | BJD   |             |
| 140   | 6/3/2017         | 7176326        | 1:41 PM        | SLOPE    | 47     | 16    | 752        | BJD   |             |
| 141   | 6/3/2017         | 7176326        | 1:44 PM        | SLOPE    | 47     | 16    | 752        | BJD   |             |
| 142   | 6/3/2017         | 7176326        | 1:59 PM        | SLOPE    | 43     | 16    | 688        | BJD   |             |
| 143   | 6/6/2017         | 7176368        | 11:13 AM       | SLOPE    | 176    | 16    | 2,816      | BJD   |             |
| PE1   | 6/6/2017         | 7176368        | 12:00 PM       | SLOPE    | 13     | 12    | 156        | BJD   |             |
| PE2   | 6/6/2017         | 7176368        | 12:10 PM       | SLOPE    | 13     | 12    | 156        | BJD   |             |
| 144   | 6/6/2017         | 7176368        | 1:26 PM        | SLOPE    | 175    | 16    | 2,800      | BJD   |             |
| 145   | 6/6/2017         | 7176368        | 1:40 PM        | SLOPE    | 38     | 16    | 608        | BJD   |             |
| 146   | 6/6/2017         | 7171890        | 1:57 PM        | SLOPE    | 148    | 16    | 2,368      | BJD   |             |
| 147   | 6/6/2017         | 7176347        | 2:10 PM        | SLOPE    | 55     | 16    | 880        | BJD   |             |
| 148   | 6/6/2017         | 7176347        | 2:15 PM        | SLOPE    | 44     | 16    | 704        | BJD   |             |
| 149   | 6/6/2017         | 7176347        | 2:19 PM        | SLOPE    | 22     | 13    | 286        | BJD   |             |
| 150   | 6/6/2017         | 7176347        | 2:26 PM        | SLOPE    | 32     | 16    | 256        | BJD   | Triangle /2 |
| 151   | 6/6/2017         | 7176347        | 2:32 PM        | SLOPE    | 72     | 16    | 1,152      | BJD   |             |
| 152   | 6/6/2017         | 7176347        | 2:36 PM        | SLOPE    | 137    | 16    | 2,192      | BJD   |             |
| 153   | 6/6/2017         | 7176347        | 2:44 PM        | SLOPE    | 141    | 16    | 2,256      | BJD   |             |
| 154   | 6/6/2017         | 7177308        | 3:00 PM        | SLOPE    | 22     | 16    | 352        | BJD   |             |
| 155   | 6/6/2017         | 7177308        | 3:10 PM        | SLOPE    | 195    | 16    | 3,120      | BJD   |             |
| 156   | 6/7/2017         | 7177308        | 1:40 PM        | SLOPE    | 208    | 16    | 3,328      | BJD   |             |
| 157   | 6/7/2017         | 7177308        | 1:50 PM        | SLOPE    | 106    | 16    | 1,696      | BJD   |             |
| 158   | 6/7/2017         | 7176384        | 2:15 PM        | SLOPE    | 108    | 16    | 1,728      | BJD   |             |
| 159   | 6/7/2017         | 7176384        | 3:25 PM        | SLOPE    | 230    | 16    | 3,680      | BJD   |             |
| 160   | 6/7/2017         | 7176384        | 3:50 PM        | SLOPE    | 217    | 16    | 3,472      | BJD   |             |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments    |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|-------------|
| 161   | 6/7/2017         | 7176384        | 4:10 PM        | SLOPE    | 8      | 16    | 128        | BJD   |             |
| 162   | 6/7/2017         | 7176173        | 4:30 PM        | SLOPE    | 232    | 16    | 3,712      | BJD   |             |
| 163   | 6/7/2017         | 7176173        | 5:00 PM        | SLOPE    | 208    | 16    | 3,328      | BJD   |             |
| 164   | 6/8/2017         | 7176173        | 1:26 PM        | SLOPE    | 90     | 16    | 1,440      | BJD   |             |
| 165   | 6/8/2017         | 7176434        | 2:00 PM        | SLOPE    | 77     | 16    | 1,232      | BJD   |             |
| 166   | 6/8/2017         | 7176434        | 2:15 PM        | SLOPE    | 140    | 16    | 2,240      | BJD   |             |
| 167   | 6/8/2017         | 7176434        | 2:20 PM        | SLOPE    | 126    | 16    | 2,016      | BJD   |             |
| 168   | 6/8/2017         | 7176434        | 2:48 PM        | SLOPE    | 92     | 16    | 1,472      | BJD   |             |
| 169   | 6/8/2017         | 7176434        | 3:00 PM        | SLOPE    | 44     | 16    | 704        | BJD   |             |
| 170   | 6/8/2017         | 7172809        | 3:25 PM        | SLOPE    | 268    | 16    | 4,288      | BJD   |             |
| 171   | 6/8/2017         | 7172809        | 3:40 PM        | SLOPE    | 267    | 16    | 4,272      | BJD   |             |
| 172   | 6/8/2017         | 7172809        | 3:50 PM        | SLOPE    | 20     | 16    | 320        | BJD   |             |
| 173   | 6/8/2017         | 7080358        | 4:10 PM        | SLOPE    | 158    | 16    | 2,528      | BJD   |             |
| 174   | 6/8/2017         | 7080358        | 4:17 PM        | SLOPE    | 140    | 16    | 2,240      | BJD   |             |
| 175   | 6/8/2017         | 7080358        | 4:33 PM        | SLOPE    | 103    | 16    | 1,648      | BJD   |             |
| 176   | 6/8/2017         | 7080358        | 4:44 PM        | SLOPE    | 58     | 16    | 928        | BJD   |             |
| 177   | 6/8/2017         | 7080358        | 4:58 PM        | SLOPE    | 35     | 16    | 280        | BJD   | Triangle /2 |
| 178   | 6/8/2017         | 7176434        | 5:15 PM        | SLOPE    | 16     | 8     | 64         | BJD   | Triangle /2 |
| PE3   | 6/9/2017         | 7080358        | 9:20 AM        | SLOPE    | 13     | 16    | 208        | BJD   |             |
| 179   | 6/9/2017         | 7080198        | 10:00 AM       | SLOPE    | 149    | 16    | 2,384      | BJD   |             |
| 180   | 6/9/2017         | 7080198        | 10:09 AM       | SLOPE    | 52     | 16    | 832        | BJD   |             |
| 181   | 6/9/2017         | 7080198        | 10:29 AM       | SLOPE    | 227    | 16    | 3,632      | BJD   |             |
| 182   | 6/9/2017         | 7080198        | 10:41 AM       | SLOPE    | 95     | 16    | 1,520      | BJD   |             |
| 183   | 6/9/2017         | 7176218        | 11:06 AM       | SLOPE    | 77     | 16    | 1,232      | BJD   |             |
| 184   | 6/9/2017         | 7176218        | 11:17 AM       | SLOPE    | 62     | 16    | 992        | BJD   |             |
| 185   | 6/9/2017         | 7176218        | 11:25 AM       | SLOPE    | 164    | 16    | 2,624      | BJD   |             |
| 186   | 6/9/2017         | 7176218        | 11:47 AM       | SLOPE    | 91     | 16    | 1,456      | BJD   |             |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments    |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|-------------|
| 187   | 6/9/2017         | 7176218        | 1:00 PM        | SLOPE    | 102    | 16    | 1,632      | BJD   |             |
| 188   | 6/9/2017         | 7176218        | 1:15 PM        | SLOPE    | 65     | 16    | 520        | BJD   | Triangle /2 |
| 189   | 6/9/2017         | 7081034        | 1:30 PM        | SLOPE    | 162    | 16    | 2,592      | BJD   |             |
| 190   | 6/9/2017         | 7081034        | 2:00 PM        | SLOPE    | 220    | 16    | 3,520      | BJD   |             |
| 191   | 6/9/2017         | 7081034        | 2:25 PM        | SLOPE    | 122    | 16    | 1,952      | BJD   |             |
| 192   | 6/9/2017         | 7080628        | 2:39 PM        | SLOPE    | 100    | 16    | 1,600      | BJD   |             |
| 193   | 6/9/2017         | 7080628        | 2:50 PM        | SLOPE    | 211    | 16    | 3,376      | BJD   |             |
| 194   | 6/9/2017         | 7080628        | 3:00 PM        | SLOPE    | 206    | 16    | 3,296      | BJD   |             |
| 195   | 6/9/2017         | 7080628        | 3:20 PM        | SLOPE    | 49     | 16    | 784        | BJD   |             |
| 196   | 6/9/2017         | 7081551        | 4:00 PM        | SLOPE    | 150    | 16    | 2,400      | BJD   |             |
| 197   | 6/9/2017         | 7081551        | 4:15 PM        | SLOPE    | 190    | 16    | 3,040      | BJD   |             |
| 198   | 6/10/2017        | 7081551        | 7:10 AM        | SLOPE    | 177    | 16    | 2,832      | BJD   |             |
| 199   | 6/10/2017        | 7081551        | 7:20 AM        | SLOPE    | 40     | 16    | 640        | BJD   |             |
| 200   | 6/10/2017        | 7080533        | 8:00 AM        | SLOPE    | 128    | 16    | 2,048      | BJD   |             |
| 201   | 6/10/2017        | 7080533        | 8:10 AM        | SLOPE    | 157    | 16    | 2,512      | BJD   |             |
| 202   | 6/10/2017        | 7080533        | 8:17 AM        | SLOPE    | 101    | 16    | 1,616      | BJD   |             |
| 203   | 6/10/2017        | 7080533        | 8:40 AM        | SLOPE    | 50     | 16    | 800        | BJD   |             |
| 204   | 6/10/2017        | 7080533        | 8:58 AM        | SLOPE    | 125    | 16    | 2,000      | BJD   |             |
| 205   | 6/12/2017        | 7174569        | 7:10 AM        | SLOPE    | 19     | 16    | 304        | BJD   |             |
| 206   | 6/12/2017        | 7174569        | 7:19 AM        | SLOPE    | 133    | 16    | 2,128      | BJD   |             |
| 207   | 6/12/2017        | 7174569        | 7:30 AM        | SLOPE    | 126    | 16    | 2,016      | BJD   |             |
| 208   | 6/12/2017        | 7174569        | 8:15 AM        | SLOPE    | 114    | 16    | 1,824      | BJD   |             |
| 209   | 6/13/2017        | 7080866        | 8:45 AM        | SLOPE    | 63     | 16    | 1,008      | BJD   |             |
| 210   | 6/13/2017        | 7080866        | 9:00 AM        | SLOPE    | 64     | 16    | 1,024      | BJD   |             |
| 211   | 6/13/2017        | 7080866        | 9:05 AM        | SLOPE    | 61     | 16    | 976        | BJD   |             |
| 212   | 6/13/2017        | 7080866        | 9:11 AM        | SLOPE    | 63     | 16    | 1,008      | BJD   |             |
| 213   | 6/13/2017        | 7080866        | 9:15 AM        | SLOPE    | 33     | 13    | 429        | BJD   |             |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|----------|
| 214   | 6/13/2017        | 7080866        | 9:25 AM        | SLOPE    | 35     | 16    | 560        | BJD   |          |
| 215   | 6/13/2017        | 7080866        | 9:30 AM        | SLOPE    | 29     | 13    | 377        | BJD   |          |
| 216   | 6/13/2017        | 7080866        | 9:36 AM        | SLOPE    | 29     | 16    | 464        | BJD   |          |
| 217   | 6/13/2017        | 7080866        | 9:45 AM        | SLOPE    | 93     | 16    | 1,488      | BJD   |          |
| 218   | 6/13/2017        | 7080866        | 9:55 AM        | SLOPE    | 87     | 16    | 1,392      | BJD   |          |
| 219   | 6/13/2017        | 7172029        | 10:05 AM       | SLOPE    | 10     | 16    | 160        | BJD   |          |
| 220   | 6/13/2017        | 7172029        | 10:14 AM       | SLOPE    | 91     | 16    | 1,456      | BJD   |          |
| 221   | 6/13/2017        | 7172029        | 10:22 AM       | SLOPE    | 73     | 16    | 1,168      | BJD   |          |
| 222   | 6/13/2017        | 7172029        | 10:30 AM       | SLOPE    | 19     | 16    | 304        | BJD   |          |
| 223   | 6/13/2017        | 7172029        | 10:41 AM       | SLOPE    | 90     | 16    | 1,440      | BJD   |          |
| 224   | 6/14/2017        | 7172029        | 7:37 AM        | SLOPE    | 90     | 16    | 1,440      | BJD   |          |
| 225   | 6/14/2017        | 7172029        | 7:45 AM        | SLOPE    | 90     | 16    | 1,440      | BJD   |          |
| 226   | 6/14/2017        | 7172029        | 7:54 AM        | SLOPE    | 89     | 16    | 1,424      | BJD   |          |
| 227   | 6/14/2017        | 7081930        | 9:10 AM        | SLOPE    | 89     | 16    | 1,424      | BJD   |          |
| 228   | 6/14/2017        | 7081930        | 9:25 AM        | SLOPE    | 89     | 16    | 1,424      | BJD   |          |
| 229   | 6/14/2017        | 7081930        | 9:37 AM        | SLOPE    | 89     | 16    | 1,424      | BJD   |          |
| 230   | 6/14/2017        | 7081930        | 9:52 AM        | SLOPE    | 89     | 16    | 1,424      | BJD   |          |
| 231   | 6/14/2017        | 7081930        | 10:07 AM       | SLOPE    | 90     | 16    | 1,440      | BJD   |          |
| 232   | 6/14/2017        | 7081930        | 10:20 AM       | SLOPE    | 61     | 16    | 976        | BJD   |          |
| 233   | 6/14/2017        | 7081930        | 10:30 AM       | SLOPE    | 32     | 16    | 512        | BJD   |          |
| 234   | 6/14/2017        | 7172035        | 11:10 AM       | SLOPE    | 90     | 16    | 1,440      | BJD   |          |
| 235   | 6/14/2017        | 7172035        | 11:28 AM       | SLOPE    | 71     | 16    | 1,136      | BJD   |          |
| 236   | 6/14/2017        | 7172035        | 11:35 AM       | SLOPE    | 23     | 16    | 368        | BJD   |          |
| 237   | 6/21/2017        | 7172035        | 8:10 AM        | SLOPE    | 79     | 16    | 1,264      | AAW   |          |
| 238   | 6/21/2017        | 7172035        | 8:30 AM        | SLOPE    | 80     | 16    | 1,280      | AAW   |          |
| 239   | 6/21/2017        | 7172035        | 8:55 AM        | SLOPE    | 34     | 16    | 544        | AAW   |          |
| 240   | 6/21/2017        | 7172035        | 9:15 AM        | SLOPE    | 50     | 16    | 800        | AAW   |          |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|----------|
| 241   | 6/21/2017        | 7080392        | 9:45 AM        | SLOPE    | 87     | 16    | 1,392      | AAW   |          |
| 242   | 6/21/2017        | 7080392        | 10:00 AM       | SLOPE    | 57     | 16    | 912        | AAW   |          |
| 243   | 6/21/2017        | 7080392        | 10:15 AM       | SLOPE    | 36     | 16    | 576        | AAW   |          |
| 244   | 6/21/2017        | 7080392        | 10:30 AM       | SLOPE    | 79     | 16    | 1,264      | AAW   |          |
| 245   | 6/21/2017        | 7080392        | 1:00 PM        | SLOPE    | 71     | 16    | 1,136      | AAW   |          |
| 246   | 6/21/2017        | 7080392        | 1:20 PM        | SLOPE    | 72     | 16    | 1,152      | AAW   |          |
| 247   | 6/21/2017        | 7080392        | 1:35 PM        | SLOPE    | 56     | 16    | 896        | AAW   |          |
| 248   | 6/21/2017        | 7172035        | 1:45 PM        | SLOPE    | 47     | 16    | 752        | AAW   |          |
| 249   | 6/21/2017        | 7172035        | 1:59 PM        | SLOPE    | 40     | 16    | 640        | AAW   |          |
| 250   | 6/21/2017        | 7172035        | 2:15 PM        | SLOPE    | 31     | 16    | 496        | AAW   |          |
| 251   | 6/21/2017        | 7172035        | 2:25 PM        | SLOPE    | 24     | 16    | 384        | AAW   |          |
| 252   | 6/22/2017        | 7172216        | 7:25 AM        | SLOPE    | 69     | 16    | 1,104      | AAW   |          |
| 253   | 6/22/2017        | 7172216        | 7:35 AM        | SLOPE    | 32     | 16    | 512        | AAW   |          |
| 254   | 6/22/2017        | 7172216        | 7:45 AM        | SLOPE    | 55     | 16    | 880        | AAW   |          |
| 255   | 6/22/2017        | 7172216        | 7:50 AM        | SLOPE    | 59     | 16    | 944        | AAW   |          |
| 256   | 6/22/2017        | 7172216        | 8:00 AM        | SLOPE    | 46     | 16    | 736        | AAW   |          |
| 257   | 6/22/2017        | 7172216        | 9:10 AM        | SLOPE    | 34     | 16    | 544        | AAW   |          |
| 258   | 6/22/2017        | 7172216        | 9:20 AM        | SLOPE    | 35     | 16    | 560        | AAW   |          |
| 259   | 6/22/2017        | 7172216        | 9:30 AM        | SLOPE    | 35     | 16    | 560        | AAW   |          |
| 260   | 6/22/2017        | 7172216        | 9:40 AM        | SLOPE    | 35     | 16    | 560        | AAW   |          |
| 261   | 6/22/2017        | 7172216        | 9:50 AM        | SLOPE    | 36     | 16    | 576        | AAW   |          |
| 262   | 6/22/2017        | 7172216        | 9:59 AM        | SLOPE    | 36     | 16    | 576        | AAW   |          |
| 263   | 6/22/2017        | 7172216        | 10:10 AM       | SLOPE    | 35     | 16    | 560        | AAW   |          |
| 264   | 6/22/2017        | 7172216        | 10:20 AM       | SLOPE    | 32     | 16    | 512        | AAW   |          |
| 265   | 6/22/2017        | 7172216        | 10:30 AM       | SLOPE    | 30     | 16    | 480        | AAW   |          |
| 266   | 6/22/2017        | 7172216        | 10:50 AM       | SLOPE    | 31     | 16    | 496        | AAW   |          |
| 267   | 6/22/2017        | 7172216        | 11:00 AM       | SLOPE    | 28     | 16    | 448        | AAW   |          |



| Panel | Date<br>Deployed | Roll<br>Number | Deploy<br>Time | Location | Length | Width | Final Area | QA ID | Comments |
|-------|------------------|----------------|----------------|----------|--------|-------|------------|-------|----------|
| 268   | 6/22/2017        | 7172216        | 11:20 AM       | SLOPE    | 28     | 16    | 448        | AAW   |          |
| 269   | 6/22/2017        | 7172216        | 11:25 AM       | SLOPE    | 26     | 16    | 416        | AAW   |          |
| 270   | 6/22/2017        | 7081252        | 2:50 PM        | SLOPE    | 107    | 16    | 1,712      | AAW   |          |
| 271   | 6/22/2017        | 7081252        | 3:00 PM        | SLOPE    | 38     | 16    | 608        | AAW   |          |
| 272   | 6/22/2017        | 7081252        | 3:15 PM        | SLOPE    | 100    | 16    | 1,600      | AAW   |          |
| 273   | 6/22/2017        | 7081252        | 3:30 PM        | SLOPE    | 38     | 16    | 608        | AAW   |          |
| 274   | 6/22/2017        | 7081252        | 3:40 PM        | SLOPE    | 76     | 16    | 1,216      | AAW   |          |
| 275   | 6/22/2017        | 7081252        | 3:50 PM        | SLOPE    | 64     | 16    | 1,024      | AAW   |          |
| 276   | 6/22/2017        | 7081252        | 4:00 PM        | SLOPE    | 23     | 16    | 368        | AAW   |          |
| 277   | 6/22/2017        | 7080474        | 4:35 PM        | SLOPE    | 19     | 15    | 285        | AAW   |          |
| 278   | 6/22/2017        | 7080474        | 4:45 PM        | SLOPE    | 22     | 15    | 330        | AAW   |          |
| 279   | 6/22/2017        | 7080474        | 4:55 PM        | SLOPE    | 63     | 12    | 756        | AAW   |          |
| 280   | 6/22/2017        | 7080474        | 4:05 PM        | SLOPE    | 54     | 16    | 864        | AAW   |          |
| 281   | 6/22/2017        | 7080474        | 4:15 PM        | SLOPE    | 111    | 16    | 1,776      | AAW   |          |
| 282   | 6/22/2017        | 7080474        | 5:25 PM        | SLOPE    | 30     | 9     | 270        | AAW   |          |
| 283   | 6/22/2017        | 7080474        | 5:30 PM        | SLOPE    | 93     | 16    | 1,488      | AAW   |          |
| 284   | 6/22/2017        | 7080474        | 5:35 PM        | SLOPE    | 20     | 8     | 160        | AAW   |          |
| 285   | 6/22/2017        | 7080474        | 5:40 PM        | SLOPE    | 44     | 16    | 704        | AAW   |          |
| 286   | 6/26/2017        | 7080474        | 3:30 PM        | SLOPE    | 51     | 4     | 204        | AAW   |          |



#### Sub-Appendix C.3

#### **Field Tensiometer Calibration Certificate**

# Demtech Services, Inc. Placerville, California, USA

## CALIBRATION CERTIFICATE

| Tensiometer Model:   | Pro-Tester T-0100  | No.                               |              |
|--|--|-----------------------------------|--------------|
|  |  | Calibration A                     | nnaratus.    |
| Device Calibrated:   | S-Type load cell   | Calibration                       | pparatus.    |
| Range:   | 0 - 750 lbs. Tension   | 1 1 1 (0/8)                       | 204704)      |
| Model No:  | M2405-750#   | Reference load cell (S/N          | 204/01)      |
| Wilder 130.  | 230339   |                                   |              |
| Serial No:   | 230339   | Dead Weight:                      | Reference    |
|  | The state of the s | W1 2                              | R1           |
| A/D Module Model No:   | T-057/06   | W2 152                            | R2           |
| A/D Module Serial No:  | 2508230339   | W3 302                            | R3           |
| Channel No:  | N/A  | VV3 502                           |              |
| Indicator reading with no load:  | 0  |                                   |              |
|  | offset: -1.690870  | Scale: 4.432524                   |              |
|  |  |                                   |              |
| Applied Force lbs.   | Cell Response:   | Deviation Error:                  |              |
|  | 2  | 0.00                              |              |
| 2  | 52   | 0.00                              |              |
| 52   | 102  | 0.00                              |              |
| 102  |  | 0.00                              |              |
| 152  | 152  | 0.00                              |              |
| 202  | 202  | 0.00                              | 0.4          |
| 252  | 252  | 0.00                              | 307-1 x      |
| 302  | 302  | 0.00                              |              |
|  |  |                                   | 10.00        |
|  | Total Deviation En   | ror (%): 0.00%                    |              |
|  |  |                                   |              |
| Temperature at time of calibra   | tion: 73 degrees F   |                                   |              |
| Exitation Voltage:   | 5 VDC  |                                   |              |
| Exitation voltage.   |  |                                   |              |
|  |  |                                   |              |
|  |  |                                   | Second Miles |
| This polibration conforms to th  | ne standards set by ASTM E4 and  | is traceable to NIST standards    |              |
|  |  |                                   | 100000       |
|  | cell above have been systems call  | ibrated and are considered a      | 1            |
| Note: A/D Module and load of   | zell above have been systems out   | and colle are not interchangeable |              |
| matched pair. In gene  | ral, calibrated A/D Modules and lo   | ad cens are not interending cook  | -            |
|  | 12-514-9   |                                   |              |
|  |  | Date:                             | 04/07/17     |
| Calibration Technician:  | Erich Beck   | Date.                             |              |
| Vacional Control of the Control of t | 6/1/6/   |                                   |              |
|  | List I tolech  |                                   |              |

#### Sub-Appendix C.4

#### **Trial Weld Qualification Test Forms**

| Date         | Time        | Material<br>Type | Tech  | Туре | Mach | Amb<br>Temp | Fusion<br>Speed | Fusion<br>Temp | Extr.<br>Preheat | Extr.<br>Barrel | Peel 1<br>(In/Out) | Peel 2<br>(In/Out) | Peel 3<br>(In/Out) | Shear 1 | Shear 2 | Shear 3 | QA ID  | Pass / Fail | Comments |
|--------------|-------------|------------------|-------|------|------|-------------|-----------------|----------------|------------------|-----------------|--------------------|--------------------|--------------------|---------|---------|---------|--------|-------------|----------|
| 5/17/2017    | 7:35 AM     | TT               | KS    | F    | 45   | 76          | 3               | 850            | -                | -               | 125<br>123         | 132<br>124         | 123<br>115         | 145     | 153     | 148     | AAW    | Р           |          |
| 5/17/2017    | 7:50 AM     |                  |       | -    | 2650 | 76          | 7               | 750            | _                | _               | 110                | 112                | 118                | 1.47    | 454     | 146     | 0.0047 | Р           |          |
| 5/1//201/    | 7:50 AIVI   | TT               | May   | F    | 2650 | 76          | /               | 750            | -                | -               | 109                | 115                | 113                | 147     | 151     | 146     | AAW    | Р           |          |
| 5/17/2017    | 1:20 PM     | TT               | PH    | х    | 211  | 85          | -               | -              | 500              | 530             | 115<br>-           | 120                | 151                | 150     | 152     | 150     | AAW    | Р           |          |
| - 4: - 4 : - |             |                  |       | _    |      |             | _               |                |                  |                 | 120                | 120                | 125                |         |         |         |        | _           |          |
| 5/18/2017    | 7:34 AM     | TT               | KS    | F    | 45   | 74          | 3               | 850            | -                | -               | 118                | 123                | 125                | 142     | 140     | 146     | AAW    | Р           |          |
| 5/18/2017    | 7:50 AM     | TT               | MAY   | F    | 2650 | 74          | 7               | 750            | -                | _               | 112                | 112                | 117                | 162     | 160     | 160     | AAW    | Р           |          |
| 3/16/2017    | 7.30 AIVI   | '''              | IVIAI | '    | 2030 | /4          | ,               | 730            |                  |                 | 123                | 123                | 120                | 102     | 100     | 100     | AAW    | '           |          |
| 5/18/2017    | 1:00 PM     | TT               | KS    | F    | 45   | 87          | 5               | 850            | -                |                 | 106                | 117                | 120                | 123     | 124     | 124     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 119                | 115                | 116                |         |         |         |        |             |          |
| 5/18/2017    | 1:00 PM     | TT               | MAY   | F    | 2650 | 87          | 7               | 750            | -                |                 | 108                | 98                 | 108                | 125     | 123     | 126     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 101                | 100                | 106                |         |         |         |        |             |          |
| 5/18/2017    | 3:00 PM     | TT               | MAY   | Х    | 211  | 80          | -               | -              | 500              | 500             | 113                | 117                | 118                | 130     | 138     | 139     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 |                    | 137                |                    |         |         |         |        |             |          |
| 5/22/2017    | 8:30 AM     | TT               | MAY   | Х    | 211  | 65          | -               | -              | 500              | 500             | 127                | -                  | 135                | 140     | 146     | 148     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 125                | 125                | 123                |         |         |         |        |             |          |
| 5/22/2017    | 3:10 PM     | TT               | KS    | F    | 45   | 74          | 5               | 850            | -                |                 | 127                | 120                | 121                | 135     | 137     | 135     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 115                | 110                | 117                | 130 13  |         |         |        |             |          |
| 5/22/2017    | 3:25 PM     | TT               | MAY   | F    | 2650 | 74          | 7               | 750            | -                | - 1             | 112                | 118                | 120                | 138 135 | 135     | 140     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 118                | 117                | 115                |         |         |         |        |             |          |
| 5/23/2017    | 9:30 AM     | TT               | KS    | F    | 45   | 70          | 5               | 850            | -                | - 1             | 116                | 114                | 115                | 139     | 141     | 142     | AAW    | Р           |          |
|              |             |                  |       | _    |      |             | _               |                |                  |                 | 112                | 108                | 116                |         |         |         |        | _           |          |
| 5/23/2017    | 9:40 AM     | TT               | MAY   | F    | 2650 | 70          | 7               | 750            | -                | - 1             | 118                | 120                | 118                | 128     | 130     | 141     | AAW    | Р           |          |
| - /0 - /0 0  |             |                  |       | _    |      |             | _               |                |                  |                 | 128                | 125                | 120                | 450     | 440     | 440     |        |             |          |
| 5/24/2017    | 8:50 AM     | TT               | KS    | F    | 45   | 59          | 5               | 850            | -                | - 1             | 123                | 122                | 124                | 150     | 148     | 149     | AAW    | Р           |          |
| E/24/2017    | 8:50 AM     | TT               | MAY   | F    | 2650 | 59          | 7               | 750            | _                | _               | 120                | 121                | 119                | 140     | 142     | 138     | AAW    | Р           |          |
| 5/24/2017    | 6.50 AIVI   | - ''             | IVIAT | Г    | 2030 | 39          | ,               | 750            | -                | -               | 116                | 118                | 117                | 140     | 142     | 138     | AAVV   | Р           |          |
| 5/24/2017    | 12:35 PM    | TT               | KS    | F    | 45   | 70          | 5               | 850            | _                | _               | 127                | 123                | 121                | 152     | 150     | 151     | AAW    | Р           |          |
| 3/24/2017    | 12.55 1 101 |                  | N3    | · ·  | 43   | 70          | 3               | 050            |                  |                 | 120                | 125                | 126                | 132     | 130     | 131     | 70100  |             |          |
| 5/25/2017    | 7:30 AM     | TT               | MAY   | F    | 2650 | 59          | 7               | 750            | _                |                 | 118                | 123                | 120                | 160     | 112     | 170     | AAW    | Р           |          |
| 0, =0, =0=:  |             |                  |       |      |      |             | •               |                |                  |                 | 117                | 121                | 120                |         |         |         |        |             |          |
| 5/25/2017    | 7:20 AM     | TT               | KS    | F    | 45   | 59          | 5               | 850            | -                |                 | 130                | 128                | 125                | 158     | 152     | 155     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 127                | 120                | 126                |         |         |         |        |             |          |
| 5/25/2017    | 9:05 AM     | TT               | AG    | Х    | 112  | 59          | -               | -              | 450              | 550             | 113                | 119                | 115                | 155     | 158     | 152     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |        |             |          |
| 5/25/2017    | 1:55 PM     | TT               | KS    | F    | 45   | 80          | 5               | 850            | -                | - 1             | 109                | 112                | 110<br>111         | 130     | 128     | 128     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 105<br>115         | 110<br>112         |                    |         |         |         |        |             |          |
| 5/25/2017    | 2:05 PM     | TT               | MAY   | F    | 2650 | 80          | 7               | 750            | -                | - 1             | 115                | 112                | 114<br>115         | 125     | 123     | 125     | AAW    | Р           |          |
|              |             |                  |       |      |      |             |                 |                |                  |                 | 112                | 110                | 110                |         |         |         |        |             |          |
| 5/25/2017    | 2:45 PM     | TT               | AG    | Х    | 112  | 76          | -               | -              | 450              | 550             | -                  | -                  | 110                | 125     | 120     | 120     | AAW    | Р           |          |



| Date      | Time     | Material<br>Type | Tech | Туре | Mach | Amb<br>Temp | Fusion<br>Speed | Fusion<br>Temp | Extr.<br>Preheat | Extr.<br>Barrel | Peel 1<br>(In/Out) | Peel 2<br>(In/Out) | Peel 3<br>(In/Out) | Shear 1 | Shear 2 | Shear 3 | QA ID | Pass / Fail | Comments |
|-----------|----------|------------------|------|------|------|-------------|-----------------|----------------|------------------|-----------------|--------------------|--------------------|--------------------|---------|---------|---------|-------|-------------|----------|
| 5/26/2017 | 7:30 AM  | TT               | KS   | F    | 45   | 60          | 5               | 850            | -                | -               | 118<br>115         | 120<br>119         | 119<br>112         | 150     | 145     | 145     | AAW   | Р           |          |
| 5/26/2017 | 9:15 AM  | TT               | AG   | х    | 112  | 65          | -               | -              | 450              | 550             | -<br>115           | -<br>117           | -<br>115           | 143     | 145     | 145     | AAW   | Р           |          |
| 5/26/2017 | 10:05 AM | тт               | MAY  | х    | 60   | 70          | -               | -              | 500              | 500             | -<br>92            | -<br>126           | -<br>119           | 120     | 125     | 125     | AAW   | Р           |          |
| 5/26/2017 | 1:10 PM  | TT               | AG   | х    | 112  | 70          | -               | -              | 500              | 550             | -<br>97            | -<br>122           | 101                | 120     | 110     | 102     | AAW   | Р           |          |
| 5/26/2017 | 1:00 PM  | TT               | MAY  | х    | 60   | 70          | -               | -              | 500              | 500             | -<br>121           | -<br>118           | -<br>126           | 133     | 132     | 122     | AAW   | Р           |          |
| 5/27/2017 | 8:00 AM  | TT               | MAY  | х    | 60   | 72          | -               | -              | 500              | 500             | -<br>120           | -<br>123           | -<br>125           | 140     | 138     | 132     | AAW   | Р           |          |
| 5/27/2017 | 8:30 AM  | тт               | AG   | х    | 112  | 72          | -               | -              | 500              | 550             | -<br>115           | -<br>110           | 112                | 138     | 140     | 136     | AAW   | Р           |          |
| 5/27/2017 | 9:20 AM  | TT               | MAY  | F    | 2650 | 75          | 7               | 750            | -                | -               | 116<br>120         | 117<br>115         | 114<br>113         | 140     | 136     | 135     | AAW   | Р           |          |
| 5/30/2017 | 8:20 AM  | тт               | May  | F    | 2650 | 70          | 7               | 750            | -                | -               | 110<br>114         | 108<br>100         | 110<br>105         | 139     | 132     | 135     | AAW   | Р           |          |
| 5/30/2017 | 8:10 AM  | тт               | AG   | х    | 211  | 70          | -               | -              | 500              | 550             | 108<br>-           | 102<br>-           | 100                | 133     | 130     | 129     | AAW   | Р           |          |
| 5/30/2017 | 1:00 PM  | TT               | May  | F    | 2650 | 75          | 7               | 750            | -                | -               | 115<br>113         | 110<br>108         | 111<br>107         | 135     | 140     | 132     | AAW   | Р           |          |
| 5/30/2017 | 1:05 PM  | TT               | AG   | х    | 211  | 75          | -               | -              | 450              | 500             | 105<br>-           | 109<br>-           | 108                | 122     | 120     | 120     | AAW   | Р           |          |
| 5/30/2017 | 2:25 PM  | тт               | May  | х    | 60   | 75          | -               | -              | 500              | 500             | 110<br>-           | 112<br>-           | 110<br>-           | 125     | 128     | 125     | AAW   | Р           |          |
| 5/31/2017 | 10:00 AM | TT               | KS   | F    | 45   | 80          | 5               | 850            | -                | -               | 109<br>121         | 112<br>115         | 127<br>120         | 126     | 128     | 126     | AAW   | Р           |          |
| 5/31/2017 | 10:20 AM | тт               | May  | F    | 25   | 80          | 5               | 850            | -                | -               | 118<br>114         | 113<br>120         | 102<br>115         | 128     | 122     | 125     | AAW   | Р           |          |
| 5/31/2017 | 1:00 PM  | TT               | May  | F    | 45   | 80          | 5               | 850            | -                | -               | 110<br>114         | 105<br>105         | 113<br>104         | 120     | 117     | 119     | AAW   | Р           |          |
| 5/31/2017 | 3:10 PM  | тт               | AG   | х    | 211  | 80          | -               | -              | 500              | 550             | -<br>115           | -<br>107           | 104                | 114     | 116     | 113     | AAW   | Р           |          |
| 6/1/2017  | 7:40 AM  | TT               | AG   | Х    | 211  | 70          | -               | -              | 500              | 500             | -<br>104           | -<br>120           | 127                | 140     | 142     | 138     | BJD   | Р           |          |
| 6/1/2017  | 7:45 AM  | TT               | May  | Х    | 60   | 70          | -               | -              | 500              | 500             | -<br>106           | -<br>110           | 108                | 130     | 128     | 138     | BJD   | Р           |          |
| 6/1/2017  | 11:40 AM | TT               | KS   | F    | 45   | 75          | 6               | 850            | -                | -               | 118<br>115         | 114<br>113         | 116<br>115         | 128     | 126     | 126     | BJD   | Р           |          |
| 6/1/2017  | 1:00 PM  | тт               | AG   | Х    | 211  | 75          | -               | -              | 500              | 500             | -<br>101           | -<br>106           | 100                | 115     | 113     | 112     | BJD   | Р           |          |
| 6/1/2017  | 3:40 PM  | TT               | KS   | F    | 45   | 75          | 6               | 850            | -                | -               | 112<br>120         | 109<br>123         | 113<br>120         | 118     | 120     | 120     | BJD   | Р           |          |



| Date     | Time       | Material<br>Type | Tech  | Туре | Mach | Amb<br>Temp | Fusion<br>Speed | Fusion<br>Temp | Extr.<br>Preheat | Extr.<br>Barrel | Peel 1<br>(In/Out) | Peel 2<br>(In/Out) | Peel 3<br>(In/Out) | Shear 1 | Shear 2 | Shear 3 | QA ID | Pass / Fail | Comments |
|----------|------------|------------------|-------|------|------|-------------|-----------------|----------------|------------------|-----------------|--------------------|--------------------|--------------------|---------|---------|---------|-------|-------------|----------|
| 6/1/2017 | 3:35 PM    | TT               | May   | F    | 25   | 75          | 5               | 850            | _                | _               | 103                | 124                | 117                | 125     | 120     | 120     | BJD   | Р           |          |
|          |            |                  | - ' ' |      |      |             |                 |                |                  |                 | 112                | 111                | 120                |         |         |         |       |             |          |
| 6/2/2017 | 7:50 AM    | TT               | May   | х    | 60   | 70          | -               | -              | 500              | 500             | 120                | 115                | 107                | 123     | 120     | 120     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 122                | 100                | 102                |         |         |         |       |             |          |
| 6/2/2017 | 7:47 AM    | TT               | AG    | Х    | 211  | 70          | -               | -              | 550              | 500             | 122                | 108                | 102                | 132     | 135     | 130     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 115                | 108                | 103                |         |         |         |       |             |          |
| 6/2/2017 | 1:15 PM    | TT               | AG    | Х    | 83   | 85          | -               | -              | 550              | 500             | -                  | -                  | -                  | 120     | 108     | 122     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 116                | 118                | 119                |         |         |         |       |             |          |
| 6/3/2017 | 7:15 AM    | TT               | KS    | F    | 45   | 80          | 5               | 850            | -                |                 | 117                | 115                | 114                | 140     | 135     | 142     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 116                | 123                | 122                |         |         |         |       |             |          |
| 6/3/2017 | 7:20 AM    | TT               | CC    | F    | 25   | 80          | 5               | 850            | -                | - '             | 104                | 106                | 116                | 135     | 132     | 132     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 113                | 110                | 106                |         |         |         |       |             |          |
| 6/3/2017 | 9:00 AM    | TT               | AG    | Х    | 83   | 85          | -               | -              | 550              | 500             | -                  | -                  | -                  | 128     | 130     | 125     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 102                | 109                | 106                |         |         |         |       |             |          |
| 6/3/2017 | 1:10 PM    | TT               | SP    | F    | 45   | 90          | 6               | 850            | -                | - '             | 102                | 109                | 101                | 105     | 112     | 109     | BJD   | Р           |          |
| 0/0/001= |            |                  |       | _    |      |             |                 |                |                  |                 | 103                | 112                | 107                |         |         |         |       |             |          |
| 6/3/2017 | 1:12 PM    | TT               | CC    | F    | 25   | 90          | 6               | 850            | -                | - '             | 101                | 105                | 110                | 112     | 110     | 110     | BJD   | Р           |          |
| 6/2/2017 | 4.00.014   |                  |       | .,   | 00   | 00          |                 |                | 550              | 500             | 101                | 103                | 106                | 112     | 111     | 112     | 212   |             |          |
| 6/3/2017 | 1:00 PM    | TT               | AG    | Х    | 83   | 90          | -               | -              | 550              | 500             | -                  | -                  | -                  | 112     | 114     | 112     | BJD   | Р           |          |
| 6/2/2017 | 2 40 514   |                  | 146   | .,   | 42   | 00          |                 |                | 500              | 500             | 112                | 98                 | 116                | 122     | 120     | 122     | 212   |             |          |
| 6/3/2017 | 3:40 PM    | TT               | VS    | Х    | 43   | 90          | -               | -              | 500              | 500             | -                  | -                  | -                  | 122     | 120     | 123     | BJD   | Р           |          |
| 6/6/2017 | 8:00 AM    | TT               | AG    | Х    | 211  | 70          | _               | _              | 550              | 500             | 106                | 118                | 119                | 130     | 126     | 126     | BJD   | Р           |          |
| 0/0/2017 | 8.00 AIVI  | '''              | AG    | ^    | 211  | 70          | -               | -              | 330              | 300             | -                  | -                  | -                  | 130     | 120     | 120     | טנפ   | P           |          |
| 6/6/2017 | 8:30 AM    | TT               | SP    | F    | 25   | 70          | 6               | 850            | -                | _               | 118                | 125                | 121                | 142     | 140     | 140     | BJD   | Р           |          |
| 0/0/2017 | 6.30 AIVI  | '''              | ЭГ    | Г    | 23   | 70          | U               | 630            | _                | _               | 128                | 130                | 126                | 142     | 140     | 140     | BJD   | -           |          |
| 6/6/2017 | 8:40 AM    | TT               | KS    | F    | 45   | 70          | 6               | 850            | _                | _               | 126                | 130                | 128                | 137     | 132     | 130     | BJD   | Р           |          |
| 0/0/2017 | 0.40 AIVI  | ""               | K3    | '    | 43   | 70          | U               | 830            | _                |                 | 123                | 130                | 126                | 137     | 132     | 130     | 5,5   | , ,         |          |
| 6/6/2017 | 1:30 PM    | TT               | AG    | х    | 211  | 80          | _               | _              | 550              | 500             | 130                | 120                | 122                | 134     | 132     | 135     | BJD   | Р           |          |
| 0,0,201, | 2.50 / 111 |                  | 7.0   | ^    |      | 00          |                 |                | 550              | 500             | -                  | -                  | -                  | 154     | 132     | 133     | 232   |             |          |
| 6/6/2017 | 1:35 PM    | TT               | SP    | F    | 25   | 80          | 6               | 850            | _                |                 | 132                | 127                | 130                | 136     | 135     | 135     | BJD   | Р           |          |
| -, -,    |            |                  | Ţ.    |      |      |             |                 |                |                  |                 | 134                | 128                | 129                |         |         |         |       |             |          |
| 6/6/2017 | 1:40 PM    | TT               | KS    | F    | 45   | 80          | 6               | 850            | _                |                 | 129                | 132                | 130                | 138     | 135     | 136     | BJD   | Р           |          |
| -, -, -  |            |                  |       |      |      |             |                 |                |                  |                 | 130                | 131                | 130                |         |         |         | -     |             |          |
| 6/7/2017 | 8:20 AM    | TT               | AG    | Х    | 211  | 80          | -               | -              | 550              | 500             | 118                | 122                | 120                | 120     | 122     | 122     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |       |             |          |
| 6/7/2017 | 12:35 PM   | TT               | AG    | Х    | 112  | 85          | -               | -              | 500              | 500             | 122                | 106                | 115                | 122     | 123     | 120     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |       |             |          |
| 6/7/2017 | 1:45 PM    | TT               | SP    | F    | 25   | 85          | 6               | 850            | -                |                 | 140                | 143                | 125                | 140     | 132     | 136     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 136                | 138                | 126                |         |         |         |       |             |          |
| 6/7/2017 | 4:00 PM    | TT               | KS    | F    | 45   | 85          | 6               | 850            | -                |                 | 123                | 123                | 130                | 140     | 141     | 140     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 126                | 126                | 132                |         |         |         |       |             |          |
| 6/8/2017 | 1:22 PM    | TT               | AG    | F    | 2650 | 80          | 9               | 750            | -                |                 | 125                | 110                | 116                | 120     | 116     | 118     | BJD   | Р           |          |
|          |            |                  |       |      |      |             |                 |                |                  |                 | 106                | 108                | 117                |         |         |         |       |             |          |



| Date      | Time     | Material<br>Type | Tech | Туре | Mach | Amb<br>Temp | Fusion<br>Speed | Fusion<br>Temp | Extr.<br>Preheat | Extr.<br>Barrel | Peel 1<br>(In/Out) | Peel 2<br>(In/Out) | Peel 3<br>(In/Out) | Shear 1 | Shear 2 | Shear 3 | QA ID | Pass / Fail | Comments |
|-----------|----------|------------------|------|------|------|-------------|-----------------|----------------|------------------|-----------------|--------------------|--------------------|--------------------|---------|---------|---------|-------|-------------|----------|
| 6/8/2017  | 4:30 PM  | TT               | SP   | F    | 2479 | 80          | 7               | 750            | -                | -               | 115<br>127         | 122<br>120         | 114<br>128         | 129     | 135     | 126     | BJD   | Р           |          |
| 6/9/2017  | 9:57 AM  | TT               | AG   | F    | 2650 | 80          | 6               | 750            | -                | -               | 124<br>122         | 120<br>114         | 115<br>129         | 141     | 135     | 130     | BJD   | Р           |          |
| 6/9/2017  | 10:19 AM | TT               | SP   | F    | 2479 | 80          | 5               | 755            | -                | -               | 125<br>109         | 115<br>116         | 113<br>110         | 140     | 136     | 139     | BJD   | Р           |          |
| 6/9/2017  | 1:00 PM  | TT               | AG   | F    | 2650 | 85          | 6               | 750            | -                | -               | 127<br>109         | 121<br>117         | 135<br>120         | 139     | 123     | 128     | BJD   | Р           |          |
| 6/9/2017  | 1:07 PM  | TT               | SP   | F    | 2479 | 85          | 6               | 755            | -                | -               | 130<br>119         | 129<br>107         | 126<br>119         | 139     | 127     | 142     | BJD   | Р           |          |
| 6/10/2017 | 7:40 AM  | TT               | SP   | F    | 2479 | 80          | 6               | 755            | -                | -               | 119<br>119<br>137  | 132<br>127         | 122                | 137     | 135     | 130     | BJD   | Р           |          |
| 6/10/2017 | 8:00 AM  | TT               | AG   | F    | 2650 | 80          | 6               | 750            | -                | -               | 129<br>124         | 126<br>124         | 137<br>116         | 153     | 150     | 149     | BJD   | Р           |          |
| 6/10/2017 | 9:53 AM  | TT               | AG   | Х    | 112  | 80          | -               | -              | 400              | 500             | -<br>96            | - 110              | -<br>99            | 133     | 130     | 128     | BJD   | Р           |          |
| 6/10/2017 | 12:56 PM | TT               | AG   | х    | 112  | 85          | -               | -              | 400              | 500             | -<br>98            | -<br>99            | -<br>115           | 119     | 125     | 130     | BJD   | Р           |          |
| 6/10/2017 | 1:08 PM  | TT               | SP   | F    | 45   | 85          | 5               | 850            | -                | -               | 137<br>110         | 138<br>135         | 140<br>129         | 133     | 142     | 140     | BJD   | Р           |          |
| 6/12/2017 | 7:43 AM  | TT               | AG   | х    | 112  | 80          | -               | -              | 400              | 500             | 122                | 137                | - 144              | 154     | 150     | 147     | BJD   | Р           |          |
| 6/12/2017 | 7:50 AM  | TT               | SP   | х    | 2650 | 80          | 6               | 750            | -                | -               | 118<br>129         | 112<br>130         | 124<br>144         | 135     | 130     | 125     | BJD   | Р           |          |
| 6/12/2017 | 8:00 AM  | TT               | СС   | F    | 45   | 80          | 5               | 850            | -                | -               | 115<br>127         | 120<br>125         | 120<br>110         | 135     | 130     | 130     | BJD   | Р           |          |
| 6/12/2017 | 1:06 PM  | TT               | СС   | F    | 45   | 90          | 4               | 850            | -                | -               | 124<br>118         | 124<br>111         | 118<br>110         | 127     | 125     | 130     | BJD   | Р           |          |
| 6/12/2017 | 1:04 PM  | TT               | AG   | х    | 112  | 90          | -               | -              | 400              | 500             | -<br>128           | -<br>112           | -<br>124           | 124     | 125     | 135     | BJD   | Р           |          |
| 6/13/2017 | 7:50 AM  | TT               | СС   | F    | 2650 | 80          | 6               | 750            | -                | -               | 120<br>118         | 114<br>116         | 121<br>116         | 134     | 146     | 133     | BJD   | Р           |          |
| 6/13/2017 | 8:25 AM  | TT               | SP   | F    | 45   | 80          | 4               | 850            | -                | -               | 128<br>112         | 118<br>124         | 114<br>123         | 137     | 133     | 130     | BJD   | Р           |          |
| 6/13/2017 | 10:10 AM | TT               | AG   | Х    | 112  | 80          | -               | -              | 400              | 500             | -<br>119           | -<br>120           | -<br>112           | 127     | 125     | 123     | BJD   | Р           |          |
| 6/13/2017 | 1:34 PM  | TT               | AG   | Х    | 112  | 90          | -               | -              | 400              | 500             | -<br>120           | -<br>123           | -<br>112           | 129     | 123     | 120     | BJD   | Р           |          |
| 6/13/2017 | 1:20 PM  | тт               | SP   | F    | 45   | 90          | 5               | 850            | -                | -               | 126<br>120         | 118<br>116         | 114<br>114         | 130     | 132     | 130     | BJD   | Р           |          |
| 6/14/2017 | 7:30 AM  | TT               | SP   | F    | 45   | 80          | 5               | 850            | -                | -               | 125<br>128         | 120<br>122         | 126<br>123         | 135     | 131     | 136     | BJD   | Р           |          |
| 6/14/2017 | 7:25 AM  | TT               | AG   | Х    | 112  | 80          | -               | -              | 400              | 500             | -<br>96            | -<br>105           | -<br>105           | 135     | 132     | 131     | BJD   | Р           |          |



| Date            | Time      | Material<br>Type | Tech | Туре | Mach | Amb<br>Temp | Fusion<br>Speed | Fusion<br>Temp | Extr.<br>Preheat | Extr.<br>Barrel | Peel 1<br>(In/Out) | Peel 2<br>(In/Out) | Peel 3<br>(In/Out) | Shear 1 | Shear 2 | Shear 3 | QA ID  | Pass / Fail | Comments |
|-----------------|-----------|------------------|------|------|------|-------------|-----------------|----------------|------------------|-----------------|--------------------|--------------------|--------------------|---------|---------|---------|--------|-------------|----------|
| 6/14/2017       | 8:33 AM   | TT               | SP   | F    | 1406 | 80          | 3               | 750            | _                | _               | 120                | 125                | 127                | 149     | 142     | 143     | BJD    | Р           |          |
| 0/14/2017       | 0.55 AIVI | ''               | 31   | r    | 1400 | 80          | 3               | 730            | -                |                 | 125                | 119                | 127                | 149     | 142     | 143     | ыл     | ,           |          |
| 6/14/2017       | 9:10 AM   | TT               | СС   | F    | 45   | 80          | 4               | 850            | _                |                 | 129                | 139                | 134                | 143     | 140     | 144     | BJD    | P           |          |
| -, , -          |           |                  |      |      |      |             |                 |                |                  |                 | 123                | 124                | 125                |         |         |         | 1      |             |          |
| 6/16/2017       | 8:00 AM   | TT               | AG   | х    | 112  | 75          | -               | -              | 400              | 530             | 110                | 109                | 112                | 135     | 132     | 131     | BJV    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |        |             |          |
| 6/16/2017       | 8:05 AM   | TT               | WL   | Х    | 211  | 75          | -               | -              | 500              | 500             | 126                | 131                | 128                | 142     | 140     | 139     | BJV    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |        |             |          |
| 6/16/2017       | 1:08 PM   | TT               | AG   | Х    | 112  | 85          | -               | -              | 400              | 550             | -                  | -                  | -                  | -       | -       | -       | BJV    | F           | Peel     |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | 120                | 114                | 116                |         |         |         |        |             |          |
| 6/16/2017       | 1:18 PM   | TT               | WL   | Х    | 211  | 85          | -               | -              | 500              | 500             | -                  | -                  | -                  | 120     | 115     | 119     | BJV    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |        |             |          |
| 6/16/2017       | 1:30 PM   | TT               | AG   | Х    | 112  | 85          | -               | -              | 400              | 550             | -                  | _                  | -                  | -       | -       | -       | BJV    | F           | Peel     |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | 121                | 127                | 128                |         |         |         |        |             |          |
| 6/16/2017       | 1:50 PM   | TT               | AG   | Х    | 112  | 85          | -               | -              | 400              | 550             | -                  | -                  | -                  | 133     | 123     | 138     | BJV    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | 113                | 107                | 120                |         |         |         |        |             |          |
| 6/19/2017       | 7:42 AM   | TT               | SP   | F    | 45   | 75          | 6               | 85             | -                | - '             | 122                | 117                | 117                | 133     | 125     | 120     | BJV    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | 135                | 139                | 140                |         |         |         |        |             |          |
| 6/19/2017       | 7:46 AM   | TT               | AG   | Х    | 112  | 75          | -               | -              | 450              | 550             | -                  | -                  | -                  | 144     | 140     | 144     | BJV    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | 128                | 137                | 130                |         |         |         |        |             |          |
| 6/19/2017       | 1:18 PM   | TT               | WL   | Х    | 211  | 85          | -               | -              | 500              | 500             | -                  | -                  | -                  | 135     | 135     | 130     | BJV    | Р           |          |
| 6/40/2047       | 4.05.014  |                  | D.C  | v    | 45   | 05          |                 |                | 540              | 550             | 129                | 120                | 123                | 420     | 422     | 424     | 507    |             |          |
| 6/19/2017       | 1:05 PM   | TT               | BS   | Х    | 15   | 85          | -               | -              | 510              | 550             | -                  | -                  | -                  | 130     | 123     | 131     | BJV    | Р           |          |
| 6/10/2017       | 1.12 DM   |                  | 4.6  | v    | 112  | O.F.        |                 |                | 450              | 550             | 121                | 119                | 111                | 126     | 120     | 120     | DIV.   |             |          |
| 6/19/2017       | 1:12 PM   | TT               | AG   | Х    | 112  | 85          | -               | -              | 450              | 550             | -                  | -                  | -                  | 126     | 130     | 129     | BJV    | Р           |          |
| 6/20/2017       | 7.45.484  |                  | 14/1 | v    | 211  | 75          | _               | -              | 500              | 500             | 141                | 140                | 147                | 165     | 165     | 160     | 0.014/ | Р           |          |
| 6/20/2017       | 7:45 AM   | TT               | WL   | Х    | 211  | 75          | -               | -              | 500              | 500             | -                  | -                  | -                  | 105     | 100     | 100     | AAW    | P           |          |
| 6/20/2017       | 8:30 AM   | TT               | AG   | х    | 112  | 75          | -               | _              | 450              | 550             | 140                | 145                | 140                | 160     | 150     | 145     | AAW    | Р           |          |
| 0/20/2017       | 0.30 AIVI | '''              | AG   | ^    | 112  | 75          | _               | _              | 430              | 330             | -                  | -                  | -                  | 100     | 130     | 143     | 77.    | '           |          |
| 6/20/2017       | 8:00 AM   | TT               | BS   | х    | 15   | 75          | _               | _              | 450              | 550             | 146                | 140                | 148                | 162     | 168     | 160     | AAW    | Р           |          |
| 0,20,201,       | 0.007     |                  | 55   | ^    | 15   | ,,          |                 |                | .50              | 330             | -                  | -                  | -                  | 102     | 200     | 200     | 75111  |             |          |
| 6/20/2017       | 12:03 PM  | TT               | BS   | х    | 15   | 80          | -               | -              | 480              | 550             | 125                | 132                | 124                | 132     | 130     | 144     | AAW    | Р           |          |
| 5, = 5, = 5 = 1 |           |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |        |             |          |
| 6/20/2017       | 12:04 PM  | TT               | WL   | х    | 211  | 80          | -               | -              | 500              | 500             | 130                | 132                | 122                | 140     | 145     | 142     | AAW    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |        |             |          |
| 6/20/2017       | 1:05 PM   | TT               | AG   | Х    | 112  | 80          | -               | -              | 500              | 500             | 121                | 120                | 129                | 137     | 135     | 141     | AAW    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         |         |         |        |             |          |
| 6/21/2017       | 7:39 AM   | TT               | SP   | F    | 1406 | 75          | 3               | 750            | -                |                 | 132                | 130                | 129                | 137     | 132     | 135     | AAW    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | 130                | 122                | 135                |         |         |         |        |             |          |
| 6/21/2017       | 8:55 AM   | TT               | СС   | F    | 45   | 90          | 4               | 850            | -                | - 1             | 123                | 124                | 130                | 132     | 130     | 127     | AAW    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | 127                | 129                | 112                |         |         |         |        |             |          |
| 6/21/2017       | 9:52 AM   | TT               | AG   | х    | 211  | 90          | -               | -              | 500              | 550             | 117                | 125                | 120                | 114     | 125     | 127     | AAW    | Р           |          |
|                 |           |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | <u> </u>           |         |         |         |        | I           |          |



#### **Trial Weld Log**

| Date      | Time     | Material<br>Type | Tech | Туре | Mach | Amb<br>Temp | Fusion<br>Speed | Fusion<br>Temp | Extr.<br>Preheat | Extr.<br>Barrel | Peel 1<br>(In/Out) | Peel 2<br>(In/Out) | Peel 3<br>(In/Out) | Shear 1 | Shear 2 | Shear 3 | QA ID | Pass / Fail | Comments |
|-----------|----------|------------------|------|------|------|-------------|-----------------|----------------|------------------|-----------------|--------------------|--------------------|--------------------|---------|---------|---------|-------|-------------|----------|
| 6/21/2017 | 10:40 AM | TT               | SP   | F    | 45   | 90          | 4               | 850            | -                |                 | 117<br>107         | 100<br>119         | 111<br>106         | 115     | 120     | 110     | AAW   | Р           |          |
| 6/21/2017 | 12:50 PM | TT               | AG   | х    | 211  | 90          | -               | -              | 500              | 550             | 118<br>-           | 121<br>-           | 118<br>-           | 120     | 126     | 125     | AAW   | Р           |          |
| 6/22/2017 | 7:30 AM  | TT               | SP   | F    | 45   | 75          | 4               | 850            | -                | -               | 134<br>128         | 127<br>122         | 132<br>125         | 162     | 155     | 155     | AAW   | Р           |          |
| 6/22/2017 | 7:55 AM  | TT               | AG   | х    | 211  | 75          | -               | -              | 500              | 550             | 107                | 125<br>-           | 127                | 140     | 142     | 138     | AAW   | Р           |          |
| 6/22/2017 | 2:00 PM  | TT               | AG   | х    | 211  | 75          | -               | -              | 500              | 550             | 110                | 120                | 122                | 135     | 137     | 136     | AAW   | Р           |          |
| 6/22/2017 | 2:30 PM  | TT               | SP   | F    | 45   | 75          | 4               | 850            | -                | -               | 123<br>125         | 131<br>125         | 134<br>130         | 130     | 125     | 135     | AAW   | Р           |          |
| 6/23/2017 | 9:00 AM  | TT               | AG   | х    | 211  | 70          | -               | -              | 500              | 500             | 126<br>-           | 131<br>-           | 130<br>-           | 142     | 140     | 141     | AAW   | Р           |          |
| 6/23/2017 | 1:30 PM  | TT               | WL   | х    | 15   | 80          | -               | -              | 500              | 450             | 125<br>-           | 123<br>-           | 120<br>-           | 130     | 132     | 130     | AAW   | Р           |          |
| 6/23/2017 | 1:40 PM  | TT               | AG   | х    | 211  | 80          | -               | -              | 500              | 500             | 130                | 135<br>-           | 136<br>-           | 146     | 145     | 142     | AAW   | Р           |          |
| 6/24/2017 | 7:40 AM  | TT               | AG   | х    | 112  | 75          | -               | -              | 500              | 550             | 109<br>-           | 110<br>-           | 106<br>-           | 132     | 135     | 136     | AAW   | Р           |          |
| 6/24/2017 | 7:50 AM  | TT               | WL   | х    | 15   | 75          | -               | -              | 450              | 500             | 106<br>-           | 103<br>-           | 105                | 129     | 133     | 130     | AAW   | Р           |          |
| 6/24/2017 | 1:00 PM  | TT               | AG   | х    | 112  | 75          | -               | -              | 500              | 500             | 122<br>-           | 119<br>-           | 121<br>-           | 135     | 133     | 131     | AAW   | Р           |          |
| 6/24/2017 | 1:05 PM  | TT               | WL   | х    | 15   | 75          | -               | -              | 450              | 500             | 120                | 122<br>-           | 120<br>-           | 132     | 130     | 131     | AAW   | Р           |          |
| 6/26/2017 | 7:40 AM  | TT               | AG   | х    | 112  | 75          | -               | -              | 500              | 500             | 130<br>-           | 110<br>-           | 120<br>-           | 135     | 133     | 136     | AAW   | Р           |          |
| 6/26/2017 | 7:30 AM  | TT               | WL   | х    | 15   | 75          | -               | -              | 450              | 500             | 132<br>-           | 119<br>-           | 126<br>-           | 138     | 135     | 131     | AAW   | Р           |          |
| 6/26/2017 | 1:15 PM  | TT               | AG   | х    | 112  | 75          | -               | -              | 500              | 500             | 102<br>-           | 110<br>-           | 115<br>-           | 130     | 132     | 128     | AAW   | Р           |          |
| 6/26/2017 | 1:20 PM  | TT               | WL   | х    | 15   | 75          | -               | -              | 450              | 500             | 108<br>-           | 112<br>-           | 110<br>-           | 133     | 130     | 130     | AAW   | Р           |          |
| 6/26/2017 | 1:40 PM  | TT               | BS   | х    | 43   | 75          | -               | -              | 500              | 550             | 112<br>-           | 110<br>-           | 111<br>-           | 130     | 130     | 128     | AAW   | Р           |          |
| 6/27/2017 | 7:30 AM  | тт               | WL   | х    | 15   | 70          | -               | -              | 500              | 500             | 114<br>-           | 112<br>-           | 112<br>-           | 132     | 135     | 131     | AAW   | Р           |          |
| 6/27/2017 | 7:40 AM  | тт               | AG   | х    | 112  | 70          | -               | -              | 500              | 500             | 113<br>-           | 112<br>-           | 110<br>-           | 138     | 136     | 132     | AAW   | Р           |          |
| 6/27/2017 | 1:15 PM  | тт               | AG   | х    | 112  | 80          | -               | -              | 500              | 500             | 110<br>-           | 105<br>-           | 112<br>-           | 125     | 123     | 123     | AAW   | Р           |          |
| 6/27/2017 | 1:20 PM  | TT               | WL   | х    | 15   | 80          | -               | -              | 500              | 500             | 115<br>-           | 110<br>-           | 110<br>-           | 125     | 123     | 126     | AAW   | Р           |          |



#### **Trial Weld Log**

| Date           | Time       | Material<br>Type | Tech | Туре | Mach | Amb<br>Temp | Fusion<br>Speed | Fusion<br>Temp | Extr.<br>Preheat | Extr.<br>Barrel | Peel 1<br>(In/Out) | Peel 2<br>(In/Out) | Peel 3<br>(In/Out) | Shear 1 | Shear 2 | Shear 3 | QA ID  | Pass / Fail | Comments |
|----------------|------------|------------------|------|------|------|-------------|-----------------|----------------|------------------|-----------------|--------------------|--------------------|--------------------|---------|---------|---------|--------|-------------|----------|
| 6/28/2017      | 8:15 AM    | TT               | WL   | х    | 15   | 80          | _               | _              | 500              | 500             | 119                | 116                | 111                | 147     | 145     | 140     | AAW    | Р           |          |
| -, -, -, -, -, | 0.120.1    |                  |      |      |      |             |                 |                |                  |                 | -                  | -                  | -                  |         | 2.0     | 1.0     |        |             |          |
| 6/28/2017      | 8:09 AM    | TT               | AG   | х    | 112  | 80          | _               | _              | 500              | 550             | 100                | 118                | 116                | 149     | 150     | 152     | AAW    | P           |          |
| 0,20,201,      | 0.037      |                  | 7.10 | ~    |      | - 00        |                 |                | 500              | 550             | -                  | -                  | -                  | 1.5     | 150     | 132     | 7.0.00 |             |          |
| 6/28/2017      | 1:00 PM    | TT               | BS   | х    | 43   | 80          | _               | _              | 500              | 550             | 100                | 102                | 110                | 145     | 150     | 145     | AAW    | D           |          |
| 0/28/2017      | 1.00 1 101 | "                | 55   | ^    | 43   | 80          | _               | _              | 300              | 330             | -                  | -                  | -                  | 143     | 130     | 143     | AAW    | '           |          |
| 6/29/2017      | 7:50 AM    | TT               | WL   | х    | 15   | 75          | _               | _              | 500              | 500             | 115                | 118                | 120                | 140     | 142     | 140     | AAW    | P           |          |
| 0/23/2017      | 7.50 74141 |                  | ***  | ^    | 13   | ,,          |                 |                | 300              | 300             | -                  | -                  | -                  | 140     | 142     | 140     | 70100  |             |          |
| 6/29/2017      | 1:00 PM    | TT               | WL   | х    | 15   | 80          | _               | _              | 500              | 500             | 110                | 121                | 124                | 138     | 141     | 129     | AAW    | P           |          |
| 0/23/2017      | 1.00 1 101 | "                | WL   | ^    | 13   | 80          | _               | _              | 300              | 300             | -                  | -                  | -                  | 130     | 141     | 123     | AAW    | '           |          |
| 6/30/2017      | 7:17 AM    | TT               | WL   | х    | 112  | 75          | _               | _              | 500              | 500             | 112                | 115                | 115                | 140     | 146     | 152     | AAW    | Р           |          |
| 0/30/2017      | 7.17 AIVI  | ''               | WL   | ^    | 112  | ,,          | _               |                | 500              | 300             | -                  | -                  | -                  | 140     | 140     | 132     | AAVV   | ,           |          |
| 7/1/2017       | 7:15 AM    | TT               | WL   | х    | 112  | 75          | _               | _              | 500              | 500             | 125                | 136                | 131                | 152     | 143     | 151     | AAW    | Р           |          |
| //1/201/       | 7.13 AIVI  | ''               | WL   | ^    | 112  | ,,          | _               | _              | 500              | 300             | -                  | -                  | -                  | 132     | 143     | 131     | AAW    | ļ ,         |          |



#### **Sub-Appendix C.5**

#### **Panel Seaming Forms**

| From | То | Date      | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|----|-----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 1    | 2  | 5/17/2017 | TT               | 7:54 AM    | 76          | SLOPE    | 0                | 84             | X              | 84             |        | AAW   |     |         |          |
| 3    | 4  | 5/17/2017 | TT               | 8:19 AM    | 80          | SLOPE    | 0                | 88             | Χ              | 88             |        | AAW   | 1   | 73      |          |
| 6    | 7  | 5/18/2017 | TT               | 7:45 AM    | 80          | SLOPE    | 9                | 103            | X              | 94             |        | AAW   |     |         |          |
| 8    | 9  | 5/18/2017 | TT               | 8:15 AM    | 81          | SLOPE    | 2                | 103            | Х              | 101            |        | AAW   |     |         |          |
| 12   | 13 | 5/18/2017 | TT               | 8:25 AM    | 81          | SLOPE    | 0                | 16             | Χ              | 16             |        | AAW   |     |         |          |
| 10   | 11 | 5/18/2017 | TT               | 8:38 AM    | 81          | SLOPE    | 5                | 113            | X              | 108            |        | AAW   |     |         |          |
| 14   | 15 | 5/18/2017 | TT               | 8:50 AM    | 81          | SLOPE    | 0                | 108            | Χ              | 108            |        | AAW   | 4   | 107     |          |
| 16   | 17 | 5/18/2017 | TT               | 11:22 AM   | 85          | SLOPE    | 0                | 107            | Χ              | 107            |        | AAW   |     |         |          |
| 17   | 20 | 5/18/2017 | TT               | 1:10 PM    | 87          | SLOPE    | 0                | 107            | Χ              | 107            |        | AAW   |     |         |          |
| 20   | 21 | 5/18/2017 | TT               | 1:30 PM    | 86          | SLOPE    | 0                | 107            | Χ              | 107            |        | AAW   |     |         |          |
| 22   | 23 | 5/18/2017 | TT               | 1:48 PM    | 86          | SLOPE    | 0                | 103            | X              | 103            |        | AAW   |     |         |          |
| 24   | 25 | 5/18/2017 | TT               | 3:20 PM    | 86          | SLOPE    | 0                | 100            | Χ              | 100            |        | AAW   | 5   | 70      |          |
| 25   | 26 | 5/18/2017 | TT               | 3:35 PM    | 86          | SLOPE    | 0                | 45             | Χ              | 45             |        | AAW   |     |         |          |
| 25   | 27 | 5/18/2017 | TT               | 3:45 PM    | 85          | SLOPE    | 0                | 55             | Х              | 55             |        | AAW   |     |         |          |
| 26   | 27 | 5/18/2017 | TT               | 3:54 PM    | 85          | SLOPE    | 0                | 48             | Х              | 48             |        | AAW   |     |         |          |
| 29   | 30 | 5/22/2017 | TT               | 3:21 PM    | 76          | SLOPE    | 0                | 117            |                | 117            |        | AAW   |     |         |          |
| 27   | 29 | 5/22/2017 | TT               | 3:52 PM    | 76          | SLOPE    | 0                | 40             | Х              | 40             |        | AAW   |     |         |          |
| 28   | 29 | 5/22/2017 | TT               | 4:13 PM    | 76          | SLOPE    | 26               | 46             | Х              | 20             |        | AAW   |     |         |          |
| 27   | 28 | 5/22/2017 | TT               | 4:50 PM    | 76          | SLOPE    | 35               | 55             | X              | 20             |        | AAW   | 7   | 44      |          |
| 36   | 37 | 5/23/2017 | TT               | 9:32 AM    | 70          | SLOPE    | 0                | 75             | Х              | 75             |        | AAW   |     |         |          |
| 36   | 38 | 5/23/2017 | TT               | 9:43 AM    | 70          | SLOPE    | 0                | 81             | Х              | 81             |        | AAW   |     |         |          |
| 37   | 39 | 5/23/2017 | TT               | 9:57 AM    | 70          | SLOPE    | 0                | 77             | Х              | 77             |        | AAW   |     |         |          |
| 41   | 42 | 5/24/2017 | TT               | 9:46 AM    | 62          | SLOPE    | 0                | 127            | Х              | 127            |        | AAW   |     |         |          |
| 44   | 45 | 5/24/2017 | TT               | 10:32 AM   | 62          | SLOPE    | 0                | 8              |                | 8              |        | AAW   |     |         |          |
| 44   | 45 | 5/24/2017 | TT               | -          | -           | SLOPE    | 8                | 16             | X              | 8              | Х      | AAW   |     |         |          |
| 43   | 46 | 5/24/2017 | TT               | 10:50 AM   | 62          | SLOPE    | 0                | 15             | X              | 15             |        | AAW   |     |         |          |
| 42   | 46 | 5/24/2017 | TT               | 10:52 AM   | 62          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |     |         |          |
| 41   | 43 | 5/24/2017 | TT               | 10:53 AM   | 62          | SLOPE    | 0                | 24             |                | 24             |        | AAW   |     |         |          |
| 41   | 43 | 5/24/2017 | TT               | -          | -           | SLOPE    | 24               | 26             | X              | 2              | Х      | AAW   |     |         |          |
| 45   | 46 | 5/24/2017 | TT               | 10:59 AM   | 62          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |          |
| 47   | 48 | 5/24/2017 | TT               | 11:21 AM   | 62          | SLOPE    | 0                | 103            | Х              | 103            |        | AAW   | 10  | 53      |          |
| 49   | 50 | 5/24/2017 | TT               | 12:43 PM   | 69          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 48   | 50 | 5/24/2017 | TT               | 12:48 PM   | 69          | SLOPE    | 0                | 23             | Х              | 23             |        | AAW   |     |         |          |
| 49   | 51 | 5/24/2017 | TT               | 12:52 PM   | 69          | SLOPE    | 0                | 29             | Х              | 29             |        | AAW   |     |         |          |
| 50   | 51 | 5/24/2017 | TT               | 12:55 PM   | 69          | SLOPE    | 0                | 9              | Х              | 9              |        | AAW   | 11  | 9       |          |
| 53   | 54 | 5/25/2017 | TT               | 7:29 AM    | 59          | SLOPE    | 0                | 73             | X              | 73             |        | AAW   |     |         |          |
| 55   | 56 | 5/25/2017 | TT               | 7:48 AM    | 59          | SLOPE    | 0                | 113            | Χ              | 113            |        | AAW   |     |         |          |



| From | То  | Date      | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS#     | DS Sta. | Comments |
|------|-----|-----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|---------|---------|----------|
| 57   | 58  | 5/25/2017 | TT               | 8:07 AM    | 59          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |         |         |          |
| 57   | 59  | 5/25/2017 | TT               | 8:11 AM    | 59          | SLOPE    | 0                | 58             | Х              | 58             |        | AAW   |         |         |          |
| 58   | 59  | 5/25/2017 | TT               | 8:20 AM    | 59          | SLOPE    | 0                | 59             | Х              | 59             |        | AAW   |         |         |          |
| 60   | 61  | 5/25/2017 | TT               | 8:32 AM    | 60          | SLOPE    | 0                | 125            | Х              | 125            |        | AAW   |         |         |          |
| 62   | 63  | 5/25/2017 | TT               | 9:09 AM    | 60          | SLOPE    | 0                | 124            | Х              | 124            |        | AAW   | 14      | 2       |          |
| 63   | 65  | 5/25/2017 | TT               | 9:28 AM    | 60          | SLOPE    | 0                | 10             | Х              | 10             |        | AAW   |         |         |          |
| 64   | 66  | 5/25/2017 | TT               | 9:40 AM    | 61          | SLOPE    | 0                | 138            |                | 138            |        | AAW   |         |         |          |
| 68   | 69  | 5/25/2017 | TT               | 2:01 PM    | 80          | SLOPE    | 0                | 35             | Х              | 35             |        | AAW   |         |         |          |
| 66   | 67  | 5/25/2017 | TT               | 2:05 PM    | 80          | SLOPE    | 120              | 135            | Х              | 15             |        | AAW   |         |         |          |
| 66   | 70  | 5/25/2017 | TT               | 2:10 PM    | 80          | SLOPE    | 0                | 2              | Х              | 2              |        | AAW   |         |         |          |
| 67   | 70  | 5/25/2017 | TT               | 2:20 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |         |         |          |
| 69   | 70  | 5/25/2017 | TT               | 2:27 PM    | 80          | SLOPE    | 0                | 50             | Х              | 50             |        | AAW   |         |         |          |
| 71   | 73  | 5/25/2017 | TT               | 2:55 PM    | 80          | SLOPE    | 0                | 34             |                | 34             |        | AAW   |         |         |          |
| 71   | 73  | 5/25/2017 | TT               | -          | -           | SLOPE    | 34               | 36             |                | 2              | Х      | AAW   |         |         |          |
| 71   | 73  | 5/25/2017 | TT               | 3:03 PM    | 80          | SLOPE    | 36               | 138            | Х              | 102            |        | AAW   | 16      | 108     |          |
| 72   | 73  | 5/25/2017 | TT               | 3:17 PM    | 80          | SLOPE    | 0                | 33             | Х              | 33             |        | AAW   |         |         |          |
| 73   | 74  | 5/25/2017 | TT               | 3:34 PM    | 80          | SLOPE    | 0                | 63             | Х              | 63             |        | AAW   |         |         |          |
| 74   | 75  | 5/25/2017 | TT               | 3:46 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |         |         |          |
| 73   | 75  | 5/25/2017 | TT               | 3:50 PM    | 80          | SLOPE    | 0                | 86             | Х              | 86             |        | AAW   |         |         |          |
| 61   | 65  | 5/25/2017 | TT               | -          | -           | SLOPE    | 0                | 3              | Х              | 3              | Х      | AAW   |         |         |          |
| 77   | 78  | 5/26/2017 | TT               | 9:08 AM    | 70          | SLOPE    | 0                | 77             | Х              | 77             |        | AAW   |         |         |          |
| 78   | 79  | 5/26/2017 | TT               | 9:23 AM    | 70          | SLOPE    | 0                | 55             | Х              | 50             |        | AAW   |         |         |          |
| 79   | 80  | 5/26/2017 | TT               | 9:32 AM    | 70          | SLOPE    | 0                | 26             | Х              | 26             |        | AAW   |         |         |          |
| 81   | 82  | 5/31/2017 | TT               | 10:22 AM   | 80          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |         |         |          |
| 82   | 83  | 5/31/2017 | TT               | 10:14 AM   | 80          | SLOPE    | 0                | 38             | Х              | 38             |        | AAW   |         |         |          |
| 83   | 84  | 5/31/2017 | TT               | 10:29 AM   | 80          | SLOPE    | 0                | 47             | Х              | 47             |        | AAW   |         |         |          |
| 84   | 85  | 5/31/2017 | TT               | 10:47 AM   | 80          | SLOPE    | 0                | 59             | Х              | 59             |        | AAW   | 19      | 4       |          |
| 87   | 88  | 5/31/2017 | TT               | 10:58 AM   | 80          | SLOPE    | 0                | 87             | Х              | 87             |        | AAW   |         |         |          |
| 96   | 97  | 6/1/2017  | TT               | 11:46 AM   | 78          | SLOPE    | 0                | 9              |                | 9              |        | BJD   |         |         |          |
| 96   | 97  | 6/1/2017  | TT               | 11:49 AM   | 78          | SLOPE    | 11               | 162            |                | 151            |        | BJD   |         |         |          |
| 96   | 97  | 6/1/2017  | TT               | 12:10 PM   | 80          | SLOPE    | 163              | 170            | Х              | 7              |        | BJD   |         |         |          |
| 98   | 99  | 6/1/2017  | TT               | 12:58 PM   | 82          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |         |         |          |
| 97   | 98  | 6/1/2017  | TT               | 1:02 PM    | 82          | SLOPE    | 0                | 6              |                | 6              |        | BJD   |         |         |          |
| 97   | 98  | 6/1/2017  | TT               | 1:05 PM    | 82          | SLOPE    | 7                | 45             | Х              | 38             |        | BJD   |         |         |          |
| 97   | 99  | 6/1/2017  | TT               | 1:09 PM    | 82          | SLOPE    | 0                | 22             |                | 22             |        | BJD   |         |         |          |
| 97   | 99  | 6/1/2017  | TT               | 1:13 PM    | 82          | SLOPE    | 24               | 126            | Х              | 102            |        | BJD   | 23B     | 123     |          |
| 100  | 101 | 6/1/2017  | TT               | 3:44 PM    | 81          | SLOPE    | 0                | 174            | Х              | 174            |        | BJD   | 23, 23A | 7, 17   |          |



| From | То  | Date     | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 103  | 105 | 6/1/2017 | TT               | 4:59 PM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 104  | 105 | 6/1/2017 | TT               | 5:03 PM    | 77          | SLOPE    | 0                | 91             |                | 91             |        | BJD   |     |         |          |
| 104  | 105 | 6/1/2017 | TT               | 5:24 PM    | 77          | SLOPE    | 94               | 111            | Х              | 37             |        | BJD   |     |         |          |
| 106  | 107 | 6/1/2017 | TT               | 6:15 PM    | 77          | SLOPE    | 0                | 52             | Х              | 52             |        | BJD   |     |         |          |
| 108  | 109 | 6/1/2017 | TT               | 6:20 PM    | 75          | SLOPE    | 0                | 129            | Х              | 129            |        | BJD   |     |         |          |
| 107  | 109 | 6/1/2017 | TT               | 6:24 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   | 25  | 8       |          |
| 23   | 107 | 6/1/2017 | TT               | 6:40 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 24   | 106 | 6/1/2017 | TT               | 6:44 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 31   | 102 | 6/1/2017 | TT               | 6:47 PM    | 75          | SLOPE    | 0                | 18             | Х              | 18             |        | BJD   |     |         |          |
| 32   | 101 | 6/1/2017 | TT               | 6:49 PM    | 73          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 29   | 101 | 6/1/2017 | TT               | 6:50 PM    | 73          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 29   | 100 | 6/1/2017 | TT               | 6:51 PM    | 73          | SLOPE    | 0                | 7              | Х              | 7              |        | BJD   |     |         |          |
| 30   | 100 | 6/1/2017 | TT               | 6:52 PM    | 73          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 30   | 99  | 6/1/2017 | TT               | 6:53 PM    | 73          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 33   | 99  | 6/1/2017 | TT               | 6:54 PM    | 72          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 33   | 97  | 6/1/2017 | TT               | 6:56 PM    | 72          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 34   | 97  | 6/1/2017 | TT               | 6:57 PM    | 72          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 34   | 96  | 6/1/2017 | TT               | 6:58 PM    | 72          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 111  | 112 | 6/3/2017 | TT               | 8:15 AM    | 85          | SLOPE    | 0                | 66             | Х              | 66             |        | BJD   |     |         |          |
| 113  | 114 | 6/3/2017 | TT               | 8:30 AM    | 85          | SLOPE    | 0                | 64             | Х              | 64             |        | BJD   |     |         |          |
| 115  | 116 | 6/3/2017 | TT               | 8:54 AM    | 85          | SLOPE    | 0                | 67             | Х              | 67             |        | BJD   |     |         |          |
| 117  | 118 | 6/3/2017 | TT               | 9:00 AM    | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 118  | 119 | 6/3/2017 | TT               | 9:05 AM    | 85          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 117  | 119 | 6/3/2017 | TT               | 9:06 AM    | 85          | SLOPE    | 0                | 61             | Х              | 61             |        | BJD   |     |         |          |
| 120  | 121 | 6/3/2017 | TT               | 9:20 AM    | 85          | SLOPE    | 0                | 61             |                | 61             |        | BJD   |     |         |          |
| 120  | 121 | 6/3/2017 | TT               | 9:26 AM    | 85          | SLOPE    | 63               | 66             | Х              | 3              |        | BJD   |     |         |          |
| 121  | 122 | 6/3/2017 | TT               | 9:30 AM    | 85          | SLOPE    | 0                | 66             | Х              | 66             |        | BJD   | 26  | 22      |          |
| 123  | 124 | 6/3/2017 | TT               | 9:42 AM    | 85          | SLOPE    | 0                | 66             | Х              | 66             |        | BJD   |     |         |          |
| 125  | 126 | 6/3/2017 | TT               | 10:02 AM   | 85          | SLOPE    | 0                | 63             | Х              | 63             |        | BJD   |     |         |          |
| 126  | 128 | 6/3/2017 | TT               | 10:20 AM   | 85          | SLOPE    | 0                | 22             | Х              | 22             |        | BJD   |     |         |          |
| 127  | 129 | 6/3/2017 | TT               | 10:30 AM   | 88          | SLOPE    | 0                | 56             | Х              | 56             |        | BJD   |     |         |          |
| 129  | 130 | 6/3/2017 | TT               | 10:45 AM   | 88          | SLOPE    | 0                | 15             |                | 15             |        | BJD   |     |         |          |
| 129  | 130 | 6/3/2017 | TT               | 10:55 AM   | 88          | SLOPE    | 18               | 53             | Х              | 35             |        | BJD   |     |         |          |
| 131  | 132 | 6/3/2017 | TT               | 11:10 AM   | 88          | SLOPE    | 0                | 54             | Х              | 54             |        | BJD   |     |         |          |
| 145  | 146 | 6/6/2017 | TT               | 2:12 PM    | 83          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 144  | 145 | 6/6/2017 | TT               | 2:24 PM    | 83          | SLOPE    | 0                | 32             | Х              | 32             |        | BJD   |     |         |          |
| 144  | 146 | 6/6/2017 | TT               | 2:29 PM    | 83          | SLOPE    | 0                | 151            | Х              | 151            |        | BJD   | 28  | 97      |          |



| From | То  | Date     | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 147  | 148 | 6/6/2017 | TT               | 2:52 PM    | 83          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 148  | 149 | 6/6/2017 | TT               | 3:21 PM    | 83          | SLOPE    | 0                | 22             | Х              | 22             |        | BJD   |     |         |          |
| 150  | 151 | 6/6/2017 | TT               | 3:27 PM    | 83          | SLOPE    | 0                | 33             | Х              | 33             |        | BJD   |     |         |          |
| 149  | 150 | 6/6/2017 | TT               | 3:30 PM    | 83          | SLOPE    | 0                | 18             | Х              | 18             |        | BJD   |     |         |          |
| 153  | 154 | 6/6/2017 | TT               | 3:56 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| PE1  | PE2 | 6/6/2017 | TT               | 4:09 PM    | 80          | SLOPE    | 0                | 12             | Х              | 12             |        | BJD   |     |         |          |
| 151  | PE1 | 6/6/2017 | TT               | 4:17 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 150  | PE2 | 6/6/2017 | TT               | 4:26 PM    | 80          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 149  | PE2 | 6/6/2017 | TT               | 4:28 PM    | 80          | SLOPE    | 0                | 10             | Х              | 10             |        | BJD   |     |         |          |
| 147  | 151 | 6/6/2017 | TT               | 4:40 PM    | 80          | SLOPE    | 0                | 29             | Х              | 29             |        | BJD   |     |         |          |
| 147  | 152 | 6/6/2017 | TT               | 4:47 PM    | 80          | SLOPE    | 0                | 37             | Х              | 37             |        | BJD   |     |         |          |
| 151  | 152 | 6/6/2017 | TT               | 4:52 PM    | 80          | SLOPE    | 0                | 87             | Х              | 87             |        | BJD   |     |         |          |
| 9    | 155 | 6/6/2017 | TT               | 5:07 PM    | 80          | SLOPE    | 0                | 4              | Х              | 4              |        | BJD   |     |         |          |
| 10   | 155 | 6/6/2017 | TT               | 5:08 PM    | 80          | SLOPE    | 0                | 12             | Х              | 12             |        | BJD   |     |         |          |
| 10   | 154 | 6/6/2017 | TT               | 5:09 PM    | 80          | SLOPE    | 0                | 3              | Χ              | 3              |        | BJD   |     |         |          |
| 11   | 154 | 6/6/2017 | TT               | 5:09 PM    | 80          | SLOPE    | 0                | 12             | Χ              | 12             |        | BJD   |     |         |          |
| 11   | 152 | 6/6/2017 | TT               | 5:11 PM    | 80          | SLOPE    | 0                | 3              | Х              | 3              |        | BJD   |     |         |          |
| 13   | 152 | 6/6/2017 | TT               | 5:12 PM    | 80          | SLOPE    | 0                | 14             | Χ              | 14             |        | BJD   |     |         |          |
| 14   | 151 | 6/6/2017 | TT               | 5:14 PM    | 80          | SLOPE    | 0                | 14             | Χ              | 14             |        | BJD   |     |         |          |
| 15   | 150 | 6/6/2017 | TT               | 5:17 PM    | 80          | SLOPE    | 0                | 15             | Χ              | 15             |        | BJD   |     |         |          |
| 16   | 149 | 6/6/2017 | TT               | 5:19 PM    | 80          | SLOPE    | 0                | 14             | Х              | 14             |        | BJD   |     |         |          |
| 17   | 148 | 6/6/2017 | TT               | 5:22 PM    | 80          | SLOPE    | 0                | 15             | Χ              | 15             |        | BJD   |     |         |          |
| 20   | 146 | 6/6/2017 | TT               | 5:24 PM    | 80          | SLOPE    | 0                | 14             | Χ              | 14             |        | BJD   |     |         |          |
| 21   | 144 | 6/6/2017 | TT               | 5:27 PM    | 80          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |          |
| 22   | 143 | 6/6/2017 | TT               | 5:29 PM    | 80          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   | 30  | 14      |          |
| 160  | 161 | 6/7/2017 | TT               | 4:42 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 160  | 162 | 6/7/2017 | TT               | 4:50 PM    | 80          | SLOPE    | 0                | 163            |                | 163            |        | BJD   |     |         |          |
| 160  | 162 | 6/7/2017 | TT               | 5:21 PM    | 80          | SLOPE    | 169              | 217            | Х              | 48             |        | BJD   |     |         |          |
| 161  | 162 | 6/7/2017 | TT               | 5:29 PM    | 80          | SLOPE    | 0                | 12             | Х              | 12             |        | BJD   |     |         |          |
| 162  | 163 | 6/7/2017 | TT               | 5:36 PM    | 80          | SLOPE    | 0                | 55             |                | 55             |        | BJD   |     |         |          |
| 162  | 163 | 6/7/2017 | TT               | 5:46 PM    | 80          | SLOPE    | 57               | 209            | Х              | 152            |        | BJD   |     |         |          |



| From | То | Date      | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|----|-----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 2    | 3  | 5/17/2017 | TT               | 8:00 AM    | 76          | SLOPE    | 0                | 85             | Х              | 85             |        | AAW   |     |         |          |
| 4    | 5  | 5/17/2017 | TT               | 8:20 AM    | 80          | SLOPE    | 0                | 92             | х              | 92             |        | AAW   |     |         |          |
| 5    | 6  | 5/17/2017 | TT               | 8:38 AM    | 80          | SLOPE    | 0                | 96             | Х              | 96             |        | AAW   | 2   | 93      |          |
| 7    | 8  | 5/18/2017 | TT               | 7:50 AM    | 80          | SLOPE    | 7                | 109            | х              | 102            |        | AAW   |     |         |          |
| 9    | 10 | 5/18/2017 | TT               | 8:13 AM    | 81          | SLOPE    | 4                | 108            | Х              | 104            |        | AAW   |     |         |          |
| 11   | 12 | 5/18/2017 | TT               | 8:30 AM    | 81          | SLOPE    | 0                | 32             | х              | 32             |        | AAW   |     |         |          |
| 11   | 13 | 5/18/2017 | TT               | 8:35 AM    | 81          | SLOPE    | 0                | 79             | Х              | 79             |        | AAW   |     |         |          |
| 12   | 14 | 5/18/2017 | TT               | 8:50 AM    | 81          | SLOPE    | 0                | 32             | Х              | 32             |        | AAW   |     |         |          |
| 13   | 14 | 5/18/2017 | TT               | 8:54 AM    | 81          | SLOPE    | 0                | 78             | Х              | 78             |        | AAW   | 3   | 77      |          |
| 15   | 16 | 5/18/2017 | TT               | 11:21 AM   | 85          | SLOPE    | 0                | 108            | Х              | 108            |        | AAW   |     |         |          |
| 18   | 19 | 5/18/2017 | TT               | 1:05 PM    | 87          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 18   | 1  | 5/18/2017 | TT               | 1:10 PM    | 87          | SLOPE    | 0                | 60             | Х              | 60             |        | AAW   |     |         |          |
| 19   | 1  | 5/18/2017 | TT               | 1:15 PM    | 87          | SLOPE    | 0                | 23             | Х              | 23             |        | AAW   |     |         |          |
| 21   | 22 | 5/18/2017 | TT               | 1:55 PM    | 86          | SLOPE    | 0                | 106            | х              | 106            |        | AAW   |     |         |          |
| 23   | 24 | 5/18/2017 | TT               | 2:04 PM    | 86          | SLOPE    | 0                | 99             | х              | 99             |        | AAW   | 6   | 97      |          |
| 27   | 28 | 5/22/2017 | TT               | 3:35 PM    | 76          | SLOPE    | 0                | 31             |                | 31             |        | AAW   |     |         |          |
| 28   | 31 | 5/22/2017 | TT               | 3:51 PM    | 76          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 27   | 31 | 5/22/2017 | TT               | 3:56 PM    | 76          | SLOPE    | 0                | 13             | Х              | 13             |        | AAW   |     |         |          |
| 27   | 28 | 5/22/2017 | TT               | -          | -           | SLOPE    | 31               | 35             |                | 4              | Х      | AAW   |     |         |          |
| 31   | 32 | 5/22/2017 | TT               | 4:00 PM    | 76          | SLOPE    | 0                | 19             | Х              | 19             |        | AAW   |     |         |          |
| 28   | 32 | 5/22/2017 | TT               | 4:03 PM    | 76          | SLOPE    | 0                | 10             | Х              | 10             |        | AAW   |     |         |          |
| 32   | 29 | 5/22/2017 | TT               | 4:11 PM    | 76          | SLOPE    | 0                | 27             | Х              | 27             |        | AAW   |     |         |          |
| 28   | 29 | 5/22/2017 | TT               | 4:24 PM    | 76          | SLOPE    | 0                | 26             |                | 26             |        | AAW   |     |         |          |
| 30   | 33 | 5/22/2017 | TT               | 4:30 PM    | 75          | SLOPE    | 0                | 135            | Х              | 135            |        | AAW   |     |         |          |
| 34   | 35 | 5/22/2017 | TT               | 4:55 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 33   | 34 | 5/22/2017 | TT               | 5:00 PM    | 75          | SLOPE    | 0                | 86             | Х              | 86             |        | AAW   |     |         |          |
| 33   | 35 | 5/22/2017 | TT               | 5:15 PM    | 75          | SLOPE    | 0                | 56             | Х              | 56             |        | AAW   |     |         |          |
| 34   | 36 | 5/22/2017 | TT               | 5:35 PM    | 75          | SLOPE    | 0                | 87             | Х              | 87             |        | AAW   | 8   | 2       |          |
| 35   | 36 | 5/22/2017 | TT               | 5:50 PM    | 74          | SLOPE    | 0                | 61             | Х              | 61             |        | AAW   |     |         |          |
| 37   | 38 | 5/23/2017 | TT               | 9:48 AM    | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 38   | 39 | 5/23/2017 | TT               | 9:53 AM    | 70          | SLOPE    | 0                | 74             | Х              | 74             |        | AAW   |     |         |          |
| 39   | 40 | 5/24/2017 | TT               | 9:05 AM    | 61          | SLOPE    | 0                | 151            | Х              | 151            |        | AAW   |     |         |          |
| 40   | 41 | 5/24/2017 | TT               | 9:33 AM    | 61          | SLOPE    | 0                | 157            | Х              | 157            |        | AAW   | 9   | 107     |          |
| 42   | 45 | 5/24/2017 | TT               | 10:30 AM   | 62          | SLOPE    | 0                | 57             | Х              | 57             |        | AAW   |     |         |          |
| 42   | 44 | 5/24/2017 | TT               | 10:40 AM   | 62          | SLOPE    | 0                | 73             | Х              | 73             |        | AAW   |     |         |          |
| 45   | 47 | 5/24/2017 | TT               | 11:00 AM   | 62          | SLOPE    | 0                | 50             | Х              | 50             |        | AAW   |     |         |          |



| From | То | Date      | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|----|-----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 44   | 47 | 5/24/2017 | TT               | -          | -           | SLOPE    | 0                | 9              |                |                | Х      | AAW   |     |         |          |
| 44   | 47 | 5/24/2017 | TT               | 11:11 AM   | 62          | SLOPE    | 9                | 79             | Х              | 70             |        | AAW   |     |         |          |
| 48   | 49 | 5/24/2017 | TT               | 11:30 AM   | 62          | SLOPE    | 0                | 52             | Х              | 52             |        | AAW   | 12  | 2       |          |
| 52   | 53 | 5/25/2017 | TT               | 7:30 AM    | 59          | SLOPE    | 0                | 30             | Х              | 30             |        | AAW   |     |         |          |
| 54   | 55 | 5/25/2017 | TT               | 7:40 AM    | 59          | SLOPE    | 0                | 107            | Х              | 107            |        | AAW   |     |         |          |
| 56   | 57 | 5/25/2017 | TT               | 8:06 AM    | 59          | SLOPE    | 0                | 59             | Х              | 59             |        | AAW   |     |         |          |
| 56   | 58 | 5/25/2017 | TT               | 8:17 AM    | 59          | SLOPE    | 0                | 57             | Х              | 57             |        | AAW   |     |         |          |
| 59   | 60 | 5/25/2017 | TT               | 8:42 AM    | 59          | SLOPE    | 0                | 123            | Х              | 123            |        | AAW   |     |         |          |
| 61   | 62 | 5/25/2017 | TT               | 9:00 AM    | 60          | SLOPE    | 0                | 125            | Х              | 125            |        | AAW   | 13  | 70      |          |
| 62   | 65 | 5/25/2017 | TT               | 9:21 AM    | 60          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 63   | 64 | 5/25/2017 | TT               | 9:35 AM    | 60          | SLOPE    | 0                | 136            | Х              | 136            |        | AAW   |     |         |          |
| 66   | 67 | 5/25/2017 | TT               | 10:00 AM   | 61          | SLOPE    | 0                | 120            |                | 120            |        | AAW   |     |         |          |
| 43   | 63 | 5/25/2017 | TT               | 11:00 AM   | 62          | SLOPE    | 0                | 11             | Х              | 11             |        | AAW   |     |         |          |
| 43   | 65 | 5/25/2017 | TT               | 11:03 AM   | 62          | SLOPE    | 0                | 10             | Х              | 10             |        | AAW   |     |         |          |
| 46   | 65 | 5/25/2017 | TT               | 11:04 AM   | 62          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |     |         |          |
| 46   | 62 | 5/25/2017 | TT               | 11:04 AM   | 62          | SLOPE    | 0                | 2              | Х              | 2              |        | AAW   |     |         |          |
| 46   | 61 | 5/25/2017 | TT               | 11:05 AM   | 62          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 45   | 61 | 5/25/2017 | TT               | 11:06 AM   | 62          | SLOPE    | 0                | 0.5            | Х              | 0.5            |        | AAW   |     |         |          |
| 45   | 60 | 5/25/2017 | TT               | 11:07 AM   | 62          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |     |         |          |
| 47   | 60 | 5/25/2017 | TT               | 11:09 AM   | 62          | SLOPE    | 0                | 9              | Х              | 9              |        | AAW   |     |         |          |
| 47   | 59 | 5/25/2017 | TT               | 11:10 AM   | 62          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |          |
| 47   | 58 | 5/25/2017 | TT               | 11:12 AM   | 62          | SLOPE    | 0                | 10             | Х              | 10             |        | AAW   |     |         |          |
| 48   | 58 | 5/25/2017 | TT               | 11:14 AM   | 62          | SLOPE    | 0                | 7              | Х              | 7              |        | AAW   |     |         |          |
| 48   | 56 | 5/25/2017 | TT               | 11:16 AM   | 62          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |          |
| 48   | 55 | 5/25/2017 | TT               | 11:20 AM   | 62          | SLOPE    | 0                | 10             | Х              | 10             |        | AAW   |     |         |          |
| 49   | 55 | 5/25/2017 | TT               | 11:25 AM   | 62          | SLOPE    | 0                | 9              | Х              | 9              |        | AAW   |     |         |          |
| 49   | 54 | 5/25/2017 | TT               | 11:26 AM   | 62          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |          |
| 51   | 54 | 5/25/2017 | TT               | 11:30 AM   | 62          | SLOPE    | 0                | 15             | Х              | 15             |        | AAW   |     |         |          |
| 51   | 53 | 5/25/2017 | TT               | 11:32 AM   | 62          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 51   | 52 | 5/25/2017 | TT               | 11:36 AM   | 62          | SLOPE    | 0                | 9              |                | 9              |        | AAW   |     |         |          |
| 51   | 52 | 5/25/2017 | TT               | -          | -           | SLOPE    | 9                | 14             | Х              | 5              | Х      | AAW   |     |         |          |
| 66   | 69 | 5/25/2017 | TT               | 2:19 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 64   | 68 | 5/25/2017 | TT               | 2:24 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 41   | 63 | 5/25/2017 | TT               | 2:26 PM    | 80          | SLOPE    | 0                | 9              | Х              | 9              |        | AAW   |     |         |          |
| 67   | 71 | 5/25/2017 | TT               | 2:36 PM    | 80          | SLOPE    | 0                | 135            | Х              | 135            |        | AAW   |     |         |          |
| 70   | 71 | 5/25/2017 | TT               | -          | -           | SLOPE    | 0                | 3              | Х              | 3              | Х      | AAW   |     |         |          |



| From | То | Date      | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS#    | DS Sta. | Comments |
|------|----|-----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|--------|---------|----------|
| 71   | 72 | 5/25/2017 | TT               | 3:04 PM    | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   | 15     | 16      |          |
| 70   | 72 | 5/25/2017 | TT               | 3:15 PM    | 80          | SLOPE    | 0                | 52             | Х              | 52             |        | AAW   |        |         |          |
| 38   | 69 | 5/25/2017 | TT               | 3:48 PM    | 80          | SLOPE    | 0                | 10             | Х              | 10             |        | AAW   |        |         |          |
| 39   | 69 | 5/25/2017 | TT               | -          | -           | SLOPE    | 0                | 5              |                | 5              | Х      | AAW   |        |         |          |
| 39   | 69 | 5/25/2017 | TT               | 3:50 PM    | 80          | SLOPE    | 5                | 11             | Х              | 6              |        | AAW   |        |         |          |
| 39   | 68 | 5/25/2017 | TT               | -          | -           | SLOPE    | 0                | 7              | Х              | 7              | Х      | AAW   |        |         |          |
| 40   | 68 | 5/25/2017 | TT               | 3:54 PM    | 80          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |        |         |          |
| 41   | 68 | 5/25/2017 | TT               | 3:57 PM    | 80          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |        |         |          |
| 74   | 76 | 5/25/2017 | TT               | 4:02 PM    | 80          | SLOPE    | 0                | 62             | Х              | 62             |        | AAW   |        |         |          |
| 75   | 76 | 5/25/2017 | TT               | 4:12 PM    | 80          | SLOPE    | 0                | 62             | Х              | 62             |        | AAW   |        |         |          |
| 76   | 77 | 5/25/2017 | TT               | 4:30 PM    | 80          | SLOPE    | 0                | 100            | Х              | 100            |        | AAW   |        |         |          |
| 5    | WT | 5/27/2017 | TT               | 9:20 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 4    | WT | 5/27/2017 | TT               | 9:23 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 3    | WT | 5/27/2017 | TT               | 9:25 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 2    | WT | 5/27/2017 | TT               | 9:28 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 1    | WT | 5/27/2017 | TT               | 9:29 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 18   | WT | 5/27/2017 | TT               | 9:32 AM    | 78          | SLOPE    | 0                | 9              |                | 9              |        | AAW   |        |         |          |
| 18   | WT | 5/27/2017 | TT               | -          | -           | SLOPE    | 9                | 11             | Х              | 2              |        | AAW   |        |         |          |
| 15   | WT | 5/27/2017 | TT               | -          | -           | SLOPE    | 0                | 5              |                | 5              | Х      | AAW   |        |         |          |
| 15   | WT | 5/27/2017 | TT               | 9:41 AM    | 78          | SLOPE    | 5                | 16             | Х              | 11             | Х      | AAW   |        |         |          |
| 14   | WT | 5/27/2017 | TT               | 9:50 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 12   | WT | 5/27/2017 | TT               | 9:54 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 11   | WT | 5/27/2017 | TT               | 9:57 AM    | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   | 17B2   | 11      |          |
| 10   | WT | 5/27/2017 | TT               | 10:00 AM   | 78          | SLOPE    | 0                | 16             | Х              | 16             | Х      | AAW   | 17,17B | 15, 5   |          |
| 9    | WT | 5/27/2017 | TT               | 10:03 AM   | 78          | SLOPE    | 0                | 16             | Х              | 16             | Х      | AAW   | 17A    | 9       |          |
| 8    | WT | 5/27/2017 | TT               | 10:06 AM   | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   | 17A2   | 3       |          |
| 7    | WT | 5/27/2017 | TT               | 10:10 AM   | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 6    | WT | 5/27/2017 | TT               | -          | -           | SLOPE    | 0                | 16             | Х              | 16             | Х      | AAW   |        |         |          |
| 25   | WT | 5/27/2017 | TT               | -          | -           | SLOPE    | 0                | 5              |                | 5              | Х      | AAW   |        |         |          |
| 25   | WT | 5/27/2017 | TT               | 10:15 AM   | 78          | SLOPE    | 5                | 16             | Х              | 11             |        | AAW   |        |         |          |
| 24   | WT | 5/27/2017 | TT               | 10:19 AM   | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 23   | WT | 5/27/2017 | TT               | 10:21 AM   | 78          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 22   | WT | 5/27/2017 | TT               | 10:24 AM   | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 21   | WT | 5/27/2017 | TT               | 10:27 AM   | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 20   | WT | 5/27/2017 | TT               | 10:30 AM   | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |
| 17   | WT | 5/27/2017 | TT               | 10:31 AM   | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |        |         |          |



| From | То | Date      | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|----|-----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 16   | WT | 5/27/2017 | TT               | 10:35 AM   | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 47   | WT | 5/30/2017 | TT               | -          | -           | SLOPE    | 0                | 4              |                | 4              | Х      | AAW   |     |         |          |
| 47   | WT | 5/30/2017 | TT               | 9:45 AM    | 70          | SLOPE    | 4                | 16             | Х              | 12             |        | AAW   |     |         |          |
| 44   | WT | 5/30/2017 | TT               | 9:47 AM    | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 42   | WT | 5/30/2017 | TT               | 9:50 AM    | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 41   | WT | 5/30/2017 | TT               | 9:54 AM    | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 40   | WT | 5/30/2017 | TT               | -          | -           | SLOPE    | 0                | 4              |                | 4              | Х      | AAW   |     |         |          |
| 40   | WT | 5/30/2017 | TT               | 10:00 AM   | 70          | SLOPE    | 4                | 16             | Х              | 12             |        | AAW   |     |         |          |
| 39   | WT | 5/30/2017 | TT               | 10:02 AM   | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 37   | WT | 5/30/2017 | TT               | 10:05 AM   | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 36   | WT | 5/30/2017 | TT               | 10:08 AM   | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 35   | WT | 5/30/2017 | TT               | 10:10 AM   | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 33   | WT | 5/30/2017 | TT               | 10:15 AM   | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 30   | WT | 5/30/2017 | TT               | 10:19 AM   | 70          | SLOPE    | 0                | 8              |                | 8              |        | AAW   |     |         |          |
| 49   | WT | 5/30/2017 | TT               | 10:30 AM   | 70          | SLOPE    | 0                | 19             | Х              | 19             |        | AAW   |     |         |          |
| 48   | WT | 5/30/2017 | TT               | 10:35 AM   | 70          | SLOPE    | 0                | 13             |                | 13             |        | AAW   |     |         |          |
| 48   | WT | 5/30/2017 | TT               | -          | -           | SLOPE    | 13               | 17             | Х              | 4              | Х      | AAW   |     |         |          |
| 50   | WT | 5/30/2017 | TT               | 10:40 AM   | 70          | SLOPE    | 0                | 19             | Х              | 19             |        | AAW   |     |         |          |
| 54   | WT | 5/30/2017 | TT               | 10:50 AM   | 75          | SLOPE    | 0                | 23             | Х              | 23             |        | AAW   |     |         |          |
| 53   | WT | 5/30/2017 | TT               | 10:55 AM   | 75          | SLOPE    | 0                | 42             | Х              | 42             |        | AAW   |     |         |          |
| 52   | WT | 5/30/2017 | TT               | 11:02 AM   | 75          | SLOPE    | 0                | 29             | Х              | 29             |        | AAW   | 18  | 26      |          |
| 51   | WT | 5/30/2017 | TT               | 11:05 AM   | 75          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |          |
| 80   | PS | 5/30/2017 | TT               | 1:10 PM    | 75          | SLOPE    | 0                | 14             | Х              | 14             |        | AAW   |     |         |          |
| 78   | PS | 5/30/2017 | TT               | 1:12 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 79   | PS | 5/30/2017 | TT               | 1:15 PM    | 75          | SLOPE    | 0                | 16             | Χ              | 16             |        | AAW   |     |         |          |
| 77   | PS | 5/30/2017 | TT               | 1:20 PM    | 75          | SLOPE    | 0                | 16             | Χ              | 16             |        | AAW   |     |         |          |
| 76   | PS | 5/30/2017 | TT               | 1:22 PM    | 75          | SLOPE    | 0                | 16             | Χ              | 16             |        | AAW   |     |         |          |
| 74   | PS | 5/30/2017 | TT               | 1:25 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 73   | PS | 5/30/2017 | TT               | 1:27 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 71   | PS | 5/30/2017 | TT               | 1:30 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 67   | PS | 5/30/2017 | TT               | 1:32 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 66   | PS | 5/30/2017 | TT               | 1:35 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 64   | PS | 5/30/2017 | TT               | 1:37 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 63   | PS | 5/30/2017 | TT               | 1:40 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 62   | PS | 5/30/2017 | TT               | 1:43 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 61   | PS | 5/30/2017 | TT               | 1:45 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |



| From | То | Date      | Material<br>Type | Start Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|----|-----------|------------------|------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 60   | PS | 5/30/2017 | TT               | 1:47 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 59   | PS | 5/30/2017 | TT               | 1:50 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 57   | PS | 5/30/2017 | TT               | 1:52 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 56   | PS | 5/30/2017 | TT               | 1:55 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 55   | PS | 5/30/2017 | TT               | 1:58 PM    | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 54   | PS | 5/30/2017 | TT               | 2:00 PM    | 75          | SLOPE    | 0                | 11             | Х              | 11             |        | AAW   |     |         |          |



### Panel Seaming Log AG x112

| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS#     | DS Sta. | Comments |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|---------|---------|----------|
| 137  | 209 | 6/13/2017 | TT               | 10:00 AM      | 85          | SLOPE    | 0                | 27             | Х              | 27             |        | BJD   |         |         |          |
| 209  | PS  | 6/13/2017 | TT               | 10:15 AM      | 85          | SLOPE    | 0                | 36             | Х              | 36             |        | BJD   |         |         |          |
| 217  | PS  | 6/13/2017 | TT               | 10:38 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |         |         |          |
| 219  | PS  | 6/13/2017 | TT               | 3:18 PM       | 95          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |         |         |          |
| 220  | PS  | 6/13/2017 | TT               | 3:31 PM       | 95          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |         |         |          |
| 221  | PS  | 6/13/2017 | TT               | 3:38 PM       | 95          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |         |         |          |
| 223  | PS  | 6/14/2017 | TT               | 8:00 AM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |         |         |          |
| 229  | PS  | 6/14/2017 | TT               | 8:05 AM       | 80          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |         |         |          |
| 225  | PS  | 6/14/2017 | TT               | 8:10 AM       | 80          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |         |         |          |
| 226  | PS  | 6/14/2017 | TT               | 8:25 AM       | 80          | SLOPE    | 0                | 16             | Χ              | 16             |        | BJD   |         |         |          |
| 235  | 236 | 6/24/2017 | TT               | 7:50 AM       | 70          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |         |         |          |
| 144  | 244 | 6/24/2017 | TT               | 8:21 AM       | 70          | SLOPE    | 5                | 12             | X              | 7              |        | AAW   |         |         |          |
| 244  | PS  | 6/24/2017 | TT               | 8:25 AM       | 70          | SLOPE    | 0                | 2              | Х              | 2              |        | AAW   |         |         |          |
| 251  | PS  | 6/24/2017 | TT               | 8:28 AM       | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |         |         |          |
| 250  | PS  | 6/24/2017 | TT               | 8:35 AM       | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   | 67B     | 10      |          |
| 249  | PS  | 6/24/2017 | TT               | 9:08 AM       | 70          | SLOPE    | 0                | 14             | Х              | 14             | Х      | AAW   | 67, 67A | 4, 14   |          |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS#                                     | DS Sta.                      | Comments |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|---|------------------------------|----------|
| 85   | 86  | 5/31/2017 | TT               | 10:25 AM      | 80          | SLOPE    | 0                | 65             | Х              | 65             | Х      | AAW   | 20B6,20B7                               | 50, 30                       |          |
| 86   | 87  | 5/31/2017 | тт               | 10:55 AM      | 80          | SLOPE    | 0                | 77             |                | 77             | Х      | AAW   | 20, 20B, 20B2, 20B3,<br>20B4, 20B5, 20A | 67, 57, 47,<br>37, 27, 3, 77 |          |
| 86   | 87  | 5/31/2017 | TT               | -             | -           | SLOPE    | 77               | 79             | Х              |                | Х      | AAW   |   |                              |          |
| 99   | 100 | 6/1/2017  | TT               | 3:40 PM       | 81          | SLOPE    | 0                | 125            | х              | 125            | Х      | BJD   | 20A2, 20A3, 20A4,<br>20A5               | 12, 22, 32, 75               |          |
| 98   | 100 | 6/1/2017  | TT               | 4:00 PM       | 80          | SLOPE    | 0                | 46             | Х              | 46             |        | BJD   | 20A6, 20A7                              | 4, 14                        |          |
| 101  | 102 | 6/1/2017  | TT               | 4:58 PM       | 78          | SLOPE    | 27               | 39             | Х              | 12             |        | BJD   |   |                              |          |
| 101  | 104 | 6/1/2017  | TT               | 5:05 PM       | 77          | SLOPE    | 0                | 114            |                | 114            |        | BJD   |   |                              |          |
| 101  | 102 | 6/1/2017  | TT               | 5:10 PM       | 79          | SLOPE    | 0                | 15             |                | 15             |        | BJD   |   |                              |          |
| 102  | 103 | 6/1/2017  | TT               | 5:20 PM       | 78          | SLOPE    | 0                | 33             |                | 33             |        | BJD   |   |                              |          |
| 101  | 104 | 6/1/2017  | TT               | 5:24 PM       | 77          | SLOPE    | 115              | 129            | X              | 14             |        | BJD   |   |                              |          |
| 102  | 103 | 6/1/2017  | TT               | 5:36 PM       | 78          | SLOPE    | 35               | 43             | Х              | 8              |        | BJD   |   |                              |          |
| 102  | 104 | 6/1/2017  | TT               | 5:50 PM       | 77          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |   |                              |          |
| 106  | 108 | 6/1/2017  | TT               | 5:58 PM       | 75          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |   |                              |          |
| 103  | 106 | 6/1/2017  | TT               | 6:10 PM       | 75          | SLOPE    | 0                | 39             | X              | 39             |        | BJD   |   |                              |          |
| 105  | 106 | 6/1/2017  | TT               | 6:22 PM       | 75          | SLOPE    | 0                | 12             | Х              | 12             |        | BJD   |   |                              |          |
| 105  | 108 | 6/1/2017  | TT               | 6:30 PM       | 74          | SLOPE    | 0                | 128            | Х              | 128            |        | BJD   | 24                                      | 56                           |          |
| 27   | 103 | 6/1/2017  | TT               | 6:53 PM       | 74          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   | 46                                      | 13                           |          |



| From | То | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS#                      | DS Sta.           | Comments |
|------|----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|--------------------------|-------------------|----------|
| 88   | 89 | 5/31/2017 | TT               | 1:25 PM       | 80          | SLOPE    | 0                | 99             | Χ              | 99             |        | AAW   |                          |                   |          |
| 89   | 90 | 5/31/2017 | TT               | 1:42 PM       | 80          | SLOPE    | 0                | 113            | Χ              | 113            |        | AAW   |                          |                   |          |
| 90   | 91 | 5/31/2017 | TT               | 2:00 PM       | 80          | SLOPE    | 0                | 124            | X              | 124            |        | AAW   |                          |                   |          |
| 92   | 93 | 5/31/2017 | TT               | 2:35 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |                          |                   |          |
| 91   | 92 | 5/31/2017 | TT               | 2:45 PM       | 80          | SLOPE    | 0                | 83             | Х              | 83             |        | AAW   |                          |                   |          |
| 91   | 93 | 5/31/2017 | тт               | 2:57 PM       | 80          | SLOPE    | 0                | 49             | х              | 49             |        | AAW   | 21B, 21B2,<br>21B3, 21B4 | 42, 32,<br>22, 12 |          |
| 92   | 94 | 5/31/2017 | TT               | 3:05 PM       | 80          | SLOPE    | 0                | 84             | Х              | 84             |        | AAW   | 21 21A, 21A2             | 3, 13, 23         |          |
| 93   | 94 | 5/31/2017 | TT               | 3:20 PM       | 80          | SLOPE    | 0                | 62             | Х              | 62             |        | AAW   |                          |                   |          |
| 94   | 95 | 5/31/2017 | TT               | 3:40 PM       | 80          | SLOPE    | 0                | 172            | Х              | 172            |        | AAW   |                          |                   |          |
| 95   | 96 | 5/31/2017 | TT               | 4:10 PM       | 80          | SLOPE    | 0                | 173            | Х              | 173            |        | AAW   | 22                       | 172               |          |
| 36   | 96 | 5/31/2017 | TT               | 4:38 PM       | 80          | SLOPE    | 0                | 9              | Х              | 9              |        | AAW   |                          |                   |          |
| 36   | 95 | 5/31/2017 | TT               | 4:39 PM       | 80          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |                          |                   |          |
| 38   | 95 | 5/31/2017 | TT               | 4:50 PM       | 80          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |                          |                   |          |
| 38   | 94 | 5/31/2017 | TT               | 4:51 PM       | 80          | SLOPE    | 0                | 4              | Х              | 4              |        | AAW   |                          |                   |          |
| 69   | 94 | 5/31/2017 | TT               | 4:51 PM       | 80          | SLOPE    | 0                | 5              | Х              | 5              |        | AAW   |                          |                   |          |
| 70   | 94 | 5/31/2017 | TT               | 4:52 PM       | 80          | SLOPE    | 0                | 19             | Х              | 19             |        | AAW   |                          |                   |          |
| 72   | 94 | 5/31/2017 | TT               | 4:55 PM       | 80          | SLOPE    | 0                | 12             | Х              | 12             |        | AAW   |                          |                   |          |
| 72   | 93 | 5/31/2017 | TT               | 4:57 PM       | 80          | SLOPE    | 0                | 12             | Х              | 12             |        | AAW   |                          |                   |          |
| 73   | 93 | 5/31/2017 | TT               | 4:59 PM       | 80          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |                          |                   |          |
| 73   | 91 | 5/31/2017 | TT               | 5:01 PM       | 80          | SLOPE    | 0                | 19             | Х              | 19             |        | AAW   |                          |                   |          |
| 75   | 90 | 5/31/2017 | TT               | 5:05 PM       | 80          | SLOPE    | 0                | 18             | Х              | 18             |        | AAW   |                          |                   |          |
| 75   | 89 | 5/31/2017 | TT               | 5:08 PM       | 80          | SLOPE    | 0                | 10             | Х              | 10             |        | AAW   |                          |                   |          |
| 76   | 89 | 5/31/2017 | TT               | 5:10 PM       | 80          | SLOPE    | 0                | 9              | Х              | 9              |        | AAW   |                          |                   |          |
| 76   | 88 | 5/31/2017 | TT               | 5:12 PM       | 80          | SLOPE    | 0                | 18             | Х              | 18             |        | AAW   |                          |                   |          |
| 76   | 87 | 5/31/2017 | TT               | 5:16 PM       | 80          | SLOPE    | 0                | 0.5            | Х              | 0.5            | Х      | AAW   |                          |                   |          |
| 77   | 87 | 5/31/2017 | TT               | 5:16 PM       | 80          | SLOPE    | 0                | 18             | Х              | 18             |        | AAW   |                          |                   |          |
| 77   | 86 | 5/31/2017 | TT               | 5:19 PM       | 80          | SLOPE    | 0                | 11             | Х              | 11             |        | AAW   |                          |                   |          |
| 78   | 86 | 5/31/2017 | TT               | 5:22 PM       | 80          | SLOPE    | 0                | 7              | Х              | 7              |        | AAW   |                          |                   |          |
| 78   | 85 | 5/31/2017 | TT               | 5:23 PM       | 80          | SLOPE    | 0                | 19             | Х              | 19             |        | AAW   |                          |                   |          |
| 78   | 84 | 5/31/2017 | TT               | 5:27 PM       | 80          | SLOPE    | 0                | 4              | Х              | 4              |        | AAW   |                          |                   |          |
| 79   | 84 | 5/31/2017 | TT               | 5:28 PM       | 80          | SLOPE    | 0                | 14             | х              | 14             |        | AAW   |                          |                   |          |
| 79   | 83 | 5/31/2017 | TT               | 5:30 PM       | 80          | SLOPE    | 0                | 14             | Х              | 14             |        | AAW   |                          |                   |          |
| 80   | 83 | 5/31/2017 | TT               | 5:33 PM       | 80          | SLOPE    | 0                | 5              | Х              | 5              |        | AAW   |                          |                   |          |
| 80   | 82 | 5/31/2017 | TT               | 5:34 PM       | 80          | SLOPE    | 0                | 19             | Х              | 19             |        | AAW   | 49                       | 9                 |          |
| 80   | 81 | 5/31/2017 | TT               | 5:38 PM       | 80          | SLOPE    | 0                | 7              | Х              | 7              |        | AAW   |                          |                   |          |



### Panel Seaming Log AG x211

| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments              |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|-----------------------|
| 25   | WT  | 5/30/2017 | TT               | 11:25 AM      | 75          | SLOPE    | 0                | 3              |                | 3              |        | AAW   |     |         |                       |
| 25   | WT  | 5/30/2017 | TT               | -             | -           | SLOPE    | 3                | 5              |                | 2              | Х      | AAW   |     |         |                       |
| 26   | WT  | 5/30/2017 | TT               | -             | -           | SLOPE    | 0                | 3              |                | 3              | Х      | AAW   |     |         |                       |
| 26   | WT  | 5/30/2017 | TT               | 11:35 AM      | 75          | SLOPE    | 3                | 14             | X              | 11             |        | AAW   |     |         |                       |
| 27   | WT  | 5/30/2017 | TT               | -             | -           | SLOPE    | 0                | 4              | X              | 4              | Χ      | AAW   |     |         |                       |
| 29   | WT  | 5/30/2017 | TT               | -             | -           | SLOPE    | 0                | 3              |                | 3              | Х      | AAW   |     |         |                       |
| 29   | WT  | 5/30/2017 | TT               | 11:40 AM      | 75          | SLOPE    | 3                | 17             | Х              | 14             |        | AAW   |     |         |                       |
| 18   | WT  | 5/30/2017 | TT               | 1:00 PM       | 75          | SLOPE    | 9                | 12             | Х              | 3              |        | AAW   |     |         |                       |
| 30   | WT  | 5/30/2017 | TT               | 1:30 PM       | 75          | SLOPE    | 10               | 19             |                | 9              |        | AAW   |     |         |                       |
| 48   | WT  | 5/30/2017 | TT               | 3:16 PM       | 75          | SLOPE    | 16               | 19             |                | 3              |        | AAW   |     |         |                       |
| 73   | 73  | 5/30/2017 | TT               | 3:24 PM       | 75          | SLOPE    | 7                | 16             | Х              | 9              |        | AAW   |     |         |                       |
| 73   | 73  | 5/30/2017 | TT               | -             | -           | SLOPE    | 0                | 7              |                | 7              | Х      | AAW   |     |         |                       |
| 89   | PS  | 6/1/2017  | TT               | 1:46 PM       | 82          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |     |         |                       |
| 90   | PS  | 6/1/2017  | TT               | 2:10 PM       | 82          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |                       |
| 91   | PS  | 6/1/2017  | TT               | 2:32 PM       | 82          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |                       |
| 92   | PS  | 6/1/2017  | TT               | 2:38 PM       | 84          | SLOPE    | 0                | 19             | Х              | 19             |        | BJD   |     |         |                       |
| 94   | PS  | 6/1/2017  | TT               | 3:10 PM       | 84          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |                       |
| 95   | PS  | 6/1/2017  | TT               | 3:21 PM       | 83          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |                       |
| 96   | PS  | 6/1/2017  | TT               | 3:34 PM       | 82          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |     |         |                       |
| 97   | PS  | 6/1/2017  | TT               | 4:00 PM       | 80          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   | 52B | 15      |                       |
| 98   | PS  | 6/1/2017  | TT               | 5:00 PM       | 79          | SLOPE    | 0                | 12             |                | 12             | Х      | BJD   |     |         |                       |
| 98   | PS  | 6/2/2017  | TT               | 10:30 AM      | 81          | SLOPE    | 12               | 15             | X              | 3              | Х      | BJD   | 52  | 5       |                       |
| 100  | PS  | 6/2/2017  | TT               | 10:45 AM      | 82          | SLOPE    | 0                | 23             | Х              | 23             | Х      | BJD   |     |         |                       |
| 101  | PS  | 6/2/2017  | TT               | 10:55 AM      | 83          | SLOPE    | 0                | 17             | X              | 17             | Х      | BJD   |     |         | Seam covered by P-235 |
| 135  | WT  | 6/22/2017 | TT               | 8:30 AM       | 75          | SLOPE    | 0                | 17             | X              | 17             |        | AAW   | 69  | 5       | Serves as DS-52A      |
| 244  | 104 | 6/23/2017 | TT               | 4:05 PM       | 80          | SLOPE    | 0                | 15             | X              | 15             |        | AAW   |     |         |                       |
| 105  | 244 | 6/23/2017 | TT               | 4:15 PM       | 80          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |                       |
| 108  | 244 | 6/23/2017 | TT               | 4:22 PM       | 80          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |                       |
| 109  | 244 | 6/23/2017 | TT               | 4:37 PM       | 80          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |                       |
| 143  | 244 | 6/23/2017 | TT               | 4:45 PM       | 80          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |                       |
| 144  | 244 | 6/23/2017 | TT               | 5:10 PM       | 80          | SLOPE    | 0                | 5              |                | 5              |        | AAW   |     |         |                       |



| From | То | Date     | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|----|----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 82   | PS | 6/1/2017 | TT               | 8:00 AM       | 68          | SLOPE    | 0                | 1              |                | 1              |        | BJD   |     |         |          |
| 82   | PS | 6/1/2017 | TT               | 8:05 AM       | 68          | SLOPE    | 1                | 16             | Х              | 15             |        | BJD   |     |         |          |
| 83   | PS | 6/1/2017 | TT               | 8:08 AM       | 68          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 84   | PS | 6/1/2017 | TT               | 8:13 AM       | 68          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 85   | PS | 6/1/2017 | TT               | 8:56 AM       | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 86   | PS | 6/1/2017 | TT               | 9:05 AM       | 70          | SLOPE    | 0                | 20             | Х              | 20             |        | BJD   |     |         |          |
| 87   | PS | 6/1/2017 | TT               | 9:58 AM       | 72          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   | 47B | 14      |          |
| 88   | PS | 6/1/2017 | TT               | 10:07 AM      | 73          | SLOPE    | 0                | 16             | Х              | 16             | Χ      | BJD   | 47  | 13      |          |



### Panel Seaming Log AG x83

| From | То  | Date     | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 104  | PS  | 6/2/2017 | TT               | 1:20 PM       | 88          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 105  | PS  | 6/2/2017 | TT               | 1:38 PM       | 90          | SLOPE    | 0                | 20             | Х              | 20             |        | BJD   |     |         |          |
| 108  | PS  | 6/2/2017 | TT               | 3:03 PM       | 90          | SLOPE    | 0                | 20             | Х              | 20             |        | BJD   |     |         |          |
| 109  | PS  | 6/2/2017 | TT               | 3:12 PM       | 90          | SLOPE    | 0                | 11             |                | 11             |        | BJD   |     |         |          |
| 110  | PS  | 6/3/2017 | TT               | 9:30 AM       | 85          | SLOPE    | 3                | 7              | Х              | 4              |        | BJD   |     |         |          |
| 81   | 110 | 6/3/2017 | TT               | 9:32 AM       | 85          | SLOPE    | 0                | 3              | Х              | 3              |        | BJD   |     |         |          |
| 110  | PS  | 6/3/2017 | TT               | 9:40 AM       | 85          | SLOPE    | 0                | 11             | Х              | 11             |        | BJD   |     |         |          |
| 111  | PS  | 6/3/2017 | TT               | 9:59 AM       | 85          | SLOPE    | 0                | 21             |                | 21             |        | BJD   |     |         |          |
| 111  | PS  | 6/3/2017 | TT               | 10:19 AM      | 85          | SLOPE    | 21               | 28             | Х              | 7              |        | BJD   |     |         |          |
| 112  | PS  | 6/3/2017 | TT               | 10:25 AM      | 85          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |          |
| 113  | PS  | 6/3/2017 | TT               | 10:28 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 114  | PS  | 6/3/2017 | TT               | 10:36 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 115  | PS  | 6/3/2017 | TT               | 11:10 AM      | 88          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 116  | PS  | 6/3/2017 | TT               | 11:22 AM      | 88          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 117  | PS  | 6/3/2017 | TT               | 11:35 AM      | 88          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 119  | PS  | 6/3/2017 | TT               | 11:44 AM      | 88          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 120  | PS  | 6/3/2017 | TT               | 1:35 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 121  | PS  | 6/3/2017 | TT               | 1:43 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 122  | PS  | 6/3/2017 | TT               | 2:02 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 123  | PS  | 6/3/2017 | TT               | 2:34 PM       | 90          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |     |         |          |
| 124  | PS  | 6/3/2017 | TT               | 3:03 PM       | 90          | SLOPE    | 0                | 18             | Х              | 18             |        | BJD   |     |         |          |
| 125  | PS  | 6/3/2017 | TT               | 3:15 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 126  | PS  | 6/3/2017 | TT               | 3:28 PM       | 90          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |     |         |          |
| 128  | PS  | 6/3/2017 | TT               | 4:02 PM       | 90          | SLOPE    | 0                | 7              | Х              | 7              |        | BJD   |     |         |          |
| 127  | PS  | 6/3/2017 | TT               | 4:12 PM       | 90          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |     |         |          |
| 129  | PS  | 6/3/2017 | TT               | 4:20 PM       | 90          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |     |         |          |
| 130  | PS  | 6/3/2017 | TT               | 4:30 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 131  | PS  | 6/3/2017 | TT               | 4:40 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   | 40  | 12      |          |
| 132  | PS  | 6/3/2017 | TT               | 4:49 PM       | 90          | SLOPE    | 0                | 14             | Χ              | 14             |        | BJD   |     |         |          |



| From | То  | Date     | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 110  | 111 | 6/3/2017 | TT               | 8:08 AM       | 85          | SLOPE    | 0                | 27             |                | 27             |        | BJD   |     |         |          |
| 110  | 111 | 6/3/2017 | TT               | 8:13 AM       | 85          | SLOPE    | 28               | 60             |                | 32             |        | BJD   |     |         |          |
| 110  | 111 | 6/3/2017 | TT               | 8:18 AM       | 85          | SLOPE    | 62               | 72             |                | 10             |        | BJD   |     |         |          |
| 110  | 111 | 6/3/2017 | TT               | 8:19 AM       | 85          | SLOPE    | 74               | 78             | Х              | 4              |        | BJD   |     |         |          |
| 112  | 113 | 6/3/2017 | TT               | 8:24 AM       | 85          | SLOPE    | 0                | 66             | Х              | 66             |        | BJD   |     |         |          |
| 114  | 115 | 6/3/2017 | TT               | 8:37 AM       | 85          | SLOPE    | 0                | 66             | Х              | 66             |        | BJD   |     |         |          |
| 116  | 118 | 6/3/2017 | TT               | 8:56 AM       | 85          | SLOPE    | 0                | 6              | Х              | 6              |        | BJD   |     |         |          |
| 116  | 117 | 6/3/2017 | TT               | 8:57 AM       | 85          | SLOPE    | 0                | 60             | Х              | 60             |        | BJD   |     |         |          |
| 119  | 120 | 6/3/2017 | TT               | 9:15 AM       | 85          | SLOPE    | 0                | 66             | Х              | 66             |        | BJD   |     |         |          |
| 122  | 123 | 6/3/2017 | TT               | 9:30 AM       | 85          | SLOPE    | 0                | 64             | Х              | 64             |        | BJD   |     |         |          |
| 124  | 125 | 6/3/2017 | TT               | 10:03 AM      | 85          | SLOPE    | 0                | 16             |                | 16             |        | BJD   |     |         |          |
| 124  | 125 | 6/3/2017 | TT               | 10:04 AM      | 85          | SLOPE    | 19               | 65             | Х              | 46             |        | BJD   |     |         |          |
| 126  | 127 | 6/3/2017 | TT               | 10:30 AM      | 85          | SLOPE    | 0                | 35             | Х              | 35             |        | BJD   |     |         |          |
| 127  | 128 | 6/3/2017 | TT               | 10:37 AM      | 85          | SLOPE    | 0                | 23             | Х              | 23             |        | BJD   | 27  | 2       |          |
| 130  | 131 | 6/3/2017 | TT               | 10:56 AM      | 88          | SLOPE    | 39               | 54             | X              | 15             |        | BJD   |     |         |          |
| 130  | 131 | 6/3/2017 | TT               | 11:05 AM      | 88          | SLOPE    | 0                | 38             |                | 38             |        | BJD   |     |         |          |
| 133  | 134 | 6/3/2017 | TT               | 11:14 AM      | 88          | SLOPE    | 0                | 17             | X              | 17             |        | BJD   |     |         |          |
| 132  | 133 | 6/3/2017 | TT               | 11:20 AM      | 88          | SLOPE    | 0                | 18             | Х              | 18             |        | BJD   |     |         |          |
| 132  | 134 | 6/3/2017 | TT               | 11:22 AM      | 88          | SLOPE    | 0                | 21             | Х              | 21             |        | BJD   |     |         |          |
| 134  | 135 | 6/3/2017 | TT               | 11:27 AM      | 88          | SLOPE    | 0                | 34             | X              | 34             |        | BJD   |     |         |          |
| 110  | 137 | 6/3/2017 | TT               | 1:22 PM       | 90          | SLOPE    | 0                | 54             |                | 54             |        | BJD   |     |         |          |
| 110  | 137 | 6/3/2017 | TT               | 1:31 PM       | 90          | SLOPE    | 55               | 78             |                | 23             |        | BJD   |     |         |          |
| 110  | 137 | 6/3/2017 | TT               | 1:34 PM       | 90          | SLOPE    | 78               | 86             | Х              | 8              |        | BJD   |     |         |          |
| 138  | 139 | 6/3/2017 | TT               | 1:40 PM       | 90          | SLOPE    | 0                | 16             |                | 16             |        | BJD   |     |         |          |
| 138  | 139 | 6/3/2017 | TT               | 1:47 PM       | 90          | SLOPE    | 20               | 38             |                | 18             |        | BJD   |     |         |          |
| 138  | 139 | 6/3/2017 | TT               | 1:52 PM       | 90          | SLOPE    | 38               | 46             | Х              | 8              |        | BJD   | 41  | 43      |          |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 136  | 137 | 6/3/2017  | TT               | 1:30 PM       | 90          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |          |
| 137  | 138 | 6/3/2017  | TT               | 1:40 PM       | 90          | SLOPE    | 0                | 47             | Х              | 47             |        | BJD   |     |         |          |
| 139  | 140 | 6/3/2017  | TT               | 1:50 PM       | 90          | SLOPE    | 0                | 47             | Х              | 47             |        | BJD   |     |         |          |
| 140  | 141 | 6/3/2017  | TT               | 1:59 PM       | 90          | SLOPE    | 0                | 47             | Х              | 47             |        | BJD   |     |         |          |
| 141  | 142 | 6/3/2017  | TT               | 2:10 PM       | 90          | SLOPE    | 0                | 43             | X              | 43             |        | BJD   |     |         |          |
| 136  | 142 | 6/3/2017  | TT               | 2:20 PM       | 90          | SLOPE    | 6                | 12             | X              | 6              |        | BJD   |     |         |          |
| 136  | 141 | 6/3/2017  | TT               | 2:22 PM       | 90          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |          |
| 136  | 140 | 6/3/2017  | TT               | 2:24 PM       | 90          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |          |
| 136  | 139 | 6/3/2017  | TT               | 2:26 PM       | 90          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |          |
| 136  | 138 | 6/3/2017  | TT               | 2:28 PM       | 90          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |          |
| 19   | 167 | 6/10/2017 | TT               | 1:21 PM       | 85          | SLOPE    | 0                | 6              | X              | 6              |        | BJD   |     |         |          |
| 1    | 166 | 6/10/2017 | TT               | 1:31 PM       | 85          | SLOPE    | 0                | 4              | X              | 4              |        | BJD   |     |         |          |
| 2    | 166 | 6/10/2017 | TT               | 1:32 PM       | 85          | SLOPE    | 0                | 7              | X              | 7              |        | BJD   |     |         |          |
| 2    | 165 | 6/10/2017 | TT               | 1:33 PM       | 85          | SLOPE    | 0                | 6              | X              | 6              |        | BJD   |     |         |          |
| 3    | 165 | 6/10/2017 | TT               | 1:34 PM       | 85          | SLOPE    | 0                | 4              | X              | 4              |        | BJD   |     |         |          |
| 3    | 163 | 6/10/2017 | TT               | 1:40 PM       | 85          | SLOPE    | 0                | 6              | X              | 6              |        | BJD   |     |         |          |
| 4    | 163 | 6/10/2017 | TT               | 1:41 PM       | 85          | SLOPE    | 0                | 7              | Х              | 7              |        | BJD   |     |         |          |
| 4    | 162 | 6/10/2017 | TT               | 1:42 PM       | 85          | SLOPE    | 0                | 4              | X              | 4              |        | BJD   |     |         |          |
| 5    | 162 | 6/10/2017 | TT               | 1:44 PM       | 85          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 5    | 161 | 6/10/2017 | TT               | -             | -           | SLOPE    | 0                | 5              | Х              | 5              | Χ      | BJD   |     |         |          |
| 6    | 161 | 6/10/2017 | TT               | 1:48 PM       | 85          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 6    | 159 | 6/10/2017 | TT               | -             | -           | SLOPE    | 0                | 4              | Х              | Х              | Х      | BJD   |     |         |          |
| 7    | 159 | 6/10/2017 | TT               | 1:55 PM       | 85          | SLOPE    | 0                | 7              | Х              | 7              |        | BJD   |     |         |          |
| 7    | 158 | 6/10/2017 | TT               | 1:57 PM       | 85          | SLOPE    | 0                | 3              | Х              | 3              |        | BJD   |     |         |          |
| 8    | 158 | 6/10/2017 | TT               | 1:58 PM       | 85          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 8    | 156 | 6/10/2017 | TT               | 1:59 PM       | 85          | SLOPE    | 0                | 5              | Х              | 5              |        | BJD   |     |         |          |
| 9    | 156 | 6/10/2017 | TT               | 2:00 PM       | 85          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 209  | 210 | 6/13/2017 | TT               | 9:07 AM       | 80          | SLOPE    | 0                | 62             | Х              | 62             |        | BJD   |     |         |          |
| 210  | 211 | 6/13/2017 | TT               | 9:24 AM       | 80          | SLOPE    | 0                | 61             | Х              | 61             |        | BJD   |     |         |          |
| 211  | 212 | 6/13/2017 | TT               | 9:37 AM       | 80          | SLOPE    | 0                | 61             | Х              | 61             |        | BJD   | 48  | 13      |          |
| 212  | 213 | 6/13/2017 | TT               | 9:51 AM       | 80          | SLOPE    | 7                | 33             | Х              | 26             |        | BJD   |     |         |          |
| 213  | 214 | 6/13/2017 | TT               | 10:02 AM      | 85          | SLOPE    | 0                | 4              |                | 4              | Х      | BJD   |     |         |          |
| 213  | 214 | 6/13/2017 | TT               | 10:03 AM      | 85          | SLOPE    | 4                | 33             | Х              | 29             |        | BJD   |     |         |          |
| 213  | 215 | 6/13/2017 | TT               | 10:15 AM      | 85          | SLOPE    | 0                | 11             |                | 11             |        | BJD   |     |         |          |
| 212  | 215 | 6/13/2017 | TT               | 10:17 AM      | 85          | SLOPE    | 0                | 26             | Х              | 26             |        | BJD   |     |         |          |
| 212  | 213 | 6/13/2017 | TT               | 10:27 AM      | 85          | SLOPE    | 0                | 5              |                | 5              |        | BJD   |     |         |          |



| From | То   | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|------|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 215  | 216  | 6/13/2017 | TT               | 10:30 AM      | 85          | SLOPE    | 0                | 27             | Х              | 27             |        | BJD   |     |         |          |
| 214  | 216  | 6/13/2017 | TT               | 10:40 AM      | 85          | SLOPE    | 0                | 7              |                | 7              | Х      | BJD   |     |         |          |
| 214  | 216  | 6/13/2017 | TT               | 10:40 AM      | 85          | SLOPE    | 7                | 16             | X              | 9              |        | BJD   |     |         |          |
| 218  | 219  | 6/13/2017 | TT               | 10:51 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |          |
| 217  | 219  | 6/13/2017 | TT               | 10:55 AM      | 85          | SLOPE    | 0                | 10             | X              | 10             |        | BJD   |     |         |          |
| 217  | 218  | 6/13/2017 | TT               | 10:57 AM      | 85          | SLOPE    | 0                | 16             |                | 16             |        | BJD   |     |         |          |
| 217  | 218  | 6/13/2017 | TT               | 11:00 AM      | 85          | SLOPE    | 16               | 83             | X              | 67             |        | BJD   |     |         |          |
| 221  | 223  | 6/13/2017 | TT               | 11:35 AM      | 85          | SLOPE    | 0                | 21             |                | 21             |        | BJD   |     |         |          |
| 221  | 223  | 6/13/2017 | TT               | 11:40 AM      | 85          | SLOPE    | 26               | 45             |                | 19             |        | BJD   |     |         |          |
| 221  | 223  | 6/13/2017 | TT               | 11:44 AM      | 85          | SLOPE    | 52               | 69             | Х              | 17             |        | BJD   |     |         |          |
| 222  | 223  | 6/13/2017 | TT               | 1:24 PM       | 90          | SLOPE    | 0                | 18             | X              | 18             |        | BJD   |     |         |          |
| 137  | 209  | 6/13/2017 | TT               | 1:30 PM       | 90          | SLOPE    | 0                | 7              | Х              | 7              |        | BJD   |     |         |          |
| 136  | 209  | 6/13/2017 | TT               | 1:31 PM       | 90          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 136  | 210  | 6/13/2017 | TT               | 1:37 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 136  | 211  | 6/13/2017 | TT               | 1:44 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 136  | 212  | 6/13/2017 | TT               | 1:51 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 136  | 213  | 6/13/2017 | TT               | 1:58 PM       | 90          | SLOPE    | 0                | 11             | Х              | 11             |        | BJD   |     |         |          |
| 136  | 214  | 6/13/2017 | TT               | 2:04 PM       | 90          | SLOPE    | 0                | 13             | Х              | 13             |        | BJD   |     |         |          |
| 223  | 224  | 6/14/2017 | TT               | 7:42 AM       | 80          | SLOPE    | 0                | 89             | X              | 89             |        | BJD   | 50  | 47      |          |
| 224  | 225  | 6/14/2017 | TT               | 8:00 AM       | 80          | SLOPE    | 0                | 13             |                | 13             |        | BJD   |     |         |          |
| 224  | 225  | 6/14/2017 | TT               | 8:04 AM       | 80          | SLOPE    | 13               | 89             | X              | 76             |        | BJD   |     |         |          |
| R478 | 100  | 6/19/2017 | TT               | 8:09 AM       | 75          | SLOPE    | 0                | 137            | X              | 137            |        | BJV   |     |         |          |
| 99   | R478 | 6/19/2017 | TT               | 8:50 AM       | 75          | SLOPE    | 0                | 125            | X              | 125            |        | BJV   |     |         |          |
| 98   | R478 | 6/19/2017 | TT               | 9:18 AM       | 75          | SLOPE    | 0                | 12             | Х              | 12             |        | BJV   |     |         |          |
| 93   | R479 | 6/19/2017 | TT               | 9:38 AM       | 75          | SLOPE    | 0                | 43             | Х              | 43             |        | BJV   |     |         |          |
| 91   | R479 | 6/19/2017 | TT               | 9:40 AM       | 75          | SLOPE    | 0                | 43             | Х              | 43             |        | BJV   | 58  | 21      |          |
| 87   | R480 | 6/19/2017 | TT               | 9:53 AM       | 75          | SLOPE    | 0                | 70             | Х              | 70             |        | BJV   |     |         |          |
| 86   | R480 | 6/19/2017 | TT               | 10:08 AM      | 75          | SLOPE    | 0                | 70             | Х              | 70             |        | BJV   |     |         |          |
| 86   | R481 | 6/19/2017 | TT               | 10:22 AM      | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | BJV   |     |         |          |
| 85   | R481 | 6/19/2017 | TT               | 10:29 AM      | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | BJV   |     |         |          |
| 86   | R482 | 6/19/2017 | TT               | 10:32 AM      | 75          | SLOPE    | 0                | 44             | Х              | 44             |        | BJV   |     |         |          |
| 85   | R482 | 6/19/2017 | TT               | 10:42 AM      | 75          | SLOPE    | 0                | 44             | Х              | 44             |        | BJV   |     |         |          |
| 245  | 246  | 6/21/2017 | TT               | 1:25 PM       | 90          | SLOPE    | 0                | 71             | Х              | 71             |        | AAW   |     |         |          |
| 246  | 247  | 6/21/2017 | TT               | 1:45 PM       | 90          | SLOPE    | 0                | 31             |                | 31             |        | AAW   |     |         |          |
| 246  | 247  | 6/21/2017 | TT               | 1:52 PM       | 90          | SLOPE    | 36               | 56             | Х              | 20             |        | AAW   |     |         |          |
| 247  | 248  | 6/21/2017 | TT               | 1:56 PM       | 90          | SLOPE    | 0                | 47             | Х              | 47             |        | AAW   |     |         |          |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 248  | 249 | 6/21/2017 | TT               | 2:05 PM       | 90          | SLOPE    | 0                | 40             | Х              | 40             |        | AAW   |     |         |          |
| 249  | 250 | 6/21/2017 | TT               | 2:12 PM       | 90          | SLOPE    | 0                | 31             | Х              | 31             |        | AAW   | 61  | 14      |          |
| 250  | 251 | 6/21/2017 | TT               | 2:17 PM       | 90          | SLOPE    | 0                | 24             | Х              | 24             |        | AAW   |     |         |          |
| 251  | 244 | 6/21/2017 | TT               | 2:29 PM       | 90          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |          |
| 242  | 251 | 6/21/2017 | TT               | 2:32 PM       | 90          | SLOPE    | 0                | 11             | Х              | 11             |        | AAW   |     |         |          |
| 242  | 250 | 6/21/2017 | TT               | 2:34 PM       | 90          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |          |
| 242  | 249 | 6/21/2017 | TT               | 2:36 PM       | 90          | SLOPE    | 0                | 18             | Х              | 18             |        | AAW   |     |         |          |
| 242  | 248 | 6/21/2017 | TT               | 2:48 PM       | 90          | SLOPE    | 0                | 12             | Х              | 12             |        | AAW   |     |         |          |
| 243  | 248 | 6/21/2017 | TT               | 2:49 PM       | 90          | SLOPE    | 0                | 6              | Х              | 6              |        | AAW   |     |         |          |
| 243  | 247 | 6/21/2017 | TT               | 2:49 PM       | 90          | SLOPE    | 0                | 18             | Х              | 18             |        | AAW   |     |         |          |
| 243  | 246 | 6/21/2017 | TT               | 2:51 PM       | 90          | SLOPE    | 0                | 5              |                | 5              |        | AAW   |     |         |          |
| R617 | 246 | 6/21/2017 | TT               | 2:57 PM       | 90          | SLOPE    | 0                | 11             | Х              | 11             |        | AAW   |     |         |          |
| R617 | 243 | 6/21/2017 | TT               | 3:01 PM       | 90          | SLOPE    | 0                | 15             | Х              | 15             |        | AAW   |     |         |          |
| 245  | 252 | 6/22/2017 | TT               | 8:00 AM       | 75          | SLOPE    | 0                | 69             | Х              | 69             |        | AAW   |     |         |          |
| 252  | 254 | 6/22/2017 | TT               | 8:18 AM       | 75          | SLOPE    | 0                | 55             | Х              | 55             |        | AAW   |     |         |          |
| 254  | 253 | 6/22/2017 | TT               | 8:36 AM       | 75          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 252  | 253 | 6/22/2017 | TT               | 8:42 AM       | 75          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |     |         |          |
| 253  | 255 | 6/22/2017 | TT               | 8:44 AM       | 75          | SLOPE    | 0                | 4              | Х              | 4              |        | AAW   |     |         |          |
| 254  | 255 | 6/22/2017 | TT               | 8:50 AM       | 75          | SLOPE    | 0                | 55             | Х              | 55             |        | AAW   |     |         |          |
| 255  | 256 | 6/22/2017 | TT               | 9:09 AM       | 75          | SLOPE    | 0                | 46             | Х              | 46             |        | AAW   | 62  | 13      |          |
| 256  | 257 | 6/22/2017 | TT               | 9:20 AM       | 75          | SLOPE    | 0                | 34             | Х              | 34             |        | AAW   |     |         |          |
| 257  | 258 | 6/22/2017 | TT               | 9:35 AM       | 75          | SLOPE    | 0                | 30             | Х              | 30             |        | AAW   |     |         |          |
| 258  | 259 | 6/22/2017 | TT               | 9:39 AM       | 75          | SLOPE    | 0                | 30             | Х              | 30             |        | AAW   |     |         |          |
| 259  | 260 | 6/22/2017 | TT               | 9:48 AM       | 75          | SLOPE    | 0                | 33             | Х              | 33             |        | AAW   |     |         |          |
| 260  | 261 | 6/22/2017 | TT               | 9:57 AM       | 75          | SLOPE    | 0                | 36             | Х              | 36             |        | AAW   |     |         |          |
| 261  | 262 | 6/22/2017 | TT               | 10:10 AM      | 75          | SLOPE    | 0                | 35             | Х              | 35             |        | AAW   |     |         |          |
| 262  | 263 | 6/22/2017 | TT               | 10:36 AM      | 75          | SLOPE    | 3                | 35             | Х              | 32             |        | AAW   |     |         |          |
| 263  | 264 | 6/22/2017 | TT               | 10:44 AM      | 75          | SLOPE    | 0                | 32             | Х              | 32             |        | AAW   |     |         |          |
| 264  | 265 | 6/22/2017 | TT               | 10:55 AM      | 75          | SLOPE    | 0                | 30             | Х              | 30             |        | AAW   |     |         |          |
| 265  | 266 | 6/22/2017 | TT               | 11:02 AM      | 75          | SLOPE    | 0                | 30             | Х              | 30             |        | AAW   |     |         |          |
| 266  | 267 | 6/22/2017 | TT               | 11:16 AM      | 75          | SLOPE    | 0                | 28             | Х              | 28             |        | AAW   |     |         |          |
| 267  | 268 | 6/22/2017 | TT               | 11:24 AM      | 75          | SLOPE    | 0                | 27             | Х              | 27             |        | AAW   |     |         |          |
| 268  | 269 | 6/22/2017 | TT               | 11:30 AM      | 75          | SLOPE    | 0                | 26             | Х              | 26             |        | AAW   |     |         |          |
| 270  | 271 | 6/22/2017 | TT               | 3:39 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 272  | 273 | 6/22/2017 | TT               | 3:47 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 271  | 273 | 6/22/2017 | TT               | 3:53 PM       | 80          | SLOPE    | 0                | 31             | Х              | 31             |        | AAW   | 63  | 21      |          |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 270  | 273 | 6/22/2017 | TT               | 3:58 PM       | 80          | SLOPE    | 0                | 5              |                | 5              |        | AAW   |     |         |          |
| 270  | 272 | 6/22/2017 | TT               | 3:59 PM       | 80          | SLOPE    | 0                | 100            | X              | 100            |        | AAW   |     |         |          |
| 274  | 275 | 6/22/2017 | TT               | 4:02 PM       | 80          | SLOPE    | 0                | 39             |                | 39             |        | AAW   |     |         |          |
| 274  | 275 | 6/22/2017 | TT               | 4:09 PM       | 80          | SLOPE    | 46               | 68             | Х              | 22             |        | AAW   |     |         |          |
| 275  | 276 | 6/22/2017 | TT               | 4:12 PM       | 80          | SLOPE    | 0                | 27             | Х              | 27             |        | AAW   |     |         |          |
| 276  | 277 | 6/22/2017 | TT               | 4:22 PM       | 80          | SLOPE    | 0                | 15             | X              | 15             |        | AAW   |     |         |          |
| 275  | 277 | 6/22/2017 | TT               | 4:26 PM       | 80          | SLOPE    | 0                | 19             | X              | 19             |        | AAW   |     |         |          |
| 276  | 278 | 6/22/2017 | TT               | 4:29 PM       | 80          | SLOPE    | 0                | 25             | Х              | 25             |        | AAW   |     |         |          |
| 272  | 279 | 6/22/2017 | TT               | 4:40 PM       | 80          | SLOPE    | 0                | 65             | X              | 65             |        | AAW   |     |         |          |
| 278  | 279 | 6/22/2017 | TT               | 4:55 PM       | 80          | SLOPE    | 0                | 30             | Х              | 30             |        | AAW   |     |         |          |
| 276  | 279 | 6/22/2017 | TT               | 4:59 PM       | 80          | SLOPE    | 0                | 2              | Х              | 2              |        | AAW   |     |         |          |
| 277  | 279 | 6/22/2017 | TT               | 5:00 PM       | 80          | SLOPE    | 0                | 24             | X              | 24             |        | AAW   |     |         |          |
| 275  | 279 | 6/22/2017 | TT               | -             | -           | SLOPE    | 0                | 2              |                | 2              | Х      | AAW   |     |         |          |
| 279  | 280 | 6/22/2017 | TT               | 5:07 PM       | 80          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |          |
| 275  | 280 | 6/22/2017 | TT               | 5:10 PM       | 80          | SLOPE    | 0                | 26             |                | 26             |        | AAW   |     |         |          |
| 279  | 280 | 6/22/2017 | TT               | 5:13 PM       | 80          | SLOPE    | 0                | 15             | X              | 15             |        | AAW   |     |         |          |
| 274  | 280 | 6/22/2017 | TT               | 5:15 PM       | 80          | SLOPE    | 0                | 14             | X              | 14             |        | AAW   |     |         |          |
| 280  | 281 | 6/22/2017 | TT               | 5:17 PM       | 80          | SLOPE    | 0                | 22             | X              | 22             |        | AAW   |     |         |          |
| 274  | 281 | 6/22/2017 | TT               | 5:20 PM       | 80          | SLOPE    | 0                | 29             | X              | 29             |        | AAW   |     |         |          |
| 273  | 280 | 6/22/2017 | TT               | 5:28 PM       | 80          | SLOPE    | 0                | 23             | X              | 23             |        | AAW   |     |         |          |
| 272  | 280 | 6/22/2017 | TT               | 5:32 PM       | 80          | SLOPE    | 0                | 32             | X              | 32             |        | AAW   |     |         |          |
| 281  | 282 | 6/22/2017 | TT               | 5:40 PM       | 80          | SLOPE    | 0                | 24             | X              | 24             |        | AAW   | 64  | 14      |          |
| 274  | 282 | 6/22/2017 | TT               | 5:45 PM       | 80          | SLOPE    | 0                | 36             | Х              | 36             |        | AAW   |     |         |          |
| 271  | 281 | 6/22/2017 | TT               | 5:59 PM       | 80          | SLOPE    | 0                | 11             | X              | 11             |        | AAW   |     |         |          |
| 273  | 281 | 6/22/2017 | TT               | 6:02 PM       | 80          | SLOPE    | 0                | 20             | X              | 20             |        | AAW   |     |         |          |
| 208  | 281 | 6/22/2017 | TT               | 6:10 PM       | 80          | SLOPE    | 0                | 111            | X              | 111            |        | AAW   |     |         |          |
| 270  | 283 | 6/22/2017 | TT               | 6:22 PM       | 80          | SLOPE    | 0                | 95             | X              | 95             |        | AAW   |     |         |          |
| 281  | PS  | 6/22/2017 | TT               | 6:25 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |          |
| 284  | 285 | 6/22/2017 | TT               | 6:57 PM       | 80          | SLOPE    | 0                | 8              | Х              | 8              |        | AAW   |     |         |          |
| 283  | 284 | 6/22/2017 | TT               | 6:58 PM       | 80          | SLOPE    | 0                | 19             | X              | 19             |        | AAW   |     |         |          |
| 283  | 285 | 6/22/2017 | TT               | 7:01 PM       | 80          | SLOPE    | 0                | 45             | Х              | 45             |        | AAW   | 66  | 18      |          |



| From | То  | Date     | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 107  | 143 | 6/6/2017 | TT               | 11:40 AM      | 80          | SLOPE    | 0                | 50             | Х              | 50             |        | BJD   |     |         |          |
| 109  | 143 | 6/6/2017 | TT               | 11:50 AM      | 80          | SLOPE    | 0                | 52             |                | 52             |        | BJD   |     |         |          |
| 109  | 143 | 6/6/2017 | TT               | 11:58 AM      | 80          | SLOPE    | 52               | 102            |                | 50             |        | BJD   |     |         |          |
| 109  | 143 | 6/6/2017 | TT               | 12:07 PM      | 80          | SLOPE    | 103              | 127            | X              | 24             |        | BJD   |     |         |          |
| 143  | 144 | 6/6/2017 | TT               | 1:42 PM       | 83          | SLOPE    | 0                | 113            |                | 113            |        | BJD   |     |         |          |
| 143  | 144 | 6/6/2017 | TT               | 2:09 PM       | 83          | SLOPE    | 113              | 175            | Х              | 62             |        | BJD   |     |         |          |
| 146  | 147 | 6/6/2017 | TT               | 3:00 PM       | 83          | SLOPE    | 0                | 73             | Х              | 73             |        | BJD   |     |         |          |
| 146  | 148 | 6/6/2017 | TT               | 3:14 PM       | 83          | SLOPE    | 0                | 42             | Х              | 42             |        | BJD   |     |         |          |
| 152  | 153 | 6/6/2017 | TT               | 3:52 PM       | 83          | SLOPE    | 22               | 129            | Х              | 107            |        | BJD   | 29  | 56      |          |
| 152  | 154 | 6/6/2017 | TT               | 4:12 PM       | 80          | SLOPE    | 0                | 19             | X              | 19             |        | BJD   |     |         |          |
| 153  | 155 | 6/6/2017 | TT               | 4:19 PM       | 80          | SLOPE    | 0                | 153            | Х              | 153            |        | BJD   |     |         |          |
| 152  | 153 | 6/6/2017 | TT               | 4:48 PM       | 80          | SLOPE    | 0                | 22             | Х              | 22             |        | BJD   |     |         |          |
| 145  | 153 | 6/6/2017 | TT               | 4:49 PM       | 80          | SLOPE    | 0                | 26             | Х              | 26             |        | BJD   |     |         |          |
| 154  | 155 | 6/6/2017 | TT               | 4:50 PM       | 80          | SLOPE    | 0                | 24             | Х              | 24             |        | BJD   |     |         |          |
| 145  | 155 | 6/6/2017 | TT               | 5:09 PM       | 80          | SLOPE    | 0                | 11             | Х              | 11             |        | BJD   |     |         |          |
| 146  | 153 | 6/6/2017 | TT               | 5:15 PM       | 80          | SLOPE    | 0                | 4              | Х              | 4              |        | BJD   |     |         |          |
| 146  | 152 | 6/6/2017 | TT               | 5:19 PM       | 80          | SLOPE    | 0                | 21             | X              | 21             |        | BJD   |     |         |          |
| 155  | 156 | 6/7/2017 | TT               | 2:04 PM       | 80          | SLOPE    | 0                | 40             |                | 40             |        | BJD   |     |         |          |
| 155  | 156 | 6/7/2017 | TT               | 2:15 PM       | 80          | SLOPE    | 40               | 65             |                | 25             |        | BJD   |     |         |          |
| 155  | 156 | 6/7/2017 | TT               | 2:20 PM       | 80          | SLOPE    | 65               | 203            | Х              | 138            |        | BJD   | 31  | 147     |          |
| 157  | 158 | 6/7/2017 | TT               | 2:44 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 156  | 157 | 6/7/2017 | TT               | 2:50 PM       | 80          | SLOPE    | 0                | 103            | Х              | 103            |        | BJD   |     |         |          |
| 156  | 158 | 6/7/2017 | TT               | 3:08 PM       | 80          | SLOPE    | 0                | 110            | Х              | 110            |        | BJD   |     |         |          |
| 157  | 159 | 6/7/2017 | TT               | 3:31 PM       | 80          | SLOPE    | 0                | 116            | X              | 116            |        | BJD   |     |         |          |
| 158  | 159 | 6/7/2017 | TT               | 3:49 PM       | 80          | SLOPE    | 0                | 110            | Х              | 110            |        | BJD   | 32  | 99      |          |
| 159  | 160 | 6/7/2017 | TT               | 4:20 PM       | 80          | SLOPE    | 0                | 215            | Х              | 215            |        | BJD   | 53  | 213     |          |
| 159  | 161 | 6/7/2017 | TT               | 5:00 PM       | 80          | SLOPE    | 0                | 5              | Х              | 5              |        | BJD   |     |         |          |



### Panel Seaming Log AG 2650

| From | То  | Date     | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments                   |
|------|-----|----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------------------------|
| 163  | 164 | 6/8/2017 | TT               | 1:40 PM       | 80          | SLOPE    | 0                | 107            | Х              | 107            |        | BJD   |     |         |                            |
| 164  | 165 | 6/8/2017 | TT               | 2:06 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |                            |
| 163  | 165 | 6/8/2017 | TT               | 2:10 PM       | 80          | SLOPE    | 0                | 78             | Х              | 78             |        | BJD   |     |         |                            |
| 164  | 166 | 6/8/2017 | TT               | 2:25 PM       | 80          | SLOPE    | 0                | 77             | Х              | 77             |        | BJD   |     |         |                            |
| 165  | 166 | 6/8/2017 | TT               | 2:34 PM       | 80          | SLOPE    | 0                | 84             | Х              | 84             |        | BJD   |     |         |                            |
| 166  | 167 | 6/8/2017 | TT               | 2:47 PM       | 80          | SLOPE    | 0                | 134            | Х              | 134            |        | BJD   |     |         |                            |
| 167  | 168 | 6/8/2017 | TT               | 3:09 PM       | 80          | SLOPE    | 0                | 108            | Х              | 108            |        | BJD   | 33  | 4       |                            |
| 168  | 169 | 6/8/2017 | TT               | 3:28 PM       | 80          | SLOPE    | 0                | 56             | Х              | 56             |        | BJD   |     |         |                            |
| 169  | 170 | 6/8/2017 | TT               | 3:38 PM       | 80          | SLOPE    | 0                | 29             | Х              | 29             |        | BJD   |     |         |                            |
| 168  | 170 | 6/8/2017 | TT               | 3:43 PM       | 80          | SLOPE    | 0                | 33             | Х              | 33             |        | BJD   |     |         |                            |
| 167  | 170 | 6/8/2017 | TT               | 3:47 PM       | 80          | SLOPE    | 0                | 33             | Х              | 33             |        | BJD   |     |         |                            |
| 166  | 170 | 6/8/2017 | TT               | 3:52 PM       | 80          | SLOPE    | 0                | 33             | Х              | 33             |        | BJD   |     |         |                            |
| 164  | 170 | 6/8/2017 | TT               | 3:56 PM       | 80          | SLOPE    | 0                | 33             | Х              | 33             |        | BJD   |     |         |                            |
| 163  | 170 | 6/8/2017 | TT               | 3:58 PM       | 80          | SLOPE    | 0                | 30             | Х              | 30             |        | BJD   |     |         |                            |
| 162  | 170 | 6/8/2017 | TT               | 4:08 PM       | 80          | SLOPE    | 0                | 28             | Х              | 28             |        | BJD   |     |         |                            |
| 170  | 171 | 6/8/2017 | TT               | 4:14 PM       | 80          | SLOPE    | 0                | 268            | Х              | 268            |        | BJD   | 34  | 121     |                            |
| 172  | 173 | 6/8/2017 | TT               | 4:58 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |                            |
| 173  | 174 | 6/8/2017 | TT               | 5:09 PM       | 80          | SLOPE    | 0                | 140            | Х              | 140            |        | BJD   |     |         |                            |
| 172  | 174 | 6/8/2017 | TT               | 5:31 PM       | 80          | SLOPE    | 0                | 10             | Х              | 10             |        | BJD   |     |         |                            |
| 175  | 176 | 6/8/2017 | TT               | 5:34 PM       | 80          | SLOPE    | 0                | 75             | Х              | 75             |        | BJD   |     |         |                            |
| 176  | 177 | 6/8/2017 | TT               | 5:46 PM       | 80          | SLOPE    | 0                | 37             | Х              | 37             |        | BJD   |     |         |                            |
| 170  | 178 | 6/8/2017 | TT               | 5:50 PM       | 80          | SLOPE    | 0                | 13             | Х              | 13             |        | BJD   |     |         |                            |
| 169  | 178 | 6/8/2017 | TT               | 5:52 PM       | 80          | SLOPE    | 0                | 18             | Х              | 18             |        | BJD   |     |         |                            |
| 171  | 179 | 6/9/2017 | TT               | 10:09 AM      | 75          | SLOPE    | 6                | 35             | Х              | 29             |        | BJD   |     |         | 0-6 Capped                 |
| 173  | 179 | 6/9/2017 | TT               | 10:14 AM      | 75          | SLOPE    | 0                | 35             | Х              | 35             |        | BJD   | 35  | 15      |                            |
| 174  | 179 | 6/9/2017 | TT               | 10:19 AM      | 75          | SLOPE    | 0                | 35             | Х              | 35             |        | BJD   |     |         |                            |
| 175  | 179 | 6/9/2017 | TT               | 10:26 AM      | 75          | SLOPE    | 0                | 35             | Х              | 35             |        | BJD   |     |         |                            |
| 176  | 179 | 6/9/2017 | TT               | 10:34 AM      | 75          | SLOPE    | 0                | 25             | Х              | 25             |        | BJD   |     |         |                            |
| 179  | 180 | 6/9/2017 | TT               | 10:38 AM      | 75          | SLOPE    | 0                | 10             |                | 10             |        | BJD   |     |         |                            |
| 179  | 180 | 6/9/2017 | TT               | 10:39 AM      | 75          | SLOPE    | 10               | 15             | Х              | 5              |        | BJD   |     |         |                            |
| 176  | 180 | 6/9/2017 | TT               | 10:40 AM      | 75          | SLOPE    | 0                | 10             | X              | 10             |        | BJD   |     |         |                            |
| 177  | 180 | 6/9/2017 | TT               | 10:50 AM      | 75          | SLOPE    | 0                | 33             | Х              | 33             |        | BJD   |     |         |                            |
| 181  | 182 | 6/9/2017 | TT               | 10:52 AM      | 75          | SLOPE    | 0                | 93             | Х              | 93             |        | BJD   |     |         |                            |
| 181  | 183 | 6/9/2017 | TT               | 11:17 AM      | 80          | SLOPE    | 0                | 77             | Х              | 77             |        | BJD   |     |         |                            |
| 182  | 185 | 6/9/2017 | TT               | 11:40 AM      | 80          | SLOPE    | 0                | 90             | Х              | 90             |        | BJD   |     |         | Note: 182/184 to be capped |
| 184  | 185 | 6/9/2017 | TT               | 1:02 PM       | 80          | SLOPE    | 0                | 63             | Х              | 63             |        | BJD   |     |         |                            |



### Panel Seaming Log AG 2650

| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments                  |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|---------------------------|
| 185  | 186 | 6/9/2017  | TT               | 1:16 PM       | 80          | SLOPE    | 0                | 5              | Х              | 5              |        | BJD   |     |         |                           |
| 186  | 187 | 6/9/2017  | TT               | 1:20 PM       | 80          | SLOPE    | 0                | 91             | X              | 91             |        | BJD   | 36  | 4       |                           |
| 185  | 187 | 6/9/2017  | TT               | 1:28 PM       | 80          | SLOPE    | 0                | 42             | X              | 42             |        | BJD   |     |         |                           |
| 185  | 189 | 6/9/2017  | TT               | 1:42 PM       | 80          | SLOPE    | 0                | 79             | Х              | 79             |        | BJD   |     |         |                           |
| 189  | 190 | 6/9/2017  | TT               | 2:17 PM       | 85          | SLOPE    | 0                | 187            | X              | 187            |        | BJD   |     |         |                           |
| 185  | 190 | 6/9/2017  | TT               | 2:52 PM       | 85          | SLOPE    | 0                | 40             | X              | 40             |        | BJD   |     |         |                           |
| 191  | 192 | 6/9/2017  | TT               | 3:02 PM       | 85          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |                           |
| 192  | 193 | 6/9/2017  | TT               | 3:08 PM       | 85          | SLOPE    | 0                | 26             |                | 26             |        | BJD   |     |         |                           |
| 192  | 193 | 6/9/2017  | TT               | 3:11 PM       | 85          | SLOPE    | 26               | 91             | Х              | 65             |        | BJD   | 37  | 18      |                           |
| 191  | 193 | 6/9/2017  | TT               | 3:22 PM       | 85          | SLOPE    | 0                | 118            | X              | 118            |        | BJD   |     |         |                           |
| 194  | 195 | 6/9/2017  | TT               | 3:47 PM       | 85          | SLOPE    | 0                | 47             | X              | 47             |        | BJD   |     |         |                           |
| 195  | 196 | 6/9/2017  | TT               | 4:11 PM       | 85          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |                           |
| 195  | 197 | 6/9/2017  | TT               | 4:20 PM       | 85          | SLOPE    | 0                | 37             | X              | 37             |        | BJD   |     |         |                           |
| 196  | 197 | 6/9/2017  | TT               | 4:27 PM       | 85          | SLOPE    | 0                | 146            | X              | 146            |        | BJD   |     |         |                           |
| 198  | 199 | 6/10/2017 | TT               | 8:08 AM       | 80          | SLOPE    | 0                | 36             | X              | 36             |        | BJD   |     |         |                           |
| 199  | 200 | 6/10/2017 | TT               | 8:17 AM       | 80          | SLOPE    | 0                | 11             |                | 11             |        | BJD   |     |         | 11-16: Pipe Boat (16 EOS) |
| 198  | 200 | 6/10/2017 | TT               | 8:19 AM       | 80          | SLOPE    | 0                | 51             |                | 51             |        | BJD   | 44  | 42      |                           |
| 198  | 200 | 6/10/2017 | TT               | 8:29 AM       | 80          | SLOPE    | 59               | 128            | Х              | 69             |        | BJD   | 54  | 126     | 51-59: Pipe Boat          |
| 201  | 202 | 6/10/2017 | TT               | 8:46 AM       | 80          | SLOPE    | 0                | 9              |                | 9              |        | BJD   |     |         | Patch: 9                  |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments            |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|---------------------|
| 171  | 173 | 6/8/2017  | TT               | 4:38 PM       | 80          | SLOPE    | 0                | 171            | Х              | 171            |        | BJD   |     |         |                     |
| 171  | 172 | 6/8/2017  | TT               | 5:03 PM       | 80          | SLOPE    | 0                | 26             | Х              | 26             |        | BJD   |     |         |                     |
| 174  | 175 | 6/8/2017  | TT               | 5:13 PM       | 80          | SLOPE    | 0                | 120            | Х              | 120            |        | BJD   |     |         |                     |
| 180  | 181 | 6/9/2017  | TT               | 10:40 AM      | 75          | SLOPE    | 0                | 52             | Х              | 52             |        | BJD   |     |         |                     |
| 179  | 181 | 6/9/2017  | TT               | 10:50 AM      | 75          | SLOPE    | 0                | 160            | Х              | 160            |        | BJD   | 38  | 131     |                     |
| 181  | 184 | 6/9/2017  | TT               | 11:26 AM      | 75          | SLOPE    | 0                | 51             | Х              | 51             |        | BJD   |     |         |                     |
| 171  | 181 | 6/9/2017  | TT               | 11:40 AM      | 80          | SLOPE    | 0                | 25             | Х              | 25             |        | BJD   |     |         |                     |
| 183  | 186 | 6/9/2017  | TT               | 1:16 PM       | 80          | SLOPE    | 0                | 77             | Х              | 77             |        | BJD   |     |         |                     |
| 187  | 188 | 6/9/2017  | TT               | 1:37 PM       | 80          | SLOPE    | 0                | 62             | Х              | 62             |        | BJD   |     |         |                     |
| 188  | 189 | 6/9/2017  | TT               | 1:51 PM       | 80          | SLOPE    | 0                | 49             | Χ              | 49             |        | BJD   |     |         |                     |
| 187  | 189 | 6/9/2017  | TT               | 2:01 PM       | 85          | SLOPE    | 0                | 67             | Χ              | 67             |        | BJD   |     |         |                     |
| 190  | 191 | 6/9/2017  | TT               | 2:25 PM       | 85          | SLOPE    | 0                | 121            | Χ              | 121            |        | BJD   | 39  | 42      |                     |
| 190  | 192 | 6/9/2017  | TT               | 2:55 PM       | 85          | SLOPE    | 0                | 98             | Х              | 98             |        | BJD   |     |         |                     |
| 193  | 194 | 6/9/2017  | TT               | 3:20 PM       | 85          | SLOPE    | 0                | 203            | Х              | 203            |        | BJD   |     |         |                     |
| 194  | 196 | 6/9/2017  | TT               | 4:12 PM       | 85          | SLOPE    | 0                | 151            | Х              | 151            |        | BJD   |     |         |                     |
| 197  | 198 | 6/10/2017 | TT               | 7:50 AM       | 80          | SLOPE    | 0                | 176            | Х              | 176            |        | BJD   | 42  | 67      |                     |
| 199  | 201 | 6/10/2017 | TT               | 8:36 AM       | 80          | SLOPE    | 0                | 28             | Х              | 28             |        | BJD   |     |         |                     |
| 200  | 201 | 6/10/2017 | TT               | 8:45 AM       | 80          | SLOPE    | 0                | 128            | Х              | 128            |        | BJD   |     |         |                     |
| 201  | 202 | 6/10/2017 | TT               | 9:12 AM       | 80          | SLOPE    | 9                | 102            | Х              | 93             |        | BJD   |     |         |                     |
| 201  | 203 | 6/10/2017 | TT               | 9:32 AM       | 80          | SLOPE    | 0                | 50             | Х              | 50             |        | BJD   |     |         |                     |
| 202  | 203 | 6/10/2017 | TT               | 9:45 AM       | 80          | SLOPE    | 0                | 10             |                | 10             |        | BJD   |     |         | 10-16: Repair (TMP) |
| 202  | 204 | 6/10/2017 | TT               | 10:04 AM      | 80          | SLOPE    | 0                | 75             | Х              | 75             |        | BJD   |     |         |                     |
| 203  | 204 | 6/10/2017 | TT               | 10:15 AM      | 80          | SLOPE    | 0                | 48             | Х              | 48             |        | BJD   | 43  | 7       |                     |
| 198  | PS  | 6/10/2017 | TT               | 10:29 AM      | 80          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |                     |
| 200  | PS  | 6/10/2017 | TT               | 10:31 AM      | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |                     |
| 201  | PS  | 6/10/2017 | TT               | 10:33 AM      | 80          | SLOPE    | 0                | 9              |                | 9              |        | BJD   |     |         |                     |
| 201  | PS  | 6/10/2017 | TT               | 10:36 AM      | 80          | SLOPE    | 9                | 16             | Х              | 7              |        | BJD   |     |         |                     |
| 203  | PS  | 6/10/2017 | TT               | 10:40 AM      | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   | 55B | 14      |                     |
| 204  | PS  | 6/10/2017 | TT               | 10:41 AM      | 80          | SLOPE    | 0                | 16             | Х              | 16             | Х      | BJD   | 55  | 12      |                     |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| 202  | 205 | 6/12/2017 | TT               | 8:59 AM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 204  | 205 | 6/12/2017 | TT               | 8:00 AM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 207  | 208 | 6/12/2017 | TT               | 9:10 AM       | 80          | SLOPE    | 0                | 24             |                | 24             |        | BJD   |     |         |          |
| 207  | 208 | 6/12/2017 | TT               | 9:15 AM       | 80          | SLOPE    | 24               | 115            | Х              | 91             |        | BJD   | 56  | 105     |          |



| From | То   | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments    |
|------|------|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|-------------|
| 205  | 206  | 6/12/2017 | TT               | 8:14 AM       | 80          | SLOPE    | 0                | 14             | Х              | 14             |        | BJD   |     |         |             |
| 204  | 206  | 6/12/2017 | TT               | 8:18 AM       | 80          | SLOPE    | 0                | 120            | Х              | 120            |        | BJD   |     |         |             |
| 206  | 207  | 6/12/2017 | TT               | 8:39 AM       | 80          | SLOPE    | 0                | 126            | Х              | 126            |        | BJD   |     |         |             |
| 197  | R244 | 6/12/2017 | TT               | 9:40 AM       | 80          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |             |
| 196  | R244 | 6/12/2017 | TT               | 9:44 AM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |             |
| 194  | R244 | 6/12/2017 | TT               | 9:46 AM       | 80          | SLOPE    | 0                | 5              | Х              | 5              |        | BJD   |     |         |             |
| 194  | R245 | 6/12/2017 | TT               | 9:47 AM       | 80          | SLOPE    | 0                | 10             | Χ              | 10             |        | BJD   |     |         |             |
| 193  | R245 | 6/12/2017 | TT               | 9:49 AM       | 80          | SLOPE    | 0                | 16             | Χ              | 16             |        | BJD   |     |         |             |
| R245 | PS   | 6/12/2017 | TT               | 10:01 AM      | 85          | SLOPE    | 0                | 25             | Χ              | 25             |        | BJD   |     |         |             |
| R244 | PS   | 6/12/2017 | TT               | 10:04 AM      | 85          | SLOPE    | 0                | 16             |                | 16             |        | BJD   |     |         |             |
| R244 | PS   | 6/12/2017 | TT               | 10:06 AM      | 85          | SLOPE    | 16               | 35             | Х              | 19             |        | BJD   |     |         |             |
| 191  | R246 | 6/12/2017 | TT               | 10:18 AM      | 85          | SLOPE    | 0                | 12             | Χ              | 12             |        | BJD   |     |         |             |
| 191  | R247 | 6/12/2017 | TT               | 10:20 AM      | 85          | SLOPE    | 0                | 4              | Х              | 4              |        | BJD   |     |         |             |
| 190  | R247 | 6/12/2017 | TT               | 10:20 AM      | 85          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |             |
| 185  | R247 | 6/12/2017 | TT               | 10:22 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |             |
| 184  | R248 | 6/12/2017 | TT               | 10:23 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |             |
| 171  | R249 | 6/12/2017 | TT               | 10:31 AM      | 85          | SLOPE    | 0                | 4              |                | 4              |        | BJD   |     |         |             |
| 171  | R249 | 6/12/2017 | TT               | 10:31 AM      | 85          | SLOPE    | 4                | 13             | Х              | 9              |        | BJD   |     |         |             |
| 170  | R249 | 6/12/2017 | TT               | 10:33 AM      | 85          | SLOPE    | 0                | 7              | Х              | 7              |        | BJD   |     |         |             |
| R249 | PS   | 6/12/2017 | TT               | 10:38 AM      | 85          | SLOPE    | 0                | 15             |                | 15             |        | BJD   |     |         |             |
| R249 | PS   | 6/12/2017 | TT               | 10:42 AM      | 85          | SLOPE    | 15               | 21             | Х              | 6              |        | BJD   |     |         |             |
| R248 | PS   | 6/12/2017 | TT               | 10:43 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |             |
| R247 | PS   | 6/12/2017 | TT               | 10:46 AM      | 85          | SLOPE    | 0                | 27             | Х              | 27             |        | BJD   | 45  | 9       |             |
| R246 | PS   | 6/12/2017 | TT               | 10:50 AM      | 85          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |             |
| R256 | R257 | 6/12/2017 | TT               | 10:58 AM      | 85          | SLOPE    | 0                | 13             | Х              | 13             |        | BJD   |     |         |             |
| 160  | R256 | 6/12/2017 | TT               | 11:02 AM      | 85          | SLOPE    | 0                | 10             | Χ              | 10             |        | BJD   |     |         |             |
| 160  | R257 | 6/12/2017 | TT               | 11:04 AM      | 85          | SLOPE    | 0                | 6              | X              | 6              |        | BJD   |     |         |             |
| 162  | R257 | 6/12/2017 | TT               | 11:05 AM      | 85          | SLOPE    | 0                | 4              | Χ              | 4              |        | BJD   |     |         |             |
| 170  | R257 | 6/12/2017 | TT               | 11:06 AM      | 85          | SLOPE    | 0                | 13             | Χ              | 13             |        | BJD   |     |         |             |
| 170  | R256 | 6/12/2017 | TT               | 11:08 AM      | 85          | SLOPE    | 0                | 8              | Χ              | 8              |        | BJD   |     |         |             |
| 159  | R256 | 6/12/2017 | TT               | 11:12 AM      | 85          | SLOPE    | 0                | 8              |                | 8              |        | BJD   |     |         | Patch: 8-10 |
| 159  | R256 | 6/12/2017 | TT               | 11:16 AM      | 85          | SLOPE    | 10               | 16             | X              | 6              |        | BJD   |     |         |             |
| R258 | 171  | 6/12/2017 | TT               | 11:19 AM      | 85          | SLOPE    | 0                | 12             | X              | 12             |        | BJD   |     |         |             |
| R258 | 181  | 6/12/2017 | TT               | 11:23 AM      | 85          | SLOPE    | 0                | 4              | X              | 4              |        | BJD   |     |         |             |
| R258 | 184  | 6/12/2017 | TT               | 11:24 AM      | 85          | SLOPE    | 0                | 9              | X              | 9              |        | BJD   |     |         |             |
| 170  | R250 | 6/12/2017 | TT               | 11:26 AM      | 85          | SLOPE    | 0                | 6              | Х              | 6              |        | BJD   |     |         |             |



| From | То   | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments |
|------|------|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------|
| R251 | R256 | 6/12/2017 | TT               | 11:28 AM      | 85          | SLOPE    | 0                | 9              | Х              | 9              |        | BJD   |     |         |          |
| 159  | R251 | 6/12/2017 | TT               | 11:29 AM      | 85          | SLOPE    | 0                | 6              | Х              | 6              |        | BJD   |     |         |          |
| 159  | R252 | 6/12/2017 | TT               | 11:30 AM      | 85          | SLOPE    | 0                | 11             | X              | 11             |        | BJD   |     |         |          |
| 157  | R253 | 6/12/2017 | TT               | 11:35 AM      | 85          | SLOPE    | 0                | 20             | X              | 20             |        | BJD   |     |         |          |
| R250 | PS   | 6/12/2017 | TT               | 11:42 AM      | 85          | SLOPE    | 0                | 8              | X              | 8              |        | BJD   |     |         |          |
| R251 | PS   | 6/12/2017 | TT               | 11:44 AM      | 85          | SLOPE    | 0                | 9              |                | 9              |        | BJD   |     |         |          |
| R251 | PS   | 6/12/2017 | TT               | 11:45 AM      | 85          | SLOPE    | 9                | 16             | X              | 7              |        | BJD   |     |         |          |
| R252 | PS   | 6/12/2017 | TT               | 11:46 AM      | 85          | SLOPE    | 0                | 12             | Х              | 12             |        | BJD   |     |         |          |
| R253 | PS   | 6/12/2017 | TT               | 11:52 AM      | 85          | SLOPE    | 0                | 21             | Х              | 21             |        | BJD   |     |         |          |
| 145  | R255 | 6/12/2017 | TT               | 1:13 PM       | 90          | SLOPE    | 0                | 13             | Х              | 13             |        | BJD   |     |         |          |
| 155  | R254 | 6/12/2017 | TT               | 1:16 PM       | 90          | SLOPE    | 0                | 10             | Х              | 10             |        | BJD   |     |         |          |
| 156  | R254 | 6/12/2017 | TT               | 1:18 PM       | 90          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| R254 | PS   | 6/12/2017 | TT               | 1:25 PM       | 90          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |          |
| R254 | PS   | 6/12/2017 | TT               | 1:33 PM       | 90          | SLOPE    | 0                | 11             | Х              | 11             |        | BJD   |     |         |          |
| R255 | PS   | 6/12/2017 | TT               | 1:39 PM       | 90          | SLOPE    | 0                | 13             | Х              | 13             |        | BJD   |     |         |          |
| 181  | PE3  | 6/12/2017 | TT               | 1:47 PM       | 95          | SLOPE    | 0                | 8              | Х              | 8              |        | BJD   |     |         |          |
| 182  | PE3  | 6/12/2017 | TT               | 1:50 PM       | 95          | SLOPE    | 0                | 10             | Х              | 10             |        | BJD   |     |         |          |
| 186  | PE3  | 6/12/2017 | TT               | 1:54 PM       | 95          | SLOPE    | 0                | 7              | Х              | 7              |        | BJD   |     |         |          |
| 183  | PE3  | 6/12/2017 | TT               | 2:01 PM       | 95          | SLOPE    | 0                | 12             | Х              | 12             |        | BJD   |     |         |          |
| 206  | PS   | 6/12/2017 | TT               | 2:21 PM       | 95          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |          |
| 207  | PS   | 6/12/2017 | TT               | 2:24 PM       | 95          | SLOPE    | 0                | 3              |                | 3              |        | BJD   |     |         |          |
| 207  | PS   | 6/12/2017 | TT               | 2:25 PM       | 95          | SLOPE    | 3                | 16             | Х              | 13             |        | BJD   |     |         |          |
| 208  | PS   | 6/12/2017 | TT               | 2:30 PM       | 95          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 226  | 227  | 6/14/2017 | TT               | 9:24 AM       | 80          | SLOPE    | 0                | 64             |                | 64             |        | BJD   |     |         |          |
| 226  | 227  | 6/14/2017 | TT               | 9:35 AM       | 80          | SLOPE    | 64               | 71             |                | 7              |        | BJD   |     |         |          |
| 226  | 227  | 6/14/2017 | TT               | 9:40 AM       | 80          | SLOPE    | 71               | 86             | Х              | 15             |        | BJD   |     |         |          |
| 228  | 229  | 6/14/2017 | TT               | 9:50 AM       | 80          | SLOPE    | 0                | 88             | X              | 88             |        | BJD   | 51  | 29      |          |
| 230  | 231  | 6/14/2017 | TT               | 10:13 AM      | 80          | SLOPE    | 0                | 89             | Х              | 89             |        | BJD   |     |         |          |
| 232  | 233  | 6/14/2017 | TT               | 10:37 AM      | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |          |
| 227  | PS   | 6/14/2017 | TT               | 10:45 AM      | 80          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |          |
| 234  | 235  | 6/14/2017 | TT               | 11:35 AM      | 80          | SLOPE    | 0                | 67             | X              | 67             |        | BJD   |     |         |          |
| 234  | 236  | 6/14/2017 | TT               | 11:50 AM      | 80          | SLOPE    | 0                | 17             | Х              | 17             |        | BJD   |     |         |          |
| 237  | 238  | 6/21/2017 | TT               | 9:00 AM       | 80          | SLOPE    | 0                | 80             | X              | 80             |        | AAW   |     |         |          |
| 239  | 240  | 6/21/2017 | TT               | 9:15 AM       | 80          | SLOPE    | 0                | 16             | Χ              | 16             |        | AAW   |     |         |          |
| 238  | 240  | 6/21/2017 | TT               | 9:20 AM       | 80          | SLOPE    | 0                | 34             | Χ              | 34             |        | AAW   |     |         |          |
| 238  | 239  | 6/21/2017 | TT               | 9:28 AM       | 80          | SLOPE    | 0                | 41             |                | 41             |        | AAW   |     |         |          |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments           |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|--------------------|
| 240  | 241 | 6/21/2017 | TT               | 9:58 AM       | 85          | SLOPE    | 0                | 39             | Х              | 39             |        | AAW   |     |         |                    |
| 239  | 241 | 6/21/2017 | TT               | 10:08 AM      | 85          | SLOPE    | 0                | 48             | X              | 48             |        | AAW   | 59  | 6       |                    |
| 241  | 242 | 6/21/2017 | TT               | 10:32 AM      | 85          | SLOPE    | 0                | 57             | X              | 57             |        | AAW   |     |         |                    |
| 236  | 237 | 6/21/2017 | TT               | 10:54 AM      | 85          | SLOPE    | 0                | 15             |                | 15             |        | AAW   |     |         | 15-21 (eos) capped |
| 241  | 243 | 6/21/2017 | TT               | 10:45 AM      | 85          | SLOPE    | 0                | 36             | Х              | 36             |        | AAW   |     |         |                    |
| 242  | 243 | 6/21/2017 | TT               | 10:29 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 242  | 244 | 6/21/2017 | TT               | 11:15 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 241  | 244 | 6/21/2017 | TT               | 11:18 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |                    |
| 239  | 244 | 6/21/2017 | TT               | 11:20 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |                    |
| 238  | 244 | 6/21/2017 | TT               | 11:25 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   |     |         |                    |
| 237  | 244 | 6/21/2017 | TT               | 11:28 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   | 65  | 10      |                    |
| 235  | 244 | 6/21/2017 | TT               | 11:30 AM      | 85          | SLOPE    | 0                | 11             | Х              | 11             |        | AAW   |     |         | 11-16 (eos) capped |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments             |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|----------------------|
| 209  | 217 | 6/13/2017 | TT               | 10:40 AM      | 85          | SLOPE    | 0                | 4              |                | 4              | Х      | BJD   |     |         |                      |
| 209  | 217 | 6/13/2017 | TT               | 10:40 AM      | 85          | SLOPE    | 4                | 16             | Х              | 12             |        | BJD   |     |         |                      |
| 210  | 217 | 6/13/2017 | TT               | 10:45 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |                      |
| 211  | 217 | 6/13/2017 | TT               | 10:47 AM      | 85          | SLOPE    | 0                | 16             | X              | 16             |        | BJD   |     |         |                      |
| 212  | 217 | 6/13/2017 | TT               | 10:50 AM      | 85          | SLOPE    | 0                | 16             | Х              | 16             |        | BJD   |     |         |                      |
| 215  | 217 | 6/13/2017 | TT               | 10:54 AM      | 85          | SLOPE    | 0                | 15             | Х              | 15             |        | BJD   |     |         |                      |
| 216  | 217 | 6/13/2017 | TT               | 10:55 AM      | 85          | SLOPE    | 0                | 10             |                | 10             |        | BJD   |     |         |                      |
| 216  | 217 | 6/13/2017 | TT               | 10:58 AM      | 85          | SLOPE    | 10               | 16             | Х              | 6              |        | BJD   |     |         |                      |
| 219  | 220 | 6/13/2017 | TT               | 11:01 AM      | 85          | SLOPE    | 0                | 10             | Х              | 10             |        | BJD   |     |         |                      |
| 218  | 220 | 6/13/2017 | TT               | 11:02 AM      | 85          | SLOPE    | 0                | 73             |                | 73             |        | BJD   |     |         | 73-77: Patch (73-77) |
| 218  | 220 | 6/13/2017 | TT               | 11:25 AM      | 85          | SLOPE    | 77               | 81             | X              | 4              |        | BJD   |     |         |                      |
| 220  | 221 | 6/13/2017 | TT               | 11:36 AM      | 85          | SLOPE    | 0                | 69             | Х              | 69             |        | BJD   | 57B | 67      |                      |
| 221  | 222 | 6/13/2017 | TT               | 11:27 AM      | 85          | SLOPE    | 0                | 8              |                | 8              | Х      | BJD   |     |         | Pipe Boot            |
| 221  | 222 | 6/13/2017 | TT               | 11:27 AM      | 85          | SLOPE    | 8                | 16             | Х              | 8              | Х      | BJD   |     |         |                      |
| 220  | 222 | 6/13/2017 | TT               | 11:47 AM      | 85          | SLOPE    | 0                | 2              |                | 2              | Х      | BJD   |     |         | 2-10: Pipe Boot      |
| 220  | 222 | 6/13/2017 | TT               | 12:28 PM      | 90          | SLOPE    | 10               | 20             | Х              | 10             | Х      | BJD   | 57  | 18      |                      |



| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments         |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|------------------|
| 225  | 226 | 6/14/2017 | TT               | 9:05 AM       | 80          | SLOPE    | 0                | 87             | Х              | 87             |        | BJD   |     |         |                  |
| 227  | 228 | 6/14/2017 | TT               | 9:31 AM       | 80          | SLOPE    | 0                | 83             |                | 83             |        | BJD   |     |         | 83-88: CAP       |
| 229  | 230 | 6/14/2017 | TT               | 10:00 AM      | 80          | SLOPE    | 0                | 88             | Х              | 88             |        | BJD   |     |         |                  |
| 232  | 234 | 6/14/2017 | TT               | 10:21 AM      | 80          | SLOPE    | 0                | 59             | Х              | 59             |        | BJD   |     |         |                  |
| 231  | 233 | 6/14/2017 | TT               | 10:42 AM      | 80          | SLOPE    | 0                | 31             | Х              | 31             |        | BJD   |     |         |                  |
| 231  | 232 | 6/14/2017 | TT               | 10:47 AM      | 80          | SLOPE    | 0                | 27             |                | 27             |        | BJD   |     |         | Pipe Boot: 27-30 |
| 231  | 232 | 6/14/2017 | TT               | 10:51 AM      | 80          | SLOPE    | 30               | 36             |                | 6              |        | BJD   |     |         | Pipe Boot: 36-37 |
| 231  | 232 | 6/14/2017 | TT               | 10:53 AM      | 80          | SLOPE    | 37               | 43             |                | 6              |        | BJD   |     |         | Pipe Boot: 43    |
| 231  | 232 | 6/14/2017 | TT               | 10:55 AM      | 80          | SLOPE    | 43               | 57             | Х              | 14             |        | BJD   |     |         |                  |
| 233  | 234 | 6/14/2017 | TT               | 11:15 AM      | 80          | SLOPE    | 0                | 28             | Х              | 28             |        | BJD   |     |         |                  |
| 235  | 237 | 6/21/2017 | TT               | 8:45 AM       | 80          | SLOPE    | 0                | 58             | Х              | 58             |        | AAW   | 60  | 50      |                  |



## Panel Seaming Log WL x15

| From | То  | Date      | Material<br>Type | Start<br>Time | Amb<br>Temp | Location | Station<br>Start | Station<br>End | End of<br>Seam | Seam<br>Length | Capped | QA ID | DS# | DS Sta. | Comments           |
|------|-----|-----------|------------------|---------------|-------------|----------|------------------|----------------|----------------|----------------|--------|-------|-----|---------|--------------------|
| 269  | PS  | 6/23/2017 | TT               | 2:10 PM       | 80          | SLOPE    | 7                | 11             | Х              | 4              |        | AAW   |     |         | 11-13 (eos) capped |
| 268  | PS  | 6/23/2017 | TT               | 2:21 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 267  | PS  | 6/23/2017 | TT               | 2:29 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 266  | PS  | 6/23/2017 | TT               | 2:43 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 265  | PS  | 6/23/2017 | TT               | 3:17 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 263  | PS  | 6/23/2017 | TT               | 3:46 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 264  | PS  | 6/23/2017 | TT               | 3:51 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 262  | PS  | 6/23/2017 | TT               | 4:16 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 261  | PS  | 6/23/2017 | TT               | 4:52 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 260  | PS  | 6/23/2017 | TT               | 5:06 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 259  | PS  | 6/23/2017 | TT               | 5:31 PM       | 80          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 258  | PS  | 6/24/2017 | TT               | 8:08 AM       | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 257  | PS  | 6/24/2017 | TT               | 8:12 AM       | 70          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |                    |
| 256  | PS  | 6/24/2017 | TT               | 8:23 AM       | 70          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |                    |
| 255  | PS  | 6/24/2017 | TT               | 9:10 AM       | 70          | SLOPE    | 0                | 15             | Х              | 15             |        | AAW   |     |         |                    |
| 253  | PS  | 6/24/2017 | TT               | 9:40 AM       | 70          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |                    |
| 252  | PS  | 6/24/2017 | TT               | 10:01 AM      | 70          | SLOPE    | 0                | 24             | X              | 24             |        | AAW   |     |         |                    |
| 245  | PS  | 6/24/2017 | TT               | 10:50 AM      | 70          | SLOPE    | 0                | 17             | Х              | 17             |        | AAW   |     |         |                    |
| 246  | PS  | 6/24/2017 | TT               | 11:17 AM      | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 247  | PS  | 6/24/2017 | TT               | 11:36 AM      | 70          | SLOPE    | 0                | 16             | Х              | 16             |        | AAW   |     |         |                    |
| 248  | PS  | 6/24/2017 | TT               | 1:25 PM       | 80          | SLOPE    | 0                | 16             | X              | 16             |        | AAW   | 68  | 10      |                    |
| 249  | PS  | 6/24/2017 | TT               | 1:30 PM       | 80          | SLOPE    | 14               | 16             | X              | 2              |        | AAW   |     |         |                    |
| 269  | PS  | 6/26/2017 | TT               | 11:21 AM      | 75          | SLOPE    | 0                | 7              |                | 7              |        | AAW   |     |         |                    |
| 282  | PS  | 6/26/2017 | TT               | 11:25 AM      | 75          | SLOPE    | 0                | 13             | X              | 13             |        | AAW   |     |         |                    |
| 214  | 286 | 6/26/2017 | TT               | 4:00 PM       | 80          | SLOPE    | 0                | 4              | Х              | 4              |        | AAW   |     |         |                    |
| 136  | 286 | 6/26/2017 | TT               | 4:03 PM       | 80          | SLOPE    | 0                | 12             | Х              | 12             |        | AAW   |     |         |                    |
| 142  | 286 | 6/26/2017 | TT               | 4:10 PM       | 80          | SLOPE    | 0                | 34             |                | 34             |        | AAW   |     |         |                    |



#### Sub-Appendix C.6

#### **Non-Destructive Testing Results**

#### **Non-Destructive Test Log**

|           |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/17/2017 | 1    | 2    | SLOPE | BOS              | EOS            | Х              | 31              | 31              | 9:25 AM       | 9:30 AM  | Р   | İ                      |              | AT           | AAW   |          |
| 5/17/2017 | 2    | 3    | SLOPE | BOS              | EOS            | х              | 32              | 31              | 9:40 AM       | 9:45 AM  | Р   |                        |              | AT           | AAW   |          |
| 5/17/2017 | 3    | 4    | SLOPE | BOS              | 39             |                | 31              | 30              | 10:07 AM      | 10:12 AM | Р   |                        |              | AT           | AAW   |          |
| 5/17/2017 | 3    | 4    | SLOPE | 39               | 72             |                | 31              | 30              | 10:14 AM      | 10:19 AM | Р   |                        |              | AT           | AAW   |          |
| 5/17/2017 | 3    | 4    | SLOPE | 72               | EOS            | х              | 32              | 30              | 10:21 AM      | 10:26 AM | Р   |                        |              | AT           | AAW   |          |
| 5/17/2017 | 4    | 5    | SLOPE | BOS              | EOS            | х              | 31              | 29              | 10:29 AM      | 10:34 AM | Р   |                        |              | AT           | AAW   |          |
| 5/17/2017 | 5    | 6    | SLOPE | BOS              | EOS            | х              | 30              | 29              | 10:45 AM      | 10:50 AM | Р   |                        |              | AT           | AAW   |          |
| 5/18/2017 | 6    | 7    | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:54 AM       | 9:59 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 7    | 8    | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:55 AM       | 10:00 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 8    | 9    | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:59 AM       | 10:04 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 9    | 10   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:07 AM      | 10:12 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 10   | 11   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:10 AM      | 10:15 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 11   | 12   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:29 AM      | 10:34 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 11   | 13   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:14 AM      | 10:19 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 12   | 13   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:39 AM      | 10:44 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 12   | 14   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:40 AM      | 10:45 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 13   | 14   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:22 AM      | 10:27 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 14   | 15   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:23 AM      | 10:28 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 15   | 16   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:43 AM      | 11:48 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 16   | 17   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:44 AM      | 11:49 AM | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 17   | 20   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:33 PM       | 1:38 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/18/2017 | 20   | 21   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:52 PM       | 1:57 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 21   | 22   | SLOPE | BOS              | 59             |                | 30              | 30              | 2:01 PM       | 2:06 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 21   | 22   | SLOPE | 59               | 62             |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/22/2017 | 21   | 22   | SLOPE | 62               | EOS            | Х              | 30              | 30              | 9:53 AM       | 9:58 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 18   | 1    | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:55 AM       | 9:00 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 18   | 19   | SLOPE | BOS              | 10             |                | 30              | 30              | 9:46 AM       | 9:51 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 18   | 19   | SLOPE | 10               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/22/2017 | 1    | 19   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:40 AM       | 9:45 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 22   | 23   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:01 AM      | 10:06 AM | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 23   | 24   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:04 AM      | 10:09 AM | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 24   | 25   | SLOPE | BOS              | 70             |                | 30              | 30              | 10:15 AM      | 10:20 AM | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 24   | 25   | SLOPE | 70               | EOS            | Х              | 30              | 30              | 10:13 AM      | 10:18 AM | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 25   | 26   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:30 AM      | 10:35 AM | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 25   | 27   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:14 AM      | 10:19 AM | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 26   | 27   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:27 AM      | 10:32 AM | Р   |                        |              | KS           | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/22/2017 | 27   | 28   | SLOPE | BOS              | 31             |                | 30              | 30              | 4:43 PM       | 4:48 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 27   | 28   | SLOPE | 31               | 35             |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/22/2017 | 27   | 28   | SLOPE | 35               | 43             |                | 30              | 30              | 4:47 PM       | 4:52 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 27   | 28   | SLOPE | 43               | EOS            | Х              | 30              | 29              | 4:55 PM       | 5:00 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 27   | 29   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:56 PM       | 5:01 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 28   | 31   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 4:38 PM       | 4:43 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 31   | 32   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:30 PM       | 4:35 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 28   | 32   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:32 PM       | 4:37 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 29   | 32   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:31 PM       | 4:36 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 28   | 29   | SLOPE | BOS              | 26             |                | 30              | 29              | 4:33 PM       | 4:38 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 28   | 29   | SLOPE | 26               | 33             |                | 30              | 29              | 4:48 PM       | 4:53 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 28   | 29   | SLOPE | 33               | EOS            | Х              | 30              | 29              | 4:50 PM       | 4:55 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 27   | 31   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:04 PM       | 5:09 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 29   | 30   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:05 PM       | 5:10 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 30   | 33   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:23 PM       | 5:28 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 33   | 34   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:31 PM       | 5:36 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 33   | 35   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:33 PM       | 5:38 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 34   | 35   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:54 PM       | 5:59 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 34   | 36   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:53 PM       | 5:58 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/22/2017 | 35   | 36   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 6:02 PM       | 6:07 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 36   | 37   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:13 AM       | 9:18 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 36   | 38   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:10 AM       | 9:15 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 37   | 38   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:31 AM       | 9:36 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 37   | 39   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:19 AM       | 9:24 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 38   | 39   | SLOPE | BOS              | 40             |                | 30              | 29              | 9:07 AM       | 9:12 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 38   | 39   | SLOPE | 40               | EOS            | Х              | 30              | 29              | 9:08 AM       | 9:13 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 39   | 40   | SLOPE | BOS              | 46             |                | 30              | 29              | 9:40 AM       | 9:45 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 39   | 40   | SLOPE | 46               | EOS            | Х              | 30              | 30              | 9:41 AM       | 9:46 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 40   | 41   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:01 AM      | 10:06 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 41   | 43   | SLOPE | BOS              | 24             |                | 30              | 29              | 11:06 AM      | 11:11 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 41   | 43   | SLOPE | 24               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/24/2017 | 41   | 42   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:29 AM      | 10:34 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 42   | 43   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/24/2017 | 43   | 46   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:12 AM      | 11:17 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 42   | 46   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:16 AM      | 11:21 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 45   | 46   | SLOPE | BOS              | EOS            | Х              | 30              | 30              |               | 11:30 AM | Р   |                        |              | KS           | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | -               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/24/2017 | 42   | 45   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:46 AM      | 10:51 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 44   | 45   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/24/2017 | 42   | 44   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:00 AM      | 11:05 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 45   | 47   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:18 AM      | 11:23 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 44   | 47   | SLOPE | BOS              | 9              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/24/2017 | 44   | 47   | SLOPE | 9                | EOS            | Х              | 30              | 30              | 11:28 AM      | 11:33 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 47   | 48   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:39 AM      | 11:44 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 48   | 49   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:44 AM      | 11:49 AM | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 48   | 50   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:22 PM       | 1:27 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 49   | 50   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:15 PM       | 1:20 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 49   | 51   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:06 PM       | 1:11 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/24/2017 | 50   | 51   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:08 PM       | 1:13 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 52   | 53   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:11 AM      | 10:16 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 53   | 54   | SLOPE | BOS              | 54             |                | 30              | 29              | 10:12 AM      | 10:17 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 53   | 54   | SLOPE | 54               | EOS            | Х              | 30              | 30              | 10:13 AM      | 10:18 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 54   | 55   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:24 AM      | 10:29 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 55   | 56   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:25 AM      | 10:30 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 56   | 57   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:27 AM      | 10:32 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 56   | 58   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:26 AM      | 10:31 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 57   | 58   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:36 AM      | 10:41 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 57   | 59   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:35 AM      | 10:40 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 58   | 59   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:46 AM      | 10:51 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 59   | 60   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:49 AM      | 10:54 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 60   | 61   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:50 AM      | 10:55 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 61   | 62   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:51 AM      | 10:56 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 62   | 65   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:24 AM      | 11:29 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 62   | 63   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:07 AM      | 11:12 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 63   | 65   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:25 AM      | 11:30 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 63   | 64   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:18 AM      | 11:23 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 64   | 66   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:12 AM      | 11:17 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 66   | 67   | SLOPE | BOS              | 120            |                | 30              | 30              | 11:13 AM      | 11:18 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 43   | 63   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:27 AM      | 11:32 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 43   | 65   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:29 AM      | 11:34 AM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 46   | 65   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 12:46 PM      | 12:51 PM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 46   | 62   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/25/2017 | 46   | 61   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 12:48 PM      | 12:53 PM | Р   |                        |              | KS           | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/25/2017 | 45   | 61   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/25/2017 | 45   | 60   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 12:50 PM      | 12:55 PM | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 47   | 60   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:00 PM       | 1:05 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 47   | 59   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:01 PM       | 1:06 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 47   | 58   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:03 PM       | 1:08 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 48   | 58   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:13 PM       | 1:18 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 48   | 56   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:14 PM       | 1:19 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 48   | 55   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:15 PM       | 1:20 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 49   | 55   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:23 PM       | 1:28 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 49   | 54   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:25 PM       | 1:30 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 51   | 54   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:26 PM       | 1:31 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 51   | 53   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:30 PM       | 1:35 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 51   | 52   | SLOPE | BOS              | 9              |                | 30              | 29              | 1:37 PM       | 1:42 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/25/2017 | 51   | 52   | SLOPE | 9                | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/25/2017 | 41   | 63   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 4:23 PM       | 4:28 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 71   | 73   | SLOPE | 34               | 36             |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/26/2017 | 71   | 73   | SLOPE | 36               | EOS            | Х              | 30              | 30              | 5:23 PM       | 5:28 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 73   | 74   | SLOPE | BOS              | 33             |                | 30              | 30              | 5:56 PM       | 6:01 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 73   | 74   | SLOPE | 33               | EOS            | Х              | 30              | 29              | 5:12 PM       | 5:17 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 73   | 72   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:14 PM       | 5:19 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 73   | 75   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:21 PM       | 5:26 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 74   | 75   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:35 PM       | 5:40 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 74   | 76   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:55 PM       | 6:00 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 75   | 76   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:45 PM       | 5:50 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 76   | 77   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:49 PM       | 5:54 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 77   | 78   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:12 AM      | 10:17 AM | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 78   | 79   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:20 AM      | 10:25 AM | Р   |                        |              | KS           | AAW   |          |
| 5/26/2017 | 79   | 80   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:21 AM      | 10:26 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 5    | WT   | SLOPE | BOS              | 2              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 5    | WT   | SLOPE | 2                | EOS            | Х              | 30              | 30              | 9:46 AM       | 9:51 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 4    | WT   | SLOPE | BOS              | 2              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 4    | WT   | SLOPE | 2                | EOS            | Х              | 30              | 30              | 9:47 AM       | 9:52 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 3    | WT   | SLOPE | BOS              | 1              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 3    | WT   | SLOPE | 1                | 13             |                | 30              | 29              | 9:48 AM       | 9:53 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 3    | WT   | SLOPE | 13               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 2    | WT   | SLOPE | BOS              | 13             |                | 30              | 30              | 9:49 AM       | 9:54 AM  | Р   |                        |              | KS           | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/27/2017 | 2    | WT   | SLOPE | 13               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 1    | WT   | SLOPE | BOS              | 1              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 1    | WT   | SLOPE | 1                | 5              |                | 30              | 29              | 9:50 AM       | 9:55 AM  | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 1    | WT   | SLOPE | 5                | EOS            | Х              | 30              | 30              | 9:58 AM       | 10:03 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 18   | WT   | SLOPE | BOS              | 5              |                | 30              | 30              | 9:59 AM       | 10:04 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 18   | WT   | SLOPE | 5                | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 14   | WT   | SLOPE | BOS              | 5              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 14   | WT   | SLOPE | 5                | 16             |                | 30              | 29              | 11:02 AM      | 11:07 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 12   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 12   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 30              | 10:56 AM      | 11:01 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 11   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 11   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 29              | 10:53 AM      | 10:58 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 10   | WT   | SLOPE | BOS              | 5              |                | 30              | 30              | 10:52 AM      | 10:57 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 10   | WT   | SLOPE | 5                | EOS            | Х              | 30              | 30              | 10:24 AM      | 10:29 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 9    | WT   | SLOPE | BOS              | 6              |                | 30              | 29              | 10:23 AM      | 10:28 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 9    | WT   | SLOPE | 6                | EOS            | Х              | 30              | 30              | 10:21 AM      | 10:26 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 8    | WT   | SLOPE | BOS              | 6              |                | 30              | 29              | 10:20 AM      | 10:25 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 8    | WT   | SLOPE | 6                | EOS            | Х              | 30              | 30              | 10:15 AM      | 10:20 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 7    | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 7    | WT   | SLOPE | 4                | EOS            | Х              | 30              | 30              | 10:14 AM      | 10:19 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 6    | WT   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 15   | WT   | SLOPE | BOS              | 5              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 15   | WT   | SLOPE | 5                | EOS            | Х              | 30              | 30              | 11:13 AM      | 11:18 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 16   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 16   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 30              | 11:16 AM      | 11:21 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 17   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 17   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 30              | 11:19 AM      | 11:24 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 20   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 20   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 30              | 11:22 AM      | 11:27 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 21   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 21   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 30              | 11:28 AM      | 11:33 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 22   | WT   | SLOPE | BOS              | 6              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 22   | WT   | SLOPE | 6                | EOS            | Х              | 30              | 30              | 11:37 AM      | 11:42 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 23   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 23   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 30              | 11:38 AM      | 11:43 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 24   | WT   | SLOPE | BOS              | 3              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | A               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/27/2017 | 24   | WT   | SLOPE | 3                | EOS            | Х              | 30              | 30              | 11:39 AM      | 11:44 AM | Р   |                        |              | KS           | AAW   |          |
| 5/27/2017 | 25   | WT   | SLOPE | BOS              | 5              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/27/2017 | 25   | WT   | SLOPE | 5                | EOS            | Х              | 30              | 29              | 11:40 AM      | 11:45 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 30   | WT   | SLOPE | BOS              | 8              |                | 30              | 30              | 10:23 AM      | 10:28 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 33   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:24 AM      | 10:29 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 35   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:29 AM      | 10:34 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 36   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:30 AM      | 10:35 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 37   | WT   | SLOPE | BOS              | 2              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 37   | WT   | SLOPE | 2                | 14             |                | 30              | 30              | 10:35 AM      | 10:40 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 37   | WT   | SLOPE | 14               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 39   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:36 AM      | 10:41 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 40   | WT   | SLOPE | BOS              | 4              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 40   | WT   | SLOPE | 4                | EOS            | Х              | 30              | 29              | 10:40 AM      | 10:45 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 41   | WT   | SLOPE | BOS              | 2              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 41   | WT   | SLOPE | 2                | EOS            | Х              | 30              | 29              | 10:43 AM      | 10:48 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 42   | WT   | SLOPE | BOS              | 2              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 42   | WT   | SLOPE | 2                | EOS            | Х              | 30              | 30              | 10:47 AM      | 10:52 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 44   | WT   | SLOPE | BOS              | 2              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 44   | WT   | SLOPE | 2                | EOS            | Х              | 30              | 30              | 10:48 AM      | 10:53 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 47   | WT   | SLOPE | BOS              | 3              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 47   | WT   | SLOPE | 3                | EOS            | Х              | 30              | 29              | 10:52 AM      | 10:57 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 48   | WT   | SLOPE | BOS              | 13             |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 48   | WT   | SLOPE | 13               | EOS            | Х              | 30              | 30              | 11:00 AM      | 11:05 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 50   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:01 AM      | 11:06 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 51   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:17 AM      | 11:22 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 52   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:18 AM      | 11:23 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 53   | WT   | SLOPE | BOS              | 11             |                | 30              | 29              | 11:22 AM      | 11:27 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 53   | WT   | SLOPE | 11               | EOS            | Х              | 30              | 29              |               | 11:24 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 54   | WT   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:23 AM      | 11:28 AM | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 54   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:08 PM       |          | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 55   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:08 PM       | 2:13 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 56   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:08 PM       | 2:13 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 57   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:08 PM       | 2:13 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 59   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:08 PM       | 2:13 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 60   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:05 PM       | 2:10 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 61   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:05 PM       | 2:10 PM  | Р   |                        |              | KS           | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/30/2017 | 62   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:05 PM       | 2:10 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 63   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:56 PM       | 2:01 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 64   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:57 PM       | 2:02 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 66   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:57 PM       | 2:02 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 67   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:57 PM       | 2:02 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 71   | PS   | SLOPE | BOS              | 11             |                | 30              | 29              | 1:37 PM       | 1:42 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 71   | PS   | SLOPE | 11               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/30/2017 | 73   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:33 PM       | 1:38 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 74   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:33 PM       | 1:38 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 76   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:33 PM       | 1:38 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 77   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:27 PM       | 1:32 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 78   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:27 PM       | 1:32 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 79   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:27 PM       | 1:32 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 80   | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:27 PM       | 1:32 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/30/2017 | 26   | WT   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |          |
| 5/31/2017 | 81   | 82   | SLOPE | BOS              | 7              |                | 30              | 30              | 11:51 AM      | 11:56 AM | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 81   | 82   | SLOPE | 7                | EOS            | Х              | 30              | 29              | 11:53 AM      | 11:58 AM | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 82   | 83   | SLOPE | BOS              | 28             |                | 30              | 29              | 11:39 AM      | 11:44 AM | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 82   | 83   | SLOPE | 28               | EOS            | Х              | 30              | 29              | 11:47 AM      | 11:52 AM | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 83   | 84   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:31 AM      | 11:36 AM | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 84   | 85   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:30 AM      | 11:35 AM | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 85   | 86   | SLOPE | BOS              | 3              |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/31/2017 | 85   | 86   | SLOPE | 3                | 16             |                | 30              | 30              | 1:03 PM       | 1:08 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 85   | 86   | SLOPE | 16               | 21             |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/31/2017 | 85   | 86   | SLOPE | 21               | 41             |                | 30              | 29              | 1:02 PM       | 1:07 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 85   | 86   | SLOPE | 41               | 56             |                | 30              | 30              | 1:01 PM       | 1:06 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 85   | 86   | SLOPE | 56               | EOS            | Х              | 30              | 30              | 1:09 PM       | 1:14 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 86   | 87   | SLOPE | BOS              | 25             |                | 30              | 29              | 1:18 PM       | 1:23 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 86   | 87   | SLOPE | 75               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 5/31/2017 | 87   | 88   | SLOPE | BOS              | 58             |                | 30              | 30              | 1:25 PM       | 1:30 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 87   | 88   | SLOPE | 58               | 77             |                | 30              | 30              | 1:27 PM       | 1:32 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 87   | 88   | SLOPE | 77               | EOS            | Х              | 30              | 30              | 1:30 PM       | 1:35 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 88   | 89   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:44 PM       | 1:49 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 89   | 90   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:09 PM       | 2:14 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 90   | 91   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:28 PM       | 2:33 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 91   | 92   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:01 PM       | 3:06 PM  | Р   |                        |              | KS           | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | P               | ir Testing    |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 5/31/2017 | 92   | 93   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:12 PM       | 3:17 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 92   | 94   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:25 PM       | 3:30 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 91   | 93   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:11 PM       | 3:16 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 93   | 94   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:32 PM       | 3:37 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 94   | 95   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:09 PM       | 4:14 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 95   | 96   | SLOPE | BOS              | 160            |                | 30              | 30              | 4:36 PM       | 4:41 PM  | Р   |                        |              | KS           | AAW   |          |
| 5/31/2017 | 95   | 96   | SLOPE | 160              | EOS            | Х              | 30              | 30              | 4:50 PM       | 4:55 PM  | Р   |                        |              | KS           | AAW   |          |
| 6/1/2017  | 36   | 96   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 7:50 AM       | 7:55 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 36   | 95   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:51 AM       | 7:56 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 38   | 95   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:52 AM       | 7:57 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 38   | 94   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:58 AM       | 8:03 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 70   | 94   | SLOPE | BOS              | 12             |                | 30              | 30              | 8:06 AM       | 8:11 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 70   | 94   | SLOPE | 12               | 15             |                | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/1/2017  | 70   | 94   | SLOPE | 15               | EOS            | Х              | 30              | 29              | 8:07 AM       | 8:12 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 72   | 94   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:17 AM       | 8:22 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 72   | 93   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:18 AM       | 8:23 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 73   | 93   | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 8:26 AM       | 8:31 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 73   | 91   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:31 AM       | 8:36 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 75   | 90   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:36 AM       | 8:41 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 75   | 89   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:39 AM       | 8:44 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 76   | 89   | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 8:53 AM       | 8:58 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 77   | 87   | SLOPE | BOS              | EOS            | Χ              | 30              | 29              | 8:57 AM       | 9:02 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 78   | 86   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:10 AM       | 9:15 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 78   | 85   | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 9:11 AM       | 9:16 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 78   | 84   | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 9:17 AM       | 9:22 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 79   | 84   | SLOPE | BOS              | EOS            | Χ              | 30              | 29              | 9:20 AM       | 9:25 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 79   | 83   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:24 AM       | 9:29 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 80   | 83   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:29 AM       | 9:34 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 80   | 82   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:36 AM       | 9:41 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 76   | 88   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:54 AM       | 8:59 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 77   | 86   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:58 AM       | 9:03 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 96   | 97   | SLOPE | 11               | 162            |                | 30              | 30              | 1:40 PM       | 1:45 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 96   | 97   | SLOPE | BOS              | 9              |                | 30              | 30              | 2:01 PM       | 2:06 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 98   | 99   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:54 PM       | 1:59 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 97   | 98   | SLOPE | BOS              | 6              |                | 30              | 30              | 2:02 PM       | 2:07 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017  | 97   | 98   | SLOPE | 7                | EOS            | Х              | 30              | 30              | 1:55 PM       | 2:00 PM  | Р   |                        |              | KS           | BJD   |          |



|          |      | Seam |       |                  | Station        |                |                 | P               | ir Testing    |          |     |                        |              |              |       |          |
|----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date     | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/1/2017 | 97   | 99   | SLOPE | BOS              | 22             |                | 30              | 30              | 1:45 PM       | 1:50 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 97   | 99   | SLOPE | 24               | EOS            | Х              | 30              | 30              | 1:41 PM       | 1:46 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 99   | 100  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:17 PM       | 4:22 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 98   | 100  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:21 PM       | 4:26 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 100  | 101  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:20 PM       | 4:25 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 101  | 102  | SLOPE | BOS              | 15             |                | 30              | 29              | 4:26 PM       | 4:31 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 101  | 102  | SLOPE | 27               | EOS            | Х              | 30              | 28              | 4:45 PM       | 4:50 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 101  | 104  | SLOPE | BOS              | 113            |                | 30              | 30              | 4:35 PM       | 4:40 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 101  | 104  | SLOPE | 115              | EOS            | Х              | 30              | 30              | 4:54 PM       | 4:59 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 104  | 105  | SLOPE | BOS              | 92             |                | 30              | 30              | 4:33 PM       | 4:38 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 104  | 105  | SLOPE | 94               | EOS            | х              | 30              | 30              | 4:33 PM       | 4:38 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 102  | 104  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 4:40 PM       | 4:45 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 103  | 105  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:06 PM       | 5:11 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 102  | 103  | SLOPE | BOS              | 33             |                | 30              | 29              | 4:36 PM       | 4:41 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/1/2017 | 102  | 103  | SLOPE | 35               | EOS            | Х              | 30              | 30              | 4:45 PM       | 4:50 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 106  | 108  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 7:58 AM       | 8:03 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 103  | 106  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:12 AM       | 8:17 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 105  | 106  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:09 AM       | 8:14 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 105  | 108  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:50 AM       | 7:55 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 108  | 109  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:46 AM       | 7:51 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 107  | 109  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:47 AM       | 7:52 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 106  | 107  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 7:55 AM       | 8:00 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 23   | 107  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:27 AM       | 8:32 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 24   | 106  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:26 AM       | 8:31 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 27   | 103  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:38 AM       | 8:43 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 31   | 102  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:44 AM       | 8:49 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 32   | 101  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/2/2017 | 29   | 101  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 8:53 AM       | 8:58 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 29   | 100  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:00 AM       | 9:05 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 30   | 100  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:01 AM       | 9:06 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 30   | 99   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:21 AM       | 9:26 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 33   | 99   | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 9:22 AM       | 9:27 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 33   | 97   | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 9:23 AM       | 9:28 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 34   | 97   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:24 AM       | 9:29 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 34   | 96   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:25 AM       | 9:30 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/2/2017 | 82   | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | CC           | BJD   |          |



|          |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date     | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/2/2017 | 81   | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | СС           | BJD   |          |
| 6/5/2017 | 110  | 111  | SLOPE | BOS              | 27             |                | 30              | 30              | 8:51 AM       | 8:56 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 110  | 111  | SLOPE | 28               | 60             |                | 30              | 30              | 8:54 AM       | 8:59 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 110  | 111  | SLOPE | 62               | 72             |                | 30              | 29              | 9:08 AM       | 9:13 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 110  | 111  | SLOPE | 73               | EOS            | Х              | 30              | 30              | 9:17 AM       | 9:22 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 111  | 112  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 8:56 AM       | 9:01 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 112  | 113  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:58 AM       | 9:03 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 113  | 114  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:00 AM       | 9:05 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 114  | 115  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 9:56 AM       | 10:01 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 115  | 116  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:57 AM       | 10:02 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 116  | 118  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:31 AM       | 9:36 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 117  | 118  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:40 AM       | 9:45 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 118  | 119  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:46 AM       | 9:51 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 116  | 117  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:58 AM       | 10:03 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 117  | 119  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:59 AM       | 10:04 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 119  | 120  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:00 AM      | 10:05 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 120  | 121  | SLOPE | 2                | 61             |                | 30              | 30              | 10:32 AM      | 10:37 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 120  | 121  | SLOPE | 61               | EOS            | Х              | 30              | 30              | 10:12 AM      | 10:17 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 121  | 122  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:33 AM      | 10:38 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 124  | 125  | SLOPE | BOS              | 16             |                | 30              | 30              | 10:25 AM      | 10:30 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 124  | 125  | SLOPE | 19               | EOS            | Х              | 30              | 28              | 10:36 AM      | 10:41 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 125  | 126  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:57 AM      | 11:02 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 126  | 127  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:59 AM      | 11:04 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 127  | 129  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:01 AM      | 11:06 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 129  | 130  | SLOPE | BOS              | 15             |                | 30              | 28              | 11:05 AM      | 11:10 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 129  | 130  | SLOPE | 16               | EOS            | Х              | 30              | 29              | 11:11 AM      | 11:16 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 130  | 131  | SLOPE | BOS              | 38             |                | 30              | 30              | 11:14 AM      | 11:19 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 130  | 131  | SLOPE | 39               | EOS            | Х              | 30              | 30              | 11:19 AM      | 11:24 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 131  | 132  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:23 AM      | 11:28 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 132  | 133  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:25 AM      | 11:30 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 133  | 134  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:31 AM      | 11:36 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 132  | 134  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:29 AM      | 11:34 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 134  | 135  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:36 AM      | 11:41 AM | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 110  | 137  | SLOPE | BOS              | 24             |                | 30              | 28              | 3:19 PM       | 3:24 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 110  | 137  | SLOPE | 25               | 38             |                | 30              | 28              | 3:12 PM       |          | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 110  | 137  | SLOPE | 54               | 78             |                | 30              | 29              |               | 3:01 PM  | Р   |                        |              | KS           | BJD   |          |



|          |      | Seam |       |                  | Station        |                |                 | P               | ir Testing    |          |     |                        |              |              |       |          |
|----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date     | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/5/2017 | 110  | 137  | SLOPE | 79               | EOS            | Х              | 30              | 30              | 2:36 PM       | 2:41 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 137  | 138  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:22 PM       | 3:24 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 136  | 137  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:23 PM       | 3:28 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 138  | 139  | SLOPE | BOS              | 16             |                | 30              | 30              | 2:47 PM       | 2:52 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 138  | 139  | SLOPE | 20               | 38             |                | 30              | 30              | 2:41 PM       | 2:46 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 138  | 139  | SLOPE | 39               | EOS            | Х              | 30              | 30              | 2:38 PM       | 2:43 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 139  | 140  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:34 PM       | 3:39 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 140  | 141  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:35 PM       | 3:40 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 141  | 142  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:36 PM       | 3:41 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 136  | 142  | SLOPE | 10               | EOS            | Х              | 30              | 30              | 3:50 PM       | 3:55 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 136  | 141  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 3:46 PM       | 3:51 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 136  | 140  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:45 PM       | 3:50 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 136  | 139  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:44 PM       | 3:49 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/5/2017 | 136  | 138  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:26 PM       | 3:31 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 107  | 143  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:43 PM       | 1:48 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 109  | 143  | SLOPE | BOS              | 52             |                | 30              | 30              | 1:44 PM       | 1:49 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 109  | 143  | SLOPE | 52               | 102            |                | 30              | 28              | 1:51 PM       | 1:56 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 109  | 143  | SLOPE | 102              | EOS            | Х              | 30              | 28              | 1:52 PM       | 1:57 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 143  | 144  | SLOPE | BOS              | 113            |                | 30              | 30              | 2:11 PM       | 2:16 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 143  | 144  | SLOPE | 113              | EOS            | Х              | 30              | 30              | 2:41 PM       | 2:46 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 144  | 145  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:32 PM       | 2:37 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 144  | 146  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:10 PM       | 3:15 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 145  | 146  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:22 PM       | 2:27 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 146  | 147  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:16 PM       | 3:21 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 147  | 148  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:56 PM       | 3:01 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 146  | 148  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:26 PM       | 3:31 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | PE1  | PE2  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:15 PM       | 4:20 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 149  | PE2  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:35 PM       | 4:40 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 148  | 149  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:28 PM       | 3:33 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 149  | 150  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:36 PM       | 3:41 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 150  | PE2  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:32 PM       | 4:37 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 147  | 151  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 4:59 PM       | 5:04 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 151  | PE1  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:24 PM       | 4:29 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 150  | 151  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:44 PM       | 3:49 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 151  | 152  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:28 PM       | 5:33 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 152  | 154  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:31 PM       | 5:36 PM  | Р   |                        |              | KS           | BJD   |          |



|          |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date     | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/6/2017 | 153  | 154  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:00 PM       | 4:05 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 154  | 155  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:35 PM       | 5:40 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 153  | 155  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:50 AM       | 7:55 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 122  | 123  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:34 AM      | 10:39 AM | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 123  | 124  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:35 AM      | 10:40 AM | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 126  | 128  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:50 AM      | 10:55 AM | Р   |                        |              | KS           | BJD   |          |
| 6/6/2017 | 127  | 128  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:49 AM      | 10:54 AM | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 9    | 155  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/7/2017 | 10   | 155  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 8:45 AM       | 8:50 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 10   | 154  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/7/2017 | 11   | 154  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:46 AM       | 8:51 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 11   | 152  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/7/2017 | 13   | 152  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:47 AM       | 8:52 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 14   | 151  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:55 AM       | 9:00 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 15   | 150  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 8:59 AM       | 9:04 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 16   | 149  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:00 AM       | 9:05 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 17   | 148  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:03 AM       | 9:08 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 20   | 146  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 9:05 AM       | 9:10 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 21   | 144  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:08 AM       | 9:13 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 22   | 143  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:11 AM       | 9:16 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 145  | 155  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:01 AM       | 8:06 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 145  | 153  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 7:56 AM       | 8:01 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 146  | 153  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 7:56 AM       | 8:01 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 146  | 152  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 7:55 AM       | 8:00 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 147  | 152  | SLOPE | BOS              | 14             | Х              | 30              | 30              | 8:14 AM       | 8:19 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 147  | 152  | SLOPE | 14               | EOS            | Х              | 30              | 29              | 8:09 AM       | 8:14 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 152  | 153  | SLOPE | BOS              | 22             | Х              | 30              | 30              | 7:46 AM       | 7:51 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 152  | 153  | SLOPE | 22               | EOS            | Х              | 30              | 30              | 7:45 AM       | 7:50 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 155  | 156  | SLOPE | BOS              | 40             |                | 30              | 30              | 2:51 PM       | 2:56 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 155  | 156  | SLOPE | 40               | 65             |                | 30              | 28              | 2:56 PM       | 3:01 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 155  | 156  | SLOPE | 65               | EOS            | Х              | 30              | 30              | 3:13 PM       | 3:18 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 156  | 157  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:09 PM       | 3:14 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 157  | 158  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 2:49 PM       | 2:54 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 157  | 159  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:51 PM       | 3:56 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 156  | 158  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:28 PM       | 3:33 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 158  | 159  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:10 PM       | 4:15 PM  | Р   |                        |              | KS           | BJD   |          |



|          |      | Seam |       |                  | Station        |                |                 | -               | ir Testing    |          |     |                        |              |              |       |          |
|----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date     | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/7/2017 | 159  | 160  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 5:23 PM       | 5:28 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 159  | 161  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 8:01 PM       | 8:06 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 160  | 161  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:38 PM       | 5:43 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 161  | 162  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 7:54 PM       | 7:59 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 160  | 162  | SLOPE | BOS              | 163            |                | 30              | 30              | 5:25 PM       | 5:30 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 160  | 162  | SLOPE | 169              | EOS            | Х              | 30              | 30              | 5:37 PM       | 5:42 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 162  | 163  | SLOPE | BOS              | 55             |                | 30              | 30              | 8:13 PM       | 8:18 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/7/2017 | 162  | 163  | SLOPE | 57               | EOS            | Х              | 30              | 30              | 8:12 PM       | 8:17 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 163  | 164  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:19 PM       | 2:24 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 164  | 165  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:20 PM       | 2:25 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 163  | 165  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:27 PM       | 2:32 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 164  | 166  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:43 PM       | 2:48 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 165  | 166  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:57 PM       | 3:02 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 166  | 167  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:12 PM       | 3:17 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 167  | 168  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:30 PM       | 3:35 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 168  | 169  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:57 PM       | 4:02 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 169  | 170  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:58 PM       | 4:03 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 168  | 170  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 3:59 PM       | 4:04 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 167  | 170  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:17 PM       | 4:22 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 166  | 170  | SLOPE | BOS              | EOS            | Χ              | 30              | 29              | 4:18 PM       | 4:23 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 164  | 170  | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 4:20 PM       | 4:25 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 163  | 170  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:42 PM       | 4:47 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 162  | 170  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:43 PM       | 4:48 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 170  | 171  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:00 PM       | 5:05 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 171  | 172  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:17 PM       | 5:22 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 171  | 173  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:16 PM       | 5:21 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 172  | 173  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 5:22 PM       | 5:27 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 172  | 174  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:49 PM       | 5:54 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 173  | 174  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:36 PM       | 5:41 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 174  | 175  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:37 PM       | 5:42 PM  | P   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 175  | 176  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 5:54 PM       | 5:59 PM  | P   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 176  | 177  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 5:59 PM       | 6:00 PM  | P   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 169  | 178  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 8:21 PM       |          | P   |                        |              | KS           | BJD   |          |
| 6/8/2017 | 170  | 178  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 8:15 PM       |          | P   |                        |              | KS           | BJD   |          |
| 6/9/2017 | 177  | 180  | SLOPE | BOS              | EOS            | X              | 30              | 30              |               | 11:17 AM | P   |                        |              | KS           | BJD   |          |
| 6/9/2017 | 176  | 180  | SLOPE | BOS              | EOS            | Х              | 30              | 28              |               | 11:18 AM | P   |                        |              | KS           | BJD   |          |
| 6/9/2017 | 179  | 180  | SLOPE | BOS              | 10             | .,             | 30              | 28              |               | 11:26 AM | P   |                        |              | KS           | BJD   |          |
| 6/9/2017 | 179  | 180  | SLOPE | 10               | EOS            | Χ              | 30              | 29              | 11:14 AM      | 11:19 AM | Р   |                        |              | KS           | BJD   |          |



|           |      | Seam |       |                  | Station        |                |                 | -               | Air Testing   |          |        |                        |              |              |       |                       |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|--------|------------------------|--------------|--------------|-------|-----------------------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F    | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments              |
| 6/9/2017  | 176  | 179  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:24 AM      | 11:29 AM | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 180  | 181  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:18 AM      | 11:23 AM | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 179  | 181  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:46 AM      | 11:51 AM | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 175  | 179  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:29 AM      | 11:34 AM | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 174  | 179  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:43 AM      | 11:48 AM | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 173  | 179  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:25 PM       | 2:30 PM  | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 171  | 179  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:26 PM       | 2:31 PM  | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 171  | 181  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:39 PM       | 2:44 PM  | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 181  | 184  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:30 PM       | 2:35 PM  | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 181  | 185  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:36 PM       | 2:41 PM  | Р      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 181  | 182  | SLOPE | BOS              | EOS            | Х              | 30              | 30              |               | 11:50 AM | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 182  | 185  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 1:49 PM       |          | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 185  | 186  | SLOPE | BOS              | EOS            | Х              | 30              | 30              |               | 1:46 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 181  | 183  | SLOPE | BOS              | EOS            | X              | 30              | 30              |               | 11:42 AM | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 183  | 186  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:36 PM       | 1:41 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 186  | 187  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 1:37 PM       |          | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 185  | 187  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 1:46 PM       |          | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 187  | 188  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 1:56 PM       | 2:01 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 188  | 189  | SLOPE | BOS              | EOS            | X              | 30              | 29              | 2:04 PM       | 2:09 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 187  | 189  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 2:12 PM       | 2:17 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 185  | 189  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 2:08 PM       | 2:13 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 185  | 190  | SLOPE | BOS              | EOS            | X              | 30              | 29              | 3:02 PM       | 3:07 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 189  | 190  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 3:01 PM       | 3:06 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 190  | 192  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 3:24 PM       | 3:29 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 190  | 191  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 3:11 PM       | 3:16 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 191  | 193  | SLOPE | BOS              | EOS            | X              | 30              | 29              | 4:00 PM       | 4:05 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 191  | 192  | SLOPE | BOS              | EOS            | X              | 30              | 29              | 3:25 PM       | 3:30 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 192  | 193  | SLOPE | BOS              | 26             | ^              | 30              | 30              | 3:34 PM       | 3:39 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 192  | 193  | SLOPE | 26               | EOS            | Х              | 30              | 30              | 3:31 PM       | 3:36 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 193  | 194  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 4:02 PM       | 4:07 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 194  | 195  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 4:01 PM       | 4:06 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 195  | 196  | SLOPE | BOS              | EOS            | X              | 30              | 28              | 4:37 PM       | 4:42 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 195  | 197  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 4:36 PM       | 4:41 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 196  | 197  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 4:57 PM       | 5:02 PM  | P<br>P |                        |              | KS           | BJD   |                       |
| 6/9/2017  | 194  | 196  | SLOPE | BOS              | EOS            | X              | 30              | 29              | 4:56 PM       | 5:01 PM  | P      |                        |              | KS           | BJD   |                       |
| 6/10/2017 | 197  | 198  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 9:42 AM       |          | P      |                        |              | KS           | BJD   |                       |
| 6/10/2017 | 198  | 199  | SLOPE | BOS              | EOS            | X              | 30              | 30              | 9:42 AM       | 9:47 AM  | P      |                        |              | KS           | BJD   |                       |
| 6/10/2017 | 198  | 200  | SLOPE | BOS              | 11             | ^              | 30              | 30              | 9:24 AM       |          | P      |                        |              | KS           | BJD   | 11 FOS: Dino D: No AT |
|           |      |      |       |                  |                | V              |                 |                 |               | 9:30 AM  | P<br>D |                        |              |              | -     | 11-EOS; Pipe B; No AT |
| 6/10/2017 | 199  | 201  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 9:26 AM       | 9:31 AM  | Ч      |                        |              | KS           | BJD   | 1                     |



|           |      | Seam |       |                  | Station        |                |                 | -               | ir Testing    |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/10/2017 | 200  | 201  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:44 AM       | 9:49 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 198  | 200  | SLOPE | BOS              | 51             |                | 30              | 30              | 9:33 AM       | 9:38 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 198  | 200  | SLOPE | 51               | 59             |                | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/10/2017 | 198  | 200  | SLOPE | 59               | EOS            | Х              | 30              | 29              | 9:38 AM       | 9:43 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 201  | 203  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:50 AM       | 9:55 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 202  | 203  | SLOPE | BOS              | 10             |                | 30              | 28              | 9:57 AM       | 10:02 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 202  | 203  | SLOPE | 10               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/10/2017 | 203  | 204  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:26 AM      | 10:31 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 201  | 202  | SLOPE | BOS              | 9              |                | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/10/2017 | 201  | 202  | SLOPE | 9                | EOS            | Х              | 30              | 30              | 9:59 AM       | 10:04 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 202  | 204  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:20 AM      | 10:25 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 198  | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:35 AM      | 10:40 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 200  | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:36 AM      | 10:41 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 201  | PS   | SLOPE | BOS              | 9              |                | 30              | 28              | 10:46 AM      | 10:51 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 201  | PS   | SLOPE | 9                | EOS            | Х              | 30              | 29              | 10:47 AM      | 10:52 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 203  | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:03 AM      | 11:08 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 204  | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 11:04 AM      | 11:09 AM | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 19   | 167  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 1:50 PM       | 1:55 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 1    | 167  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:51 PM       | 1:56 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 1    | 166  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:52 PM       | 1:57 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 2    | 166  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 1:56 PM       | 2:01 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 2    | 165  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:58 PM       | 2:03 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 3    | 165  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:00 PM       | 2:05 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 3    | 163  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 2:03 PM       | 2:08 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 4    | 163  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:06 PM       | 2:11 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 4    | 162  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:08 PM       | 2:13 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 5    | 162  | SLOPE | BOS              | EOS            | Χ              | 30              | 28              | 2:10 PM       | 2:15 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 5    | 161  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/10/2017 | 6    | 161  | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 2:14 PM       | 2:19 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 6    | 159  | SLOPE | BOS              | EOS            | Χ              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/10/2017 | 7    | 159  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:18 PM       | 2:23 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 7    | 158  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 2:20 PM       | 2:25 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 8    | 158  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:24 PM       | 2:29 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 8    | 156  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 2:30 PM       | 2:35 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 9    | 156  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:31 PM       | 2:36 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/10/2017 | 135  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 134  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 133  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 132  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |



|           |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/10/2017 | 131  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 130  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 129  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 127  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 128  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 125  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 124  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 123  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 122  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 121  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 120  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 119  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 117  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 116  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 115  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 114  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 113  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 112  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 111  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 110  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | 137  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | PE1  | 147  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | PE1  | 148  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/10/2017 | PE2  | 148  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | BJD   |          |
| 6/12/2017 | R256 | R257 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:46 PM       | 1:51 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 160  | R257 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 1:47 PM       | 1:52 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 162  | R257 | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |          |
| 6/12/2017 | 170  | R257 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:40 PM       | 1:45 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 170  | R256 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 1:49 PM       | 1:54 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 159  | R251 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 2:59 PM       | 3:04 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 159  | R252 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:09 PM       | 3:14 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 157  | R253 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:15 PM       | 3:20 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 156  | R254 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:21 PM       | 3:26 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 155  | R254 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:27 PM       | 3:32 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 145  | R255 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:33 PM       | 3:38 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R255 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:35 PM       | 3:40 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R254 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:29 PM       | 3:34 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R254 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:23 PM       | 3:28 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R253 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:16 PM       | 3:21 PM  | Р   |                        |              | KS           | BJD   |          |



|           |      | Seam |       |                  | Station        |                |                 | ,               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/12/2017 | R252 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:10 PM       | 3:15 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R251 | PS   | SLOPE | BOS              | 9              |                | 30              | 30              | 2:45 PM       | 2:50 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R251 | PS   | SLOPE | 9                | EOS            | Х              | 30              | 29              | 3:00 PM       | 3:05 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R250 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:42 PM       | 2:47 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R249 | PS   | SLOPE | BOS              | 15             |                | 30              | 30              | 11:26 AM      | 11:31 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R249 | PS   | SLOPE | 15               | EOS            | Х              | 30              | 30              | 11:15 AM      | 11:20 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R248 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 11:14 AM      | 11:19 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R247 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:05 AM      | 11:10 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R246 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:06 AM      | 11:11 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R245 | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:25 AM      | 10:30 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R244 | PS   | SLOPE | BOS              | 16             |                | 30              | 28              | 10:17 AM      | 10:22 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R244 | PS   | SLOPE | 16               | EOS            | Х              | 30              | 30              | 10:09 AM      | 10:14 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 186  | PE3  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:09 PM       | 2:14 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 183  | PE3  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:12 PM       | 2:17 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 181  | PE3  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:05 PM       | 2:10 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 182  | PE3  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:03 PM       | 2:08 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 197  | R244 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:08 AM      | 10:13 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 196  | R244 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:15 AM      | 10:20 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 194  | R244 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:24 AM      | 10:29 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 194  | R245 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:30 AM      | 10:35 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 193  | R245 | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:32 AM      | 10:37 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 191  | R246 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:39 AM      | 10:44 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 191  | R247 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:40 AM      | 10:45 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 190  | R247 | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 10:46 AM      | 10:51 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 185  | R247 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:47 AM      | 10:52 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 184  | R248 | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:54 AM      | 10:59 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 171  | R249 | SLOPE | BOS              | 4              |                | 30              | 30              | 10:57 AM      | 11:02 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 171  | R249 | SLOPE | 4                | EOS            | Х              | 30              | 30              | 10:59 AM      | 11:04 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 171  | R258 | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 11:33 AM      | 11:38 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 181  | R258 | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 11:34 AM      | 11:39 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 184  | R258 | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 10:40 AM      | 10:45 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 170  | R249 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:27 AM      | 11:32 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 170  | R250 | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:43 AM      | 11:48 AM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | R251 | R256 | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:53 PM       | 2:58 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 159  | R256 | SLOPE | BOS              | 8              |                | 30              | 28              | 2:44 PM       | 2:49 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 159  | R256 | SLOPE | 10               | EOS            | Х              | 30              | 30              | 11:55 AM      | 12:00 PM | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 160  | R256 | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:52 PM       | 1:57 PM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 202  | 205  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 9:04 AM       | 9:09 AM  | Р   |                        |              | KS           | BJD   |          |
| 6/12/2017 | 204  | 205  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:08 AM       | 9:13 AM  | Р   |                        |              | KS           | BJD   |          |



|           |      | Seam |       |                  | Station        |                |                 | A               | Air Testing   |          |     |                        |              |              |       |                         |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|-------------------------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments                |
| 6/12/2017 | 205  | 206  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:09 AM       | 9:14 AM  | Р   |                        |              | KS           | BJD   |                         |
| 6/12/2017 | 204  | 206  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:50 AM       | 9:55 AM  | Р   |                        |              | KS           | BJD   |                         |
| 6/12/2017 | 206  | 207  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:52 AM       | 9:57 AM  | Р   |                        |              | KS           | BJD   |                         |
| 6/12/2017 | 207  | 208  | SLOPE | BOS              | 24             |                | 30              | 28              | 9:58 AM       | 10:03 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/12/2017 | 207  | 208  | SLOPE | 24               | EOS            | Х              | 30              | 30              | 9:54 AM       | 9:59 AM  | Р   |                        |              | KS           | BJD   |                         |
| 6/12/2017 | 206  | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:43 PM       | 3:48 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/12/2017 | 207  | PS   | SLOPE | BOS              | 3              |                | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |                         |
| 6/12/2017 | 207  | PS   | SLOPE | 3                | EOS            | Х              | 30              | 30              | 3:45 PM       | 3:50 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/12/2017 | 208  | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:50 PM       | 3:55 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 209  | 210  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:27 AM       | 9:32 AM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 209  | 217  | SLOPE | 4                | EOS            | Х              | 30              | 30              | 11:09 AM      | 11:14 AM | Р   |                        |              | KS           | BJD   | 0-4: Patch: No Air Test |
| 6/13/2017 | 210  | 217  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:18 AM      | 11:23 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 210  | 211  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:11 AM      | 10:16 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 211  | 217  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 11:19 AM      | 11:24 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 211  | 212  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:12 AM      | 10:17 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 212  | 217  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 11:20 AM      | 11:25 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 212  | 215  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:35 AM      | 10:40 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 212  | 213  | SLOPE | BOS              | 5              |                | 30              | 30              | 10:53 AM      | 11:08 AM | Р   |                        |              | KS           | BJD   | Patch: 5-7              |
| 6/13/2017 | 212  | 213  | SLOPE | 7                | EOS            | Х              | 30              | 30              | 11:04 AM      | 11:09 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 213  | 215  | SLOPE | BOS              | 11             |                | 30              | 30              | 10:47 AM      | 10:52 AM | Р   |                        |              | KS           | BJD   | 11-EOS: Pipe Boot       |
| 6/13/2017 | 213  | 214  | SLOPE | 4                | EOS            | Х              | 30              | 30              | 11:06 AM      | 11:11 AM | Р   |                        |              | KS           | BJD   | 0-4: Pipe Boot          |
| 6/13/2017 | 214  | 216  | SLOPE | 7                | EOS            | Х              | 30              | 29              | 10:56 AM      | 11:01 AM | Р   |                        |              | KS           | BJD   | 0-7: Pipe Boot          |
| 6/13/2017 | 215  | 217  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 11:27 AM      | 11:32 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 215  | 216  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:44 AM      | 10:49 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 216  | 217  | SLOPE | BOS              | 10             |                | 30              | 29              | 11:28 AM      | 11:33 AM | Р   |                        |              | KS           | BJD   | Patch: 10               |
| 6/13/2017 | 216  | 217  | SLOPE | 10               | EOS            | Х              | 30              | 28              | 11:31 AM      | 11:36 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 136  | 214  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:35 PM       | 1:40 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 136  | 213  | SLOPE | BOS              | EOS            | Χ              | 30              | 29              | 1:34 PM       | 1:39 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 136  | 212  | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 11:51 AM      | 11:56 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 136  | 211  | SLOPE | BOS              | EOS            | Χ              | 30              | 28              | 11:50 AM      | 11:55 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 136  | 210  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:46 AM      | 11:51 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 136  | 209  | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 11:40 AM      | 11:45 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 137  | 209  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:39 AM      | 11:44 AM | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 217  | 219  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:49 PM       | 1:54 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 218  | 219  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:56 PM       | 2:01 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 219  | 220  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:58 PM       | 2:03 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 217  | 218  | SLOPE | BOS              | 16             |                | 30              | 30              | 1:50 PM       | 1:55 PM  | Р   |                        |              | KS           | BJD   | Patch: 16               |
| 6/13/2017 | 217  | 218  | SLOPE | 16               | EOS            | Х              | 30              | 30              | 1:38 PM       | 1:43 PM  | Р   |                        |              | KS           | BJD   |                         |
| 6/13/2017 | 218  | 220  | SLOPE | BOS              | 73             |                | 30              | 30              | 1:53 PM       | 1:58 PM  | Р   |                        |              | KS           | BJD   | Patch: 73-77            |



|           |      | Seam |       |                  | Station        |                |                 | Δ               | ir Testing    |          |     |                        |              |              |       |                  |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|------------------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments         |
| 6/13/2017 | 218  | 220  | SLOPE | 77               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |                  |
| 6/13/2017 | 220  | 221  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:02 PM       | 2:07 PM  | Р   |                        |              | KS           | BJD   |                  |
| 6/13/2017 | 220  | 222  | SLOPE | BOS              | 10             |                | -               | -               | -             | -        | -   | Х                      |              |              | BJD   |                  |
| 6/13/2017 | 220  | 222  | SLOPE | 10               | EOS            | Х              | 30              | 30              | 2:50 PM       | 2:55 PM  | Р   |                        |              | KS           | BJD   |                  |
| 6/13/2017 | 221  | 222  | SLOPE | 8                | EOS            | Х              | 30              | 30              | 2:46 PM       | 2:51 PM  | Р   |                        |              | KS           | BJD   | BOS-8: Pipe Boot |
| 6/13/2017 | 222  | 223  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:43 PM       | 2:48 PM  | Р   |                        |              | KS           | BJD   | ·                |
| 6/13/2017 | 221  | 223  | SLOPE | BOS              | 21             |                | 30              | 30              | 2:13 PM       | 2:18 PM  | Р   |                        |              | KS           | BJD   | Patch: 21-26     |
| 6/13/2017 | 221  | 223  | SLOPE | 26               | 45             |                | 30              | 30              | 2:37 PM       | 2:42 PM  | Р   |                        |              | KS           | BJD   | Patch: 45-52     |
| 6/13/2017 | 221  | 223  | SLOPE | 52               | EOS            | Х              | 30              | 29              | 2:35 PM       | 2:40 PM  | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 223  | 224  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 8:12 AM       | 8:17 AM  | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 224  | 225  | SLOPE | BOS              | 13             |                | 30              | 30              | 8:13 AM       | 8:18 AM  | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 224  | 225  | SLOPE | 13               | EOS            | Х              | 30              | 30              | 8:34 AM       | 8:39 AM  | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 225  | 226  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:56 AM       | 10:01 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 226  | 222  | SLOPE | BOS              | 64             |                | 30              | 30              | 9:57 AM       | 10:02 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 226  | 227  | SLOPE | 64               | 72             |                | 30              | 28              | 10:05 AM      | 10:10 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 226  | 227  | SLOPE | 72               | EOS            | Х              | 30              | 28              | 10:12 AM      | 10:17 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 227  | 228  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:58 AM       | 10:03 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 228  | 229  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:08 AM      | 10:13 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 229  | 230  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:21 AM      | 10:26 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 230  | 231  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:42 AM      | 10:47 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 231  | 233  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:50 AM      | 10:55 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 232  | 233  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:49 AM      | 10:54 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 231  | 232  | SLOPE | BOS              | 28             |                | 30              | 28              | 10:54 AM      | 10:59 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 231  | 232  | SLOPE | 45               | EOS            | Х              | 30              | 29              | 11:13 AM      | 11:18 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 233  | 234  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 11:23 AM      | 11:28 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 232  | 234  | SLOPE | BOS              | EOS            | Χ              | 30              | 30              | 11:33 AM      | 11:38 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 231  | 232  | SLOPE | 28               | 36             |                | 30              | 30              | 11:07 AM      | 11:12 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/14/2017 | 231  | 232  | SLOPE | 36               | 45             |                | 30              | 29              | 11:08 AM      | 11:13 AM | Р   |                        |              | KS           | BJD   |                  |
| 6/16/2017 | 234  | 235  | SLOPE | BOS              | 55             |                | 30              | 30              | 7:47 AM       | 7:52 AM  | Р   |                        |              | KS           | BJD   |                  |
| 6/16/2017 | 234  | 235  | SLOPE | 55               | EOS            | Χ              | 30              | 29              | 7:56 AM       | 8:01 AM  | Р   |                        |              | KS           | BJD   |                  |
| 6/16/2017 | 101  | 235  | SLOPE | BOS              | EOS            | Χ              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 100  | 234  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 233  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 231  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 230  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 229  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 228  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 227  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |
| 6/16/2017 | 226  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |                  |



|           |      | Seam |       |                  | Station        |                |                 | P               | Air Testing   |          |     |                        |              |              |       |          |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|----------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments |
| 6/16/2017 | 225  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 224  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 223  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 221  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 220  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 219  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 217  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 209  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/16/2017 | 137  | 209  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | BS           | BJD   |          |
| 6/19/2017 | R478 | 100  | SLOPE | BOS              | 76             |                | 30              | 30              | 8:54 AM       | 8:59 AM  | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R478 | 100  | SLOPE | 76               | EOS            | Х              | 30              | 30              | 8:56 AM       | 9:01 AM  | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R478 | 99   | SLOPE | BOS              | 76             |                | 30              | 30              | 9:12 AM       | 9:17 AM  | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R478 | 99   | SLOPE | 76               | EOS            | Х              | 30              | 29              | 9:20 AM       | 9:25 AM  | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R478 | 98   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:26 AM       | 9:31 AM  | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R479 | 93   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:43 AM       | 9:48 AM  | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R479 | 91   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 9:51 AM       | 9:56 AM  | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R480 | 87   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:11 AM      | 10:16 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R480 | 86   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:26 AM      | 10:31 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R481 | 86   | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:34 AM      | 10:39 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | R481 | 85   | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:35 AM      | 10:40 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | 86   | R482 | SLOPE | BOS              | 34             |                | 30              | 28              | 10:47 AM      | 10:52 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | 86   | R482 | SLOPE | 34               | EOS            | Х              | 30              | 30              | 10:50 AM      | 10:55 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | 85   | R482 | SLOPE | BOS              | 10             |                | 30              | 30              | 10:52 AM      | 10:57 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | 85   | R482 | SLOPE | 10               | EOS            | Х              | 30              | 30              | 10:57 AM      | 11:02 AM | Р   |                        |              | KS           | BJV   |          |
| 6/19/2017 | 234  | 236  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:56 PM       | 2:01 PM  | Р   |                        |              | KS           | BJV   |          |
| 6/21/2017 | 235  | 237  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 8:59 AM       | 9:04 AM  | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 237  | 238  | SLOPE | BOS              | 9              |                | 30              | 28              | 9:30 AM       | 9:35 AM  | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 237  | 238  | SLOPE | 9                | EOS            | Χ              | 30              | 30              | 9:28 AM       | 9:33 AM  | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 238  | 239  | SLOPE | BOS              | 41             |                | 30              | 30              | 9:47 AM       | 9:52 AM  | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 236  | 237  | SLOPE | BOS              | 15             |                | 30              | 30              | 11:03 AM      | 11:08 AM | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 236  | 237  | SLOPE | 15               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 6/21/2017 | 239  | 238  | SLOPE | 41               | EOS            |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |          |
| 6/21/2017 | 238  | 240  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 9:55 AM       | 10:00 AM | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 239  | 240  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:20 AM      | 10:25 AM | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 240  | 241  | SLOPE | BOS              | 28             |                | 30              | 30              | 10:16 AM      | 10:21 AM | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 240  | 241  | SLOPE | 28               | EOS            | Х              | 30              | 29              | 10:21 AM      | 10:26 AM | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 239  | 241  | SLOPE | BOS              | 21             |                | 30              | 30              | 10:22 AM      | 10:27 AM | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 239  | 241  | SLOPE | 21               | EOS            | Х              | 30              | 30              | 10:30 AM      | 10:35 AM | Р   |                        |              | KS           | AAW   |          |
| 6/21/2017 | 241  | 242  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:00 AM      | 11:05 AM | Р   |                        |              | KS           | AAW   |          |



|           |      | Seam |       |                  | Station        |                |                 | -               | Air Testing   |          |     |                        |              |              |       |                           |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|---------------------------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments                  |
| 6/21/2017 | 241  | 243  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:11 AM      | 11:16 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 242  | 243  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:34 AM      | 10:39 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 242  | 244  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:29 AM      | 11:34 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 241  | 244  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:31 AM      | 11:36 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 239  | 244  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:33 AM      | 11:38 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 238  | 244  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:34 AM      | 11:39 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 237  | 244  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 1:10 AM       | 1:15 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 235  | 244  | SLOPE | BOS              | 11             |                | 30              | 30              | 1:09 AM       | 1:14 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 235  | 244  | SLOPE | 11               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |                           |
| 6/21/2017 | 244  | 251  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:59 AM       | 3:04 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 242  | 251  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:00 AM       | 3:05 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 250  | 251  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:01 AM       | 3:06 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 242  | 250  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:02 AM       | 3:07 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 249  | 250  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:15 AM       | 3:20 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 242  | 249  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:16 AM       | 3:21 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 248  | 249  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:17 AM       | 3:22 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 242  | 248  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:26 AM       | 3:31 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 243  | 248  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:27 AM       | 3:32 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 248  | 247  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:18 AM       | 3:23 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 243  | 247  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:39 AM       | 3:44 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/21/2017 | 246  | 247  | SLOPE | BOS              | 31             |                | 30              | 30              | 3:37 AM       | 3:42 AM  | Р   |                        |              | KS           | AAW   | 31-36 capped              |
| 6/21/2017 | 246  | 247  | SLOPE | 36               | EOS            | Х              | 30              | 30              | 3:38 AM       | 3:43 AM  | Р   |                        |              | KS           | AAW   | •                         |
| 6/21/2017 | 245  | 246  | SLOPE | 4                | 66             |                | 30              | 30              | 3:40 AM       | 3:45 AM  | Р   |                        |              | KS           | AAW   | Bos-4 capped; 66-71 (eos) |
| 6/21/2017 | 243  | 246  | SLOPE | BOS              | 4              |                | 30              | 28              | 3:57 PM       | 4:02 PM  | Р   |                        |              | KS           | AAW   | 4-9 capped                |
| 6/21/2017 | 243  | 246  | SLOPE | 9                | EOS            | Х              | 30              | 29              | 4:07 PM       | 4:12 PM  | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 245  | 252  | SLOPE | BOS              | 26             |                | 30              | 30              | 9:13 AM       | 9:18 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 245  | 252  | SLOPE | 26               | 32             |                | 30              | 30              | 9:18 AM       | 9:23 AM  | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 245  | 252  | SLOPE | 32               | 54             |                | 30              | 30              | 9:19 AM       | 9:24 AM  | Р   |                        |              | KS           | AAW   | 54-57                     |
| 6/22/2017 | 245  | 252  | SLOPE | 57               | 69             |                | 30              | 30              | 10:41 AM      | 10:46 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 245  | 252  | SLOPE | 69               | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |                           |
| 6/22/2017 | 252  | 253  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:20 AM      | 10:25 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 252  | 254  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:45 AM      | 10:50 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 253  | 254  | SLOPE | BOS              | 6              |                | 30              | 30              | 10:27 AM      | 10:32 AM | Р   |                        |              | KS           | AAW   | 6-8 capped                |
| 6/22/2017 | 253  | 254  | SLOPE | 8                | EOS            | Х              | 30              | 29              | 10:21 AM      | 10:26 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 253  | 255  | SLOPE |                  |                |                | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |                           |
| 6/22/2017 | 254  | 255  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:55 AM      | 11:00 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 255  | 256  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 10:56 AM      | 11:01 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 256  | 257  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 10:57 AM      | 11:02 AM | Р   |                        |              | KS           | AAW   |                           |
| 6/22/2017 | 257  | 258  | SLOPE | BOS              | 14             |                | 30              | 30              | 11:09 AM      | 11:14 AM | Р   |                        |              | KS           | AAW   |                           |



|           |      | Seam |       |                  | Station        |                |                 |                 | ir Testing    |          |     |                        |              |              |       |              |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|--------------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments     |
| 6/22/2017 | 257  | 258  | SLOPE | 14               | EOS            | Х              | 30              | 28              | 11:08 AM      | 11:13 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 258  | 259  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:21 AM      | 11:26 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 259  | 260  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:23 AM      | 11:28 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 260  | 261  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 11:24 AM      | 11:29 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 261  | 262  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:35 AM      | 11:40 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 262  | 263  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 11:36 AM      | 11:41 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 263  | 264  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:38 AM      | 11:43 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 264  | 265  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 11:43 AM      | 11:48 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 265  | 266  | SLOPE | BOS              | 20             |                | 30              | 29              | 11:48 AM      | 11:53 AM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 265  | 266  | SLOPE | 20               | EOS            | Х              | 30              | 28              | 11:58 AM      | 12:03 PM | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 266  | 267  | SLOPE | 3                | EOS            | Х              | 30              | 30              | 1:04 PM       | 1:09 PM  | Р   |                        |              | KS           | AAW   | 0-3 capped   |
| 6/22/2017 | 267  | 268  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:05 PM       | 1:10 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/22/2017 | 268  | 269  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:07 PM       | 1:12 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 281  | PS   | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 1:58 PM       | 2:03 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 208  | 281  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 1:57 PM       | 2:02 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 281  | 282  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:04 PM       | 2:09 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 274  | 282  | SLOPE | BOS              | 28             |                | 30              | 30              | 2:05 PM       | 2:10 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 274  | 282  | SLOPE | 28               | EOS            | Х              | 30              | 29              | 2:08 PM       | 2:13 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 269  | 274  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:22 PM       | 2:27 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 274  | 281  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:25 PM       | 3:30 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 280  | 281  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:01 PM       | 4:06 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 273  | 281  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:17 PM       | 4:22 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 271  | 281  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:16 PM       | 4:21 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 274  | 280  | SLOPE | BOS              | EOS            | Х              | 30              | 28              | 3:40 PM       | 3:45 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 275  | 280  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:38 PM       | 3:43 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 277  | 279  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:57 PM       | 3:02 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 278  | 279  | SLOPE | BOS              | 16             |                | 30              | 30              | 2:37 PM       | 2:42 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 278  | 279  | SLOPE | 16               | EOS            | Х              | 30              | 30              | 2:44 PM       | 2:49 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 276  | 279  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |              |
| 6/23/2017 | 275  | 279  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   | Х                      |              |              | AAW   |              |
| 6/23/2017 | 274  | 275  | SLOPE | BOS              | 39             |                | 30              | 30              | 3:39 PM       | 3:44 PM  | Р   |                        |              | KS           | AAW   | 39-46 capped |
| 6/23/2017 | 274  | 275  | SLOPE | 46               | EOS            | Х              | 30              | 28              | 2:23 PM       | 2:28 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 275  | 277  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:59 PM       | 3:04 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 275  | 276  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:24 PM       | 2:29 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 276  | 277  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:45 PM       | 2:50 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 276  | 278  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 2:25 PM       | 2:30 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 279  | 280  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:23 PM       | 3:28 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 272  | 279  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:48 PM       | 2:53 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 272  | 280  | SLOPE | BOS              | EOS            | Х              | 30              | 29              | 3:42 PM       | 3:47 PM  | Р   |                        |              | KS           | AAW   |              |



|           |      | Seam |       |                  | Station        |                |                 |                 | Air Testing   |          |     |                        |              |              |       |              |
|-----------|------|------|-------|------------------|----------------|----------------|-----------------|-----------------|---------------|----------|-----|------------------------|--------------|--------------|-------|--------------|
| Date      | From | То   | Loc   | Station<br>Start | Station<br>End | End of<br>Seam | Beg<br>Pressure | End<br>Pressure | Start<br>Time | End Time | P/F | Capped, No Air<br>Test | V-box<br>P/F | Test<br>Tech | QA ID | Comments     |
| 6/23/2017 | 272  | 273  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:50 PM       | 3:55 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 273  | 280  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:59 PM       | 4:04 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 271  | 273  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:58 PM       | 4:03 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 270  | 271  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:18 PM       | 4:23 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 270  | 273  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 4:19 PM       | 4:24 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 270  | 272  | SLOPE | BOS              | 28             |                | 30              | 30              | 3:56 PM       | 4:01 PM  | Р   |                        |              | KS           | AAW   | 28-30 capped |
| 6/23/2017 | 270  | 272  | SLOPE | 30               | EOS            | Х              | 30              | 28              | 2:50 PM       | 2:55 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 283  | 284  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:20 PM       | 3:25 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 270  | 283  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 2:54 PM       | 2:59 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 284  | 285  | SLOPE | BOS              | EOS            | Х              | 30              | 30              | 3:21 PM       | 3:26 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/23/2017 | 283  | 285  | SLOPE | BOS              | 27             |                | 30              | 30              | 3:12 PM       | 3:17 PM  | Р   |                        |              | KS           | AAW   | 27-28 capped |
| 6/23/2017 | 283  | 285  | SLOPE | 28               | EOS            | Х              | 30              | 29              | 3:13 PM       | 3:18 PM  | Р   |                        |              | KS           | AAW   |              |
| 6/24/2017 | 235  | 236  | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 250  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 249  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |
| 6/24/2017 | 248  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 247  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 246  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 244  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 252  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 253  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 255  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |
| 6/24/2017 | 256  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 257  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 258  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 259  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |
| 6/24/2017 | 260  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 261  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 262  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |
| 6/24/2017 | 263  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 264  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 265  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |
| 6/24/2017 | 266  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |
| 6/24/2017 | 267  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/24/2017 | 268  | PS   | SLOPE | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | WE           | AAW   |              |
| 6/26/2017 | 269  | PS   | Slope | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |
| 6/26/2017 | 282  | PS   | Slope | BOS              | EOS            | Х              | -               | -               | -             | -        | -   |                        | Р            | PP           | AAW   |              |



#### Sub-Appendix C.7

#### **Destructive Sampling**

#### Sub-Appendix C.7.1

#### **Destructive Sample Log**

| Destruct<br>Number | From | То | Technician | Machine | Station | Field Test<br>Date | Field P/F | Lab P/F | QA ID | Reason / Comments |
|--------------------|------|----|------------|---------|---------|--------------------|-----------|---------|-------|-------------------|
| 1                  | 3    | 4  | KS         | 45      | 73      | 5/17/2017          | Р         | Р       | AAW   |                   |
| 2                  | 5    | 6  | MAY        | 2650    | 93      | 5/17/2017          | Р         | Р       | AAW   |                   |
| 3                  | 13   | 14 | MAY        | 2650    | 77      | 5/18/2017          | Р         | Р       | AAW   |                   |
| 4                  | 14   | 15 | KS         | 45      | 107     | 5/18/2017          | Р         | Р       | AAW   |                   |
| 5                  | 24   | 25 | KS         | 45      | 70      | 5/18/2017          | Р         | Р       | AAW   |                   |
| 6                  | 23   | 24 | MAY        | 2650    | 97      | 5/18/2017          | Р         | Р       | AAW   |                   |
| 7                  | 27   | 28 | KS         | 45      | 44      | 5/22/2017          | Р         | Р       | AAW   |                   |
| 8                  | 34   | 36 | MAY        | 2650    | 2       | 5/22/2017          | Р         | Р       | AAW   |                   |
| 9                  | 40   | 41 | MAY        | 2650    | 107     | 5/24/2017          | Р         | Р       | AAW   |                   |
| 10                 | 47   | 48 | KS         | 45      | 53      | 5/24/2017          | Р         | Р       | AAW   |                   |
| 11                 | 50   | 51 | KS         | 45      | 9       | 5/24/2017          | Р         | Р       | AAW   |                   |
| 12                 | 48   | 49 | MAY        | 2650    | 2       | 5/24/2017          | Р         | Р       | AAW   |                   |
| 13                 | 61   | 62 | MAY        | 2650    | 70      | 5/29/2017          | Р         | Р       | AAW   |                   |
| 14                 | 62   | 63 | KS         | 45      | 2       | 5/29/2017          | Р         | Р       | AAW   |                   |
| 15                 | 71   | 72 | MAY        | 2650    | 16      | 5/29/2017          | Р         | Р       | AAW   |                   |
| 16                 | 71   | 73 | KS         | 45      | 108     | 5/29/2017          | Р         | Р       | AAW   |                   |
| 17                 | 10   | WT | MAY        | 2650    | 15      | 5/31/2017          | Р         | F       | AAW   |                   |
| 17A                | 9    | WT | MAY        | 2650    | 9       | 6/2/2017           | Р         | F       | BJD   |                   |
| 17A2               | 11   | WT | MAY        | 2650    | 11      | 6/8/2017           | Р         | Р       | BJD   |                   |
| 17B                | 10   | WT | MAY        | 2650    | 5       | 6/2/2017           | Р         | F       | BJD   |                   |
| 17B2               | 8    | WT | MAY        | 2650    | 3       | 6/8/2017           | Р         | Р       | BJD   |                   |
| 18                 | 52   | WT | MAY        | 2650    | 26      | 5/31/2017          | Р         | Р       | AAW   |                   |
| 19                 | 84   | 85 | KS         | 45      | 4       | 5/31/2017          | Р         | F       | AAW   |                   |
| 19A                | 84   | 85 | KS         | 45      | 14      | 6/2/2017           | Р         | F       | BJD   |                   |
| 19A2               | 84   | 85 | Ks         | 45      | 24      | 6/8/2017           | Р         | Р       | BJD   |                   |
| 19B                | 83   | 84 | KS         | 45      | 41      | 6/2/2017           | Р         | F       | BJD   |                   |
| 19B2               | 83   | 84 | KS         | 45      | 31      | 6/8/2017           | Р         | Р       | BJD   |                   |
| 20                 | 86   | 87 | MAY        | 25      | 67      | 5/31/2017          | Р         | F       | AAW   |                   |



| Destruct<br>Number | From | То  | Technician | Machine | Station | Field Test<br>Date | Field P/F | Lab P/F | QA ID | Reason / Comments |
|--------------------|------|-----|------------|---------|---------|--------------------|-----------|---------|-------|-------------------|
| 20A                | 86   | 87  | MAY        | 25      | 77      | 6/2/2017           | Р         | F       | BJD   |                   |
| 20A2               | 99   | 100 | MAY        | 25      | 12      | 6/8/2017           | Р         | F       | BJD   |                   |
| 20A3               | 99   | 100 | MAY        | 25      | 22      | 6/12/2017          | Р         | F       | BJD   |                   |
| 20A4               | 99   | 100 | MAY        | 25      | 32      | 6/14/2017          | Р         | F       | BJD   |                   |
| 20A5               | 99   | 100 | MAY        | 25      | 75      | 6/16/2017          | F         | -       | BJV   |                   |
| 20A6               | 98   | 100 | MAY        | 25      | 4       | 6/16/2017          | Р         | F       | BJV   |                   |
| 20A7               | 98   | 100 | MAY        | 25      | 14      | 6/20/2017          | Р         | Р       | BJV   |                   |
| 20B                | 86   | 87  | MAY        | 25      | 57      | 6/2/2017           | Р         | F       | BJD   |                   |
| 20B2               | 86   | 87  | MAY        | 25      | 47      | 6/8/2017           | Р         | F       | BJD   |                   |
| 20B3               | 86   | 87  | MAY        | 25      | 37      | 6/12/2017          | Р         | F       | BJD   |                   |
| 20B4               | 86   | 87  | MAY        | 25      | 27      | 6/14/2017          | Р         | F       | BJD   |                   |
| 20B5               | 86   | 87  | MAY        | 25      | 3       | 6/16/2017          | F         | -       | BJV   |                   |
| 20B6               | 85   | 86  | MAY        | 25      | 50      | 6/16/2017          | F         | -       | BJV   |                   |
| 20B7               | 85   | 86  | MAY        | 25      | 30      | 6/16/2017          | F         | -       | BJV   |                   |
| 21                 | 92   | 94  | MAY        | 45      | 3       | 5/31/2017          | Р         | F       | AAW   |                   |
| 21A                | 92   | 94  | MAY        | 45      | 13      | 6/2/2017           | Р         | F       | BJD   |                   |
| 21A2               | 92   | 94  | MAY        | 45      | 23      | 6/8/2017           | Р         | Р       | BJD   |                   |
| 21B                | 91   | 93  | MAY        | 45      | 42      | 6/2/2017           | Р         | F       | BJD   |                   |
| 21B2               | 91   | 93  | MAY        | 45      | 32      | 6/8/2017           | Р         | F       | BJD   |                   |
| 21B3               | 91   | 93  | MAY        | 45      | 22      | 6/12/2017          | Р         | F       | BJD   |                   |
| 21B4               | 91   | 93  | MAY        | 45      | 12      | 6/14/2017          | Р         | Р       | BJD   |                   |
| 22                 | 95   | 96  | MAY        | 45      | 172     | 5/31/2017          | Р         | Р       | AAW   |                   |
| 23                 | 100  | 101 | KS         | 45      | 7       | 6/2/2017           | Р         | F       | BJD   |                   |
| 23A                | 100  | 101 | KS         | 45      | 17      | 6/8/2017           | Р         | Р       | BJD   |                   |
| 23B                | 97   | 99  | KS         | 45      | 123     | 6/8/2017           | Р         | Р       | BJD   |                   |
| 24                 | 105  | 108 | MAY        | 25      | 56      | 6/2/2017           | Р         | Р       | BJD   |                   |
| 25                 | 107  | 109 | KS         | 45      | 8       | 6/2/2017           | Р         | Р       | BJD   |                   |
| 26                 | 121  | 122 | KS         | 45      | 22      | 6/6/2017           | Р         | Р       | BJD   |                   |



| Destruct<br>Number | From | То  | Technician | Machine | Station | Field Test<br>Date | Field P/F | Lab P/F | QA ID | Reason / Comments            |
|--------------------|------|-----|------------|---------|---------|--------------------|-----------|---------|-------|------------------------------|
| 27                 | 127  | 128 | CC         | 25      | 2       | 6/6/2017           | Р         | Р       | BJD   |                              |
| 28                 | 144  | 146 | KS         | 45      | 97      | 6/8/2017           | Р         | Р       | BJD   |                              |
| 29                 | 152  | 153 | SP         | 25      | 56      | 6/8/2017           | Р         | Р       | BJD   |                              |
| 30                 | 22   | 143 | KS         | 45      | 14      | 6/8/2017           | Р         | Р       | BJD   |                              |
| 31                 | 155  | 156 | SP         | 25      | 147     | 6/8/2017           | Р         | Р       | BJD   |                              |
| 32                 | 158  | 159 | SP         | 25      | 99      | 6/8/2017           | Р         | Р       | BJD   |                              |
| 33                 | 167  | 168 | AG         | 2650    | 4       | 6/11/2017          | Р         | Р       | BJD   |                              |
| 34                 | 170  | 171 | AG         | 2650    | 121     | 6/11/2017          | Р         | Р       | BJD   |                              |
| 35                 | 173  | 179 | AG         | 2650    | 15      | 6/12/2017          | Р         | Р       | BJD   |                              |
| 36                 | 186  | 187 | AG         | 2650    | 4       | 6/12/2017          | Р         | Р       | BJD   | TRIMMED OFF IN ANCHOR TRENCH |
| 37                 | 192  | 193 | AG         | 2650    | 18      | 6/12/2017          | Р         | Р       | BJD   |                              |
| 38                 | 179  | 181 | SP         | 2479    | 131     | 6/12/2017          | Р         | Р       | BJD   |                              |
| 39                 | 190  | 191 | SP         | 2479    | 42      | 6/12/2017          | Р         | Р       | BJD   |                              |
| 40                 | 131  | PS  | AG         | 83      | 12      | 6/12/2017          | Р         | Р       | BJD   |                              |
| 41                 | 138  | 139 | CC         | 25      | 43      | 6/12/2017          | Р         | Р       | BJD   |                              |
| 42                 | 197  | 198 | SP         | 2479    | 67      | 6/12/2017          | Р         | Р       | BJD   |                              |
| 43                 | 203  | 204 | SP         | 2479    | 7       | 6/12/2017          | Р         | Р       | BJD   |                              |
| 44                 | 198  | 200 | AG         | 2650    | 42      | 6/12/2017          | Р         | Р       | BJD   |                              |
| 45                 | R247 | PS  | CC         | 45      | 9       | 6/14/2017          | Р         | Р       | BJD   |                              |
| 46                 | 27   | 103 | MAY        | 25      | 13      | 6/14/2017          | Р         | Р       | BJD   |                              |
| 47                 | 88   | PS  | MAY        | 60      | 13      | 6/14/2017          | Р         | F       | BJD   |                              |
| 47B                | 87   | PS  | MAY        | 60      | 14      | 6/16/2017          | Р         | Р       | BJV   |                              |
| 48                 | 211  | 212 | SP         | 45      | 13      | 6/14/2017          | Р         | Р       | BJD   |                              |
| 49                 | 80   | 82  | MAY        | 45      | 9       | 6/14/2017          | Р         | Р       | BJD   |                              |
| 50                 | 223  | 224 | SP         | 45      | 47      | 6/16/2017          | Р         | Р       | BJD   |                              |
| 51                 | 228  | 229 | CC         | 45      | 29      | 6/16/2017          | Р         | Р       | BJD   |                              |
| 52                 | 98   | PS  | AG         | 211     | 5       | 6/16/2017          | Р         | F       | BJV   |                              |
| 52B                | 97   | PS  | AG         | 211     | 15      | 6/20/2017          | Р         | Р       | BJV   |                              |
| 53                 | 159  | 160 | SP         | 25      | 213     | 6/16/2017          | Р         | Р       | BJV   |                              |



| Destruct<br>Number | From | То     | Technician | Machine | Station | Field Test<br>Date | Field P/F | Lab P/F | QA ID | Reason / Comments |
|--------------------|------|--------|------------|---------|---------|--------------------|-----------|---------|-------|-------------------|
| 54                 | 198  | 200    | AG         | 2650    | 126     | 6/16/2017          | Р         | Р       | BJV   |                   |
| 55                 | 204  | PS     | SP         | 2479    | 12      | 6/16/2017          | Р         | F       | BJV   |                   |
| 55B                | 203  | PS     | SP         | 2479    | 14      | 6/20/2017          | Р         | Р       | BJV   |                   |
| 56                 | 207  | 208    | SP         | 2650    | 105     | 6/16/2017          | Р         | Р       | BJV   |                   |
| 57                 | 220  | 222    | CC         | 2650    | 18      | 6/16/2017          | Р         | F       | BJV   |                   |
| 57B                | 220  | 221    | CC         | 2650    | 104     | 6/20/2017          | Р         | Р       | BJV   |                   |
| 58                 | 91   | R479   | SP         | 45      | 21      | 6/20/2017          | Р         | Р       | BJV   |                   |
| 59                 | 239  | 241    | CC         | 45      | 6       | 6/22/2017          | Р         | Р       | AAW   |                   |
| 60                 | 235  | 237    | SP         | 1406    | 50      | 6/22/2017          | Р         | Р       | AAW   |                   |
| 61                 | 249  | 250    | SP         | 45      | 14      | 6/22/2017          | Р         | F       | AAW   |                   |
| 61A                | 249  | 250    | SP         | 45      | 24      | 6/25/2017          | Р         | Р       | AAW   |                   |
| 61B                | 249  | 250    | SP         | 45      | 4       | 6/25/2017          | Р         | Р       | AAW   |                   |
| 62                 | 255  | 256    | SP         | 45      | 13      | 6/22/2017          | Р         | Р       | AAW   |                   |
| 63                 | 271  | 273    | SP         | 45      | 21      | 6/25/2017          | Р         | Р       | AAW   |                   |
| 64                 | 281  | 282    | SP         | 45      | 14      | 6/25/2017          | Р         | Р       | AAW   |                   |
| 65                 | 237  | 244    | CC         | 45      | 10      | 6/25/2017          | Р         | Р       | AAW   |                   |
| 66                 | 283  | 285    | SP         | 45      | 18      | 6/25/2017          | Р         | Р       | AAW   |                   |
| 67                 | 249  | PS     | AG         | 112     | 4       | 6/26/2017          | Р         | F       | AAW   |                   |
| 67A                | 249  | PS     | AG         | 112     | 14      | 6/27/2017          | Р         | F       | BJV   |                   |
| 67B                | 250  | PS     | AG         | 112     | 10      | 6/27/2017          | Р         | Р       | BJV   |                   |
| 68                 | 248  | PS     | WL         | 15      | 10      | 6/26/2017          | Р         | Р       | AAW   |                   |
| 69                 | 135  | Tie-in | AG         | 211     | 5       | 6/27/2017          | Р         | Р       | BJV   |                   |



#### Sub-Appendix C.7.2

#### **Destructive Sample Laboratory Testing Results**

Date: 2017-05-18

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:aweber@feezorengineering.com

Dear Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 28948

Material(s) Tested: (2) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge. SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,



Patricia Zabaleta Project Manager Geosynthetic Services Division http://www.geosyntheticstestinc.com

# DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS TRI Client: Feezor Engineering. Inc. Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 28948

#### **TEST REPLICATE NUMBER**

|   |           | IESI       | REPLICATE N | UMBEK |     |              |  |
|---|-----------|------------|-------------|-------|-----|--------------|--|
| PARAMETER   | 1         | 2          | 3           | 4     | 5   | MEAN         |  |
| Sample ID: DS-1   Weld: Heat Fusion   |           |            |             |       |     |              |  |
| Side: A   |           |            |             |       |     | Peel A       |  |
| Peel Strength (ppi)   | 122       | 117        | 123         | 121   | 129 | 122          |  |
| Peel Incursion (%)  | <5        | <5         | <5          | <5    | <5  |              |  |
| Peel Locus Of Failure Code  | SE        | SE         | SE          | SE    | SIP |              |  |
| Peel NSF Failure Code   | FTB       | FTB        | FTB         | FTB   | FTB |              |  |
| Side: B   |           |            |             |       |     | Peel B       |  |
| Peel Strength (ppi)   | 117       | 126        | 121         | 122   | 120 | 121          |  |
| Peel Incursion (%)  | <5        | <5         | <5          | <5    | <5  |              |  |
| Peel Locus Of Failure Code  | SE        | SE         | SE          | SE    | SE  |              |  |
| Peel NSF Failure Code   | FTB       | FTB        | FTB         | FTB   | FTB |              |  |
| Shear   |           |            |             |       |     | Shear        |  |
| Shear Strength (ppi)  | 150       | 154        | 152         | 152   | 153 | 152          |  |
| Shear Elongation @ Break (%)  | >50       | >50        | >50         | >50   | >50 |              |  |
| Sample ID: DS-2   Weld: Heat Fusion   |           |            |             |       |     |              |  |
| Side: A   |           |            |             |       |     | Peel A       |  |
| Peel Strength (ppi)   | 123       | 124        | 107         | 120   | 118 | 118          |  |
| Peel Incursion (%)  | <5        | <5         | <5          | <5    | <5  |              |  |
| Peel Locus Of Failure Code  | SE        | SE         | SIP         | SE    | SE  |              |  |
| Peel NSF Failure Code   | FTB       | FTB        | FTB         | FTB   | FTB |              |  |
| Side: B   |           |            |             |       |     | Peel B       |  |
| Peel Strength (ppi)   | 98        | 118        | 120         | 86    | 119 | 108          |  |
| Peel Incursion (%)  | <5        | <5         | <5          | <5    | <5  | L            |  |
|   |           |            |             | SIP   | SIP |              |  |
| , ,   | SE        | SIP        | SIP         | SIP   | SIF |              |  |
| Peel Locus Of Failure Code  | SE<br>FTB | SIP<br>FTB | SIP<br>FTB  | FTB   | FTB |              |  |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code                         |           |            |             |       |     | Shear        |  |
| Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) |           |            |             |       |     | Shear<br>152 |  |

The testing herein is based upon accepted industry practice as well as the test method listed. Test results reported herein do not apply to samples other than those tested. TRI neither accepts responsibility for nor makes claim as to the final use and purpose of the material. TRI observes and maintains client confidentiality. TRI limits reproduction of this report, except in full, without prior approval of TRI.

Date: 2017-05-19

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 28973

Material(s) Tested: (4) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,



Patricia Zabaleta Project Manager Geosynthetic Services Division http://www.geosyntheticstestinc.com

# DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS TRI Client: Feezor Engineering. Inc. Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 28973

#### **TEST REPLICATE NUMBER**

|                                     |     | 1631 | REPLICATE N | UMBEK |     |          |
|-------------------------------------|-----|------|-------------|-------|-----|----------|
| PARAMETER                           | 1   | 2    | 3           | 4     | 5   | MEAN     |
| Sample ID: DS-3   Weld: Heat Fusion |     |      |             |       |     |          |
| Side: A                             |     |      |             |       |     | Peel A   |
| Peel Strength (ppi)                 | 112 | 126  | 119         | 127   | 126 | 122      |
| Peel Incursion (%)                  | <5  | <5   | <5          | <5    | <5  | <u>'</u> |
| Peel Locus Of Failure Code          | SIP | SIP  | SIP         | SIP   | SIP |          |
| Peel NSF Failure Code               | FTB | FTB  | FTB         | FTB   | FTB |          |
| Side: B                             |     |      |             |       |     | Peel B   |
| Peel Strength (ppi)                 | 116 | 113  | 116         | 118   | 113 | 115      |
| Peel Incursion (%)                  | <5  | <5   | <5          | <5    | <5  |          |
| Peel Locus Of Failure Code          | SE  | SE   | SE          | SE    | SE  |          |
| Peel NSF Failure Code               | FTB | FTB  | FTB         | FTB   | FTB |          |
| Shear                               |     |      |             |       |     | Shear    |
| Shear Strength (ppi)                | 148 | 149  | 147         | 148   | 148 | 148      |
| Shear Elongation @ Break (%)        | >50 | >50  | >50         | >50   | >50 |          |
|                                     |     |      |             |       |     |          |
| Sample ID: DS-4   Weld: Heat Fusion |     |      |             |       |     |          |
| Side: A                             |     |      |             |       |     | Peel A   |
| Peel Strength (ppi)                 | 126 | 122  | 123         | 119   | 123 | 123      |
| Peel Incursion (%)                  | <5  | <5   | <5          | <5    | <5  |          |
| Peel Locus Of Failure Code          | SIP | SIP  | SIP         | SIP   | SIP |          |
| Peel NSF Failure Code               | FTB | FTB  | FTB         | FTB   | FTB |          |
| Side: B                             |     |      |             |       |     | Peel B   |
| Peel Strength (ppi)                 | 121 | 119  | 114         | 126   | 122 | 120      |
| Peel Incursion (%)                  | <5  | <5   | <5          | <5    | <5  | •        |
| Peel Locus Of Failure Code          | SE  | SE   | SE          | SE    | SE  |          |
| Peel NSF Failure Code               | FTB | FTB  | FTB         | FTB   | FTB |          |
| Shear                               |     |      |             |       |     | Shear    |
| Shear Strength (ppi)                | 153 | 151  | 151         | 150   | 151 | 151      |
|                                     |     |      |             |       |     |          |

The testing herein is based upon accepted industry practice as well as the test method listed. Test results reported herein do not apply to samples other than those tested. TRI neither accepts responsibility for nor makes claim as to the final use and purpose of the material. TRI observes and maintains client confidentiality. TRI limits reproduction of this report, except in full, without prior approval of TRI.

# DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS TRI Client: Feezor Engineering. Inc. Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 28973

#### **TEST REPLICATE NUMBER**

| PARAMETER  | 1                                    | 2                                    | 3                                    | 4                                    | 5                                   | MEAN   |
|--|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|-------------------------------------|--------|
| Sample ID: DS-5   Weld: Heat Fusion  |                                      |                                      |                                      |                                      |                                     |        |
| Side: A  |                                      |                                      |                                      |                                      |                                     | Peel A |
| Peel Strength (ppi)  | 117                                  | 124                                  | 126                                  | 127                                  | 128                                 | 124    |
| Peel Incursion (%)   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                  |        |
| Peel Locus Of Failure Code   | SIP                                  | SE                                   | SE                                   | SIP                                  | SE                                  |        |
| Peel NSF Failure Code  | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                 |        |
| Side: B  |                                      |                                      |                                      |                                      |                                     | Peel B |
| Peel Strength (ppi)  | 116                                  | 116                                  | 116                                  | 115                                  | 119                                 | 116    |
| Peel Incursion (%)   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                  |        |
| Peel Locus Of Failure Code   | SE                                   | SE                                   | SE                                   | SE                                   | SE                                  |        |
| Peel NSF Failure Code  | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                 |        |
| Shear  |                                      |                                      |                                      |                                      |                                     | Shear  |
| Shear Strength (ppi)   | 149                                  | 151                                  | 149                                  | 148                                  | 150                                 | 149    |
| Shear Elongation @ Break (%)   | >50                                  | >50                                  | >50                                  | >50                                  | >50                                 |        |
| Sample ID: DS-6   Weld: Heat Fusion  |                                      |                                      |                                      |                                      |                                     |        |
| Side: A  |                                      |                                      |                                      |                                      |                                     | Peel A |
| Peel Strength (ppi)  | 132                                  |                                      |                                      |                                      |                                     |        |
|  |                                      | 129                                  | 133                                  | 132                                  | 120                                 | 129    |
| Peel Incursion (%)   |                                      | 129<br><5                            | 133<br><5                            | 132<br><5                            | 120<br><5                           | 129    |
| , ,  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                  | 129    |
| Peel Locus Of Failure Code   | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SE                            | 129    |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                  | 129    |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B   | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SE                            |        |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code<br><b>Side: B</b><br>Peel Strength (ppi)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SE<br>FTB                     | Peel B |
| Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB<br>116<br><5        | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB<br>121<br><5        | <5<br>SE<br>FTB                     | Peel B |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code   | <5<br>SIP<br>FTB<br>119<br><5        | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB<br>116<br><5        | <5<br>SIP<br>FTB                     | <5<br>SE<br>FTB<br>119<br><5        | Peel B |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code   | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | <5<br>SIP<br>FTB<br>116<br><5<br>SIP | <5<br>SIP<br>FTB<br>116<br><5<br>SIP | <5<br>SIP<br>FTB<br>121<br><5<br>SIP | <5<br>SE<br>FTB<br>119<br><5<br>SIP | Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | <5<br>SIP<br>FTB<br>116<br><5<br>SIP | <5<br>SIP<br>FTB<br>116<br><5<br>SIP | <5<br>SIP<br>FTB<br>121<br><5<br>SIP | <5<br>SE<br>FTB<br>119<br><5<br>SIP | Peel B |

The testing herein is based upon accepted industry practice as well as the test method listed. Test results reported herein do not apply to samples other than those tested. TRI neither accepts responsibility for nor makes claim as to the final use and purpose of the material. TRI observes and maintains client confidentiality. TRI limits reproduction of this report, except in full, without prior approval of TRI.

Date: 2017-05-23

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29049

Material(s) Tested: (2) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

# DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS TRI Client: Feezor Engineering. Inc. Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29049

#### **TEST REPLICATE NUMBER**

| PARAMETER  | 1   | 2   | 3   | 4   | 5  | MEAN       |
|--|---|---|---|---|--|------------|
| Sample ID: DS-7   Weld: Heat Fusion  |   |   |   |   |  |            |
| Side: A  |   |   |   |   |  | Peel A     |
| Peel Strength (ppi)  | 121   | 122   | 127   | 124   | 127  | 124        |
| Peel Incursion (%)   | <5  | <5  | <5  | <5  | <5   |            |
| Peel Locus Of Failure Code   | SE  | SE  | SE  | SE  | SE   |            |
| Peel NSF Failure Code  | FTB   | FTB   | FTB   | FTB   | FTB  |            |
| Side: B  |   |   |   |   |  | Peel B     |
| Peel Strength (ppi)  | 121   | 125   | 114   | 125   | 123  | 122        |
| Peel Incursion (%)   | <5  | <5  | <5  | <5  | <5   |            |
| Peel Locus Of Failure Code   | SIP   | SIP   | SIP   | SE  | SIP  |            |
| Peel NSF Failure Code  | FTB   | FTB   | FTB   | FTB   | FTB  |            |
| Shear  |   |   |   |   |  | Shear      |
| Shear Strength (ppi)   | 158   | 162   | 159   | 160   | 161  | 160        |
|  |   |   |   |   | . 50                                       |            |
| Shear Elongation @ Break (%)   | >50   | >50   | >50   | >50   | >50  |            |
| Sample ID: DS-8   Weld: Heat Fusion  | >50   | >50   | >50   | >50   | >50  | Peel A     |
| Sample ID: DS-8   Weld: Heat Fusion Side: A  | >50   | >50   | >50   | 118   | 122  | Peel A     |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi)  |   |   |   |   |  |            |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%)   | 121   | 116   | 126   | 118   | 122  |            |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | 121<br><5                                   | 116<br><5                                   | 126<br><5                                   | 118 <5                                      | 122  |            |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  | 121<br><5<br>SIP                            | 116<br><5<br>SIP                            | 126<br><5<br>SIP                            | 118<br><5<br>SIP                            | 122<br><5<br>SIP                           |            |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | 121<br><5<br>SIP                            | 116<br><5<br>SIP                            | 126<br><5<br>SIP                            | 118<br><5<br>SIP                            | 122<br><5<br>SIP                           | 121        |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | 121<br><5<br>SIP<br>FTB                     | 116<br><5<br>SIP<br>FTB                     | 126<br><5<br>SIP<br>FTB                     | 118<br><5<br>SIP<br>FTB                     | 122<br><5<br>SIP<br>FTB                    | 121        |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)   | 121<br><5<br>SIP<br>FTB                     | 116<br><5<br>SIP<br>FTB                     | 126<br><5<br>SIP<br>FTB                     | 118<br><5<br>SIP<br>FTB                     | 122<br><5<br>SIP<br>FTB                    | 121        |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | 121<br><5<br>SIP<br>FTB<br>124<br><5        | 116<br><5<br>SIP<br>FTB<br>120<br><5        | 126<br><5<br>SIP<br>FTB<br>129<br><5        | 118<br><5<br>SIP<br>FTB<br>124<br><5        | 122<br><5<br>SIP<br>FTB<br>123<br><5       | 121        |
| Sample ID: DS-8   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  | 121<br><5<br>SIP<br>FTB<br>124<br><5<br>SIP | 116<br><5<br>SIP<br>FTB<br>120<br><5<br>SIP | 126<br><5<br>SIP<br>FTB<br>129<br><5<br>SIP | 118<br><5<br>SIP<br>FTB<br>124<br><5<br>SIP | 122<br><5<br>SIP<br>FTB<br>123<br><5<br>SE | 121        |
| Shear Elongation @ Break (%)  Sample ID: DS-8   Weld: Heat Fusion  Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Shear  Shear Strength (ppi) | 121<br><5<br>SIP<br>FTB<br>124<br><5<br>SIP | 116<br><5<br>SIP<br>FTB<br>120<br><5<br>SIP | 126<br><5<br>SIP<br>FTB<br>129<br><5<br>SIP | 118<br><5<br>SIP<br>FTB<br>124<br><5<br>SIP | 122<br><5<br>SIP<br>FTB<br>123<br><5<br>SE | Peel B 124 |

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Date: 2017-05-25

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29137

Material(s) Tested: (4) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Jennifer Tenney Project Manager

Sensip T. Tenney

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29137

### **TEST REPLICATE NUMBER**

|   |     | 1631 | TEST REPLICATE NUMBER |      |      |        |  |  |
|---|-----|------|-----------------------|------|------|--------|--|--|
| PARAMETER                                       | 1   | 2    | 3                     | 4    | 5    | MEAN   |  |  |
| Sample ID: DS-9   Weld: Heat Fusion             |     |      |                       |      |      |        |  |  |
| Side: A   |     |      |                       |      |      | Peel A |  |  |
| Peel Strength (ppi)                             | 119 | 118  | 112                   | 119  | 103  | 114    |  |  |
| Peel Incursion (%)                              | <5  | <5   | <5                    | <5   | <5   |        |  |  |
| Peel Locus Of Failure Code                      | SIP | SIP  | SIP                   | SIP  | SIP  |        |  |  |
| Peel NSF Failure Code                           | FTB | FTB  | FTB                   | FTB  | FTB  |        |  |  |
| Side: B   |     |      |                       |      |      | Peel B |  |  |
| Peel Strength (ppi)                             | 109 | 115  | 108                   | 113  | 110  | 111    |  |  |
| Peel Incursion (%)                              | <5  | <5   | <5                    | <5   | <5   |        |  |  |
| Peel Locus Of Failure Code                      | SIP | SIP  | SIP                   | SIP  | SIP  |        |  |  |
| Peel NSF Failure Code                           | FTB | FTB  | FTB                   | FTB  | FTB  |        |  |  |
| Shear   |     |      |                       |      |      | Shear  |  |  |
| Shear Strength (ppi)                            | 143 | 143  | 144                   | 143  | 142  | 143    |  |  |
| Shear Elongation @ Break (%)                    | >50 | >50  | >50                   | >50  | >50  |        |  |  |
| Sample ID: DS-10   Weld: Heat Fusion<br>Side: A | 1   |      |                       |      |      | Peel A |  |  |
| Peel Strength (ppi)                             | 123 | 118  | 122                   | 115  | 120  | 120    |  |  |
| Peel Incursion (%)                              | <5  | <5   | <5                    | <5   | <5   |        |  |  |
| Peel Locus Of Failure Code                      | SIP | SIP  | SIP                   | SIP  | SIP  |        |  |  |
| Peel NSF Failure Code                           | FTB | FTB  | FTB                   | FTB  | FTB  |        |  |  |
| Side: B   |     |      |                       |      |      | Peel B |  |  |
| Peel Strength (ppi)                             | 122 | 120  | 125                   | 121  | 121  | 122    |  |  |
| Peel Incursion (%)                              | <5  | <5   | <5                    | <5   | <5   |        |  |  |
| Peel Locus Of Failure Code                      | SIP | SIP  | SIP                   | SIP  | SIP  |        |  |  |
| Peel NSF Failure Code                           | FTB | FTB  | FTB                   | FTB  | FTB  |        |  |  |
| Shear   |     |      |                       |      |      | Shear  |  |  |
|   |     |      |                       | 1.40 | 2.45 |        |  |  |
| Shear Strength (ppi)                            | 146 | 146  | 142                   | 148  | 145  | 145    |  |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29137

### **TEST REPLICATE NUMBER**

|   | TEST REPLICATE NUMBER                |                                      |                                      |                                      |                                      |               |
|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| PARAMETER   | 1                                    | 2                                    | 3                                    | 4                                    | 5                                    | MEAN          |
| Sample ID: DS-11   Weld: Heat Fusion  |                                      |                                      |                                      |                                      |                                      |               |
| Side: A   |                                      |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)   | 113                                  | 109                                  | 116                                  | 106                                  | 110                                  | 111           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B   |                                      |                                      |                                      |                                      |                                      | Peel B        |
| Peel Strength (ppi)   | 110                                  | 124                                  | 117                                  | 116                                  | 117                                  | 117           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SE                                   | SIP                                  | SE                                   | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Shear   |                                      |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)  | 154                                  | 156                                  | 151                                  | 153                                  | 153                                  | 153           |
| Shear Elongation @ Break (%)  | >50                                  | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-12   Weld: Heat Fusion<br>Side: A   | <u> </u>                             |                                      |                                      |                                      |                                      | Peel A        |
|   |                                      |                                      |                                      |                                      |                                      | reel A        |
| Peel Strength (ppi)   | 110                                  | 113                                  | 112                                  | 117                                  | 113                                  | 113           |
|   | 110<br><5                            | 113<br><5                            | 112<br><5                            | 117<br><5                            | 113<br><5                            |               |
| Peel Incursion (%)  |                                      |                                      |                                      |                                      | _                                    |               |
| Peel Incursion (%)<br>Peel Locus Of Failure Code  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code   | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B   | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 113           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)                              | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 113           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 113           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code                       | <5<br>SIP<br>FTB<br>105<br><5        | <5<br>SIP<br>FTB<br>118<br><5        | <5<br>SIP<br>FTB<br>119<br><5        | <5<br>SIP<br>FTB<br>121<br><5        | <5<br>SIP<br>FTB<br>113<br><5        | 113           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code | <5<br>SIP<br>FTB<br>105<br><5<br>SIP | <5<br>SIP<br>FTB<br>118<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | <5<br>SIP<br>FTB<br>121<br><5<br>SIP | <5<br>SIP<br>FTB<br>113<br><5<br>SIP | 113           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%)  | <5<br>SIP<br>FTB<br>105<br><5<br>SIP | <5<br>SIP<br>FTB<br>118<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | <5<br>SIP<br>FTB<br>121<br><5<br>SIP | <5<br>SIP<br>FTB<br>113<br><5<br>SIP | Peel B<br>115 |

Date: 2017-05-30

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29214

Material(s) Tested: (4) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29214

### **TEST REPLICATE NUMBER**

|                                      |     | TEST | REPLICATE N | UMBEK |     |        |
|--------------------------------------|-----|------|-------------|-------|-----|--------|
| PARAMETER                            | 1   | 2    | 3           | 4     | 5   | MEAN   |
| Sample ID: DS-13   Weld: Heat Fusion |     |      |             |       |     |        |
| Side: A                              |     |      |             |       |     | Peel A |
| Peel Strength (ppi)                  | 132 | 127  | 127         | 126   | 126 | 128    |
| Peel Incursion (%)                   | <5  | <5   | <5          | <5    | <5  |        |
| Peel Locus Of Failure Code           | SE  | SE   | SE          | SE    | SE  |        |
| Peel NSF Failure Code                | FTB | FTB  | FTB         | FTB   | FTB |        |
| Side: B                              |     |      |             |       |     | Peel B |
| Peel Strength (ppi)                  | 118 | 123  | 122         | 117   | 125 | 121    |
| Peel Incursion (%)                   | <5  | <5   | <5          | <5    | <5  |        |
| Peel Locus Of Failure Code           | SIP | SE   | SIP         | SIP   | SE  |        |
| Peel NSF Failure Code                | FTB | FTB  | FTB         | FTB   | FTB |        |
| Shear                                |     |      |             |       |     | Shear  |
| Shear Strength (ppi)                 | 150 | 151  | 151         | 151   | 152 | 151    |
| Shear Elongation @ Break (%)         | >50 | >50  | >50         | >50   | >50 |        |
|                                      |     |      |             |       |     |        |
| Sample ID: DS-14   Weld: Heat Fusion |     |      |             |       |     |        |
| Side: A                              |     |      |             |       |     | Peel A |
| Peel Strength (ppi)                  | 121 | 135  | 118         | 124   | 120 | 124    |
| Peel Incursion (%)                   | <5  | <5   | <5          | <5    | <5  |        |
| Peel Locus Of Failure Code           | SE  | SIP  | SIP         | SIP   | SE  |        |
| Peel NSF Failure Code                | FTB | FTB  | FTB         | FTB   | FTB |        |
| Side: B                              |     |      |             |       |     | Peel B |
| Peel Strength (ppi)                  | 132 | 128  | 128         | 125   | 127 | 128    |
| Peel Incursion (%)                   | <5  | <5   | <5          | <5    | <5  |        |
| Peel Locus Of Failure Code           | SIP | SIP  | SIP         | SIP   | SIP |        |
| Peel NSF Failure Code                | FTB | FTB  | FTB         | FTB   | FTB |        |
| . ccc aa.c ccac                      |     |      |             |       |     | Shear  |
|                                      |     |      |             |       |     | Sileai |
| Shear Shear Strength (ppi)           | 149 | 155  | 153         | 154   | 153 | 153    |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29214

### **TEST REPLICATE NUMBER**

|   | TEST REPLICATE NUMBER                       |                                      |                                      |                                     |                                      |            |
|---|---|--------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------|------------|
| PARAMETER   | 1   | 2                                    | 3                                    | 4                                   | 5                                    | MEAN       |
| Sample ID: DS-15   Weld: Heat Fusion  | l   |                                      |                                      |                                     |                                      |            |
| Side: A   |   |                                      |                                      |                                     |                                      | Peel A     |
| Peel Strength (ppi)   | 124   | 139                                  | 139                                  | 130                                 | 124                                  | 131        |
| Peel Incursion (%)  | <5  | <5                                   | <5                                   | <5                                  | <5                                   |            |
| Peel Locus Of Failure Code  | SIP   | SE                                   | SIP                                  | SE                                  | SIP                                  |            |
| Peel NSF Failure Code   | FTB   | FTB                                  | FTB                                  | FTB                                 | FTB                                  |            |
| Side: B   |   |                                      |                                      |                                     |                                      | Peel B     |
| Peel Strength (ppi)   | 127   | 129                                  | 126                                  | 126                                 | 126                                  | 127        |
| Peel Incursion (%)  | <5  | <5                                   | <5                                   | <5                                  | <5                                   |            |
| Peel Locus Of Failure Code  | SIP   | SIP                                  | SIP                                  | SIP                                 | SIP                                  |            |
| Peel NSF Failure Code   | FTB   | FTB                                  | FTB                                  | FTB                                 | FTB                                  |            |
| Shear   |   |                                      |                                      |                                     |                                      | Shear      |
| Shear Strength (ppi)  | 148   | 148                                  | 146                                  | 147                                 | 147                                  | 147        |
| Shear Elongation @ Break (%)  | >50   | >50                                  | >50                                  | >50                                 | >50                                  |            |
|   |   |                                      |                                      |                                     |                                      |            |
| ·   | <u> </u>                                    |                                      |                                      |                                     |                                      | Peel A     |
| Side: A   | 132   | 130                                  | 129                                  | 130                                 | 128                                  | Peel A     |
| Side: A Peel Strength (ppi)   |   | 130<br><5                            | 129<br><5                            | 130<br><5                           | 128<br><5                            |            |
| Side: A Peel Strength (ppi) Peel Incursion (%)  | 132   |                                      |                                      |                                     |                                      |            |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code   | 132<br><5                                   | <5                                   | <5                                   | <5                                  | <5                                   |            |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code   | 132<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SE                            | <5<br>SIP                            |            |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B   | 132<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SE                            | <5<br>SIP                            | 130        |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | 132<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SE<br>FTB                     | <5<br>SIP<br>FTB                     | 130        |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)   | 132<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SE<br>FTB                     | <5<br>SIP<br>FTB                     | 130        |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code   | 132<br><5<br>SIP<br>FTB<br>114<br><5        | <5<br>SIP<br>FTB<br>124<br><5        | <5<br>SIP<br>FTB<br>123<br><5        | <5<br>SE<br>FTB<br>128<br><5        | <5<br>SIP<br>FTB<br>125<br><5        | 130        |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  | 132<br><5<br>SIP<br>FTB<br>114<br><5<br>SIP | <5<br>SIP<br>FTB<br>124<br><5<br>SIP | <5<br>SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SE<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | 130        |
| Sample ID: DS-16   Weld: Heat Fusion  Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Shear  Shear Strength (ppi) | 132<br><5<br>SIP<br>FTB<br>114<br><5<br>SIP | <5<br>SIP<br>FTB<br>124<br><5<br>SIP | <5<br>SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SE<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | Peel B 123 |

Date: 2017-06-01

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29291

Material(s) Tested: (6) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29291

#### **TEST REPLICATE NUMBER**

|   | TEST REPLICATE NUMBER               |                                    |                                      |                                     |                                     |                      |
|---|-------------------------------------|------------------------------------|--------------------------------------|-------------------------------------|-------------------------------------|----------------------|
| PARAMETER   | 1                                   | 2                                  | 3                                    | 4                                   | 5                                   | MEAN                 |
| Sample ID: DS-17   Weld: Heat Fusion  |                                     |                                    |                                      |                                     |                                     |                      |
| Side: A   |                                     |                                    |                                      |                                     |                                     | Peel A               |
| Peel Strength (ppi)   | 121                                 | 95                                 | 112                                  | 114                                 | 115                                 | 111                  |
| Peel Incursion (%)  | <5                                  | 100                                | <5                                   | <5                                  | 100                                 |                      |
| Peel Locus Of Failure Code  | SIP                                 | AD                                 | SIP                                  | SIP                                 | AD                                  |                      |
| Peel NSF Failure Code   | FTB                                 | NON-FTB                            | FTB                                  | FTB                                 | NON-FTB                             |                      |
| Side: B   |                                     |                                    |                                      |                                     |                                     | Peel B               |
| Peel Strength (ppi)   | 127                                 | 131                                | 117                                  | 124                                 | 114                                 | 123                  |
| Peel Incursion (%)  | <5                                  | <5                                 | <5                                   | <5                                  | <5                                  |                      |
| Peel Locus Of Failure Code  | SIP                                 | SIP                                | SIP                                  | SIP                                 | SIP                                 |                      |
| Peel NSF Failure Code   | FTB                                 | FTB                                | FTB                                  | FTB                                 | FTB                                 |                      |
| Shear   |                                     |                                    |                                      |                                     |                                     | Shear                |
| Shear Strength (ppi)  | 154                                 | 154                                | 150                                  | 154                                 | 150                                 | 152                  |
| Shear Elongation @ Break (%)  | >50                                 | >50                                | >50                                  | >50                                 | >50                                 |                      |
| Sample ID: DS-18   Weld: Heat Fusion Side: A  |                                     |                                    |                                      |                                     |                                     |                      |
|   |                                     |                                    |                                      |                                     |                                     | Peel A               |
| Peel Strength (ppi)   | 121                                 | 118                                | 114                                  | 116                                 | 116                                 |                      |
| •   | 121<br><5                           | 118<br><5                          | 114<br><5                            | 116<br><5                           | 116 [                               | 117                  |
| Peel Incursion (%)  |                                     |                                    |                                      |                                     | L                                   |                      |
| Peel Incursion (%) Peel Locus Of Failure Code   | <5                                  | <5                                 | <5                                   | <5                                  | <b>&lt;</b> 5                       |                      |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code   | <5<br>SE                            | <5<br>SE                           | <5<br>SIP                            | <5<br>SE                            | <5<br>SE                            |                      |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SE                            | <5<br>SE                           | <5<br>SIP                            | <5<br>SE                            | <5<br>SE                            | 117                  |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SE<br>FTB                     | <5<br>SE<br>FTB                    | <5<br>SIP<br>FTB                     | <5<br>SE<br>FTB                     | <5<br>SE<br>FTB                     | 117<br>Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)  | <5<br>SE<br>FTB                     | <5<br>SE<br>FTB                    | <5<br>SIP<br>FTB                     | <5<br>SE<br>FTB                     | <5<br>SE<br>FTB                     | 117<br>Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Bide: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code                       | <5<br>SE<br>FTB<br>116<br><5        | <5<br>SE<br>FTB<br>124<br><5       | <5<br>SIP<br>FTB<br>122<br><5        | <5<br>SE<br>FTB<br>119<br><5        | <5<br>SE<br>FTB<br>120 [<br><5      | 117<br>Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code | <5<br>SE<br>FTB<br>116<br><5<br>SIP | <5<br>SE<br>FTB<br>124<br><5<br>SE | <5<br>SIP<br>FTB<br>122<br><5<br>SIP | <5<br>SE<br>FTB<br>119<br><5<br>SIP | <5<br>SE<br>FTB<br>120<br><5<br>SIP | 117<br>Peel B        |
| Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B  | <5<br>SE<br>FTB<br>116<br><5<br>SIP | <5<br>SE<br>FTB<br>124<br><5<br>SE | <5<br>SIP<br>FTB<br>122<br><5<br>SIP | <5<br>SE<br>FTB<br>119<br><5<br>SIP | <5<br>SE<br>FTB<br>120<br><5<br>SIP | 117<br>Peel B<br>120 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29291

### **TEST REPLICATE NUMBER**

| PARAMETER   | 1                                    | 2  | 3   | 4                          | 5                         | MEAN          |
|---|--------------------------------------|--|---|----------------------------|---------------------------|---------------|
| Sample ID: DS-19   Weld: Heat Fusion  |                                      |  |   |                            |                           |               |
| Side: A   |                                      |  |   |                            |                           | Peel A        |
| Peel Strength (ppi)   | 127                                  | 110  | 126   | 120                        | 132                       | 123           |
| Peel Incursion (%)  | <5                                   | <5   | 100   | <5                         | <5                        |               |
| Peel Locus Of Failure Code  | SE                                   | SE   | AD  | SE                         | SE                        |               |
| Peel NSF Failure Code   | FTB                                  | FTB  | NON-FTB                                     | FTB                        | FTB                       |               |
| Side: B   |                                      |  |   |                            |                           | Peel B        |
| Peel Strength (ppi)   | 81                                   | 123  | 96  | 125                        | 121                       | 109           |
| Peel Incursion (%)  | 90                                   | 90   | 90  | <5                         | <5                        |               |
| Peel Locus Of Failure Code  | AD-BRK                               | AD-BRK                                     | AD-BRK                                      | SE                         | SE                        |               |
| Peel NSF Failure Code   | FTB                                  | FTB  | FTB   | FTB                        | FTB                       |               |
| Shear   |                                      |  |   |                            |                           | Shear         |
| Shear Strength (ppi)  | 157                                  | 156  | 154   | 153                        | 153                       | 155           |
| Shear Elongation @ Break (%)  | >50                                  | >50  | >50   | >50                        | >50                       |               |
| Sample ID: DS-20   Weld: Heat Fusion Side: A  |                                      |  |   |                            |                           | Peel A        |
| Peel Strength (ppi)   | 82                                   | 129  | 63  | 65                         | 55                        |               |
|   |                                      |  |   |                            |                           | 79            |
| Peel Incursion (%)  | 90                                   | 90   | 100   | 100                        | 100                       | 79            |
| , ,   | 90<br>AD-BRK                         |  |   | 100<br>AD                  | 100<br>AD                 | 79            |
| Peel Locus Of Failure Code  |                                      | 90   | 100   |                            |                           | 79            |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code   | AD-BRK                               | 90<br>AD-BRK                               | 100<br>AD                                   | AD                         | AD                        |               |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | AD-BRK                               | 90<br>AD-BRK                               | 100<br>AD                                   | AD                         | AD                        |               |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | AD-BRK<br>FTB                        | 90<br>AD-BRK<br>FTB                        | 100<br>AD<br>NON-FTB                        | AD<br>NON-FTB              | AD<br>NON-FTB             | Peel B        |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)   | AD-BRK<br>FTB<br>121                 | 90<br>AD-BRK<br>FTB<br>132                 | 100<br>AD<br>NON-FTB<br>138                 | AD<br>NON-FTB<br>100       | AD<br>NON-FTB<br>98       | Peel B        |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | AD-BRK<br>FTB<br>121<br>90           | 90<br>AD-BRK<br>FTB<br>132<br>90           | 100<br>AD<br>NON-FTB<br>138<br>20           | AD<br>NON-FTB<br>100<br>90 | AD NON-FTB  98  90        | Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear | AD-BRK<br>FTB<br>121<br>90<br>AD-BRK | 90<br>AD-BRK<br>FTB<br>132<br>90<br>AD-BRK | 100<br>AD<br>NON-FTB<br>138<br>20<br>AD-BRK | AD NON-FTB  100 90 AD-BRK  | AD NON-FTB  98  90 AD-BRK | Peel B        |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code                          | AD-BRK<br>FTB<br>121<br>90<br>AD-BRK | 90<br>AD-BRK<br>FTB<br>132<br>90<br>AD-BRK | 100<br>AD<br>NON-FTB<br>138<br>20<br>AD-BRK | AD NON-FTB  100 90 AD-BRK  | AD NON-FTB  98  90 AD-BRK | Peel B<br>118 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29291

### **TEST REPLICATE NUMBER**

| PARAMETER   | 1                | 2                | 3                | 4                | 5                  | MEAN   |
|---|------------------|------------------|------------------|------------------|--------------------|--------|
| Sample ID: DS-21   Weld: Heat Fusion  | 1                |                  |                  |                  |                    |        |
| Side: A   |                  |                  |                  |                  |                    | Peel A |
| Peel Strength (ppi)   | 122              | 126              | 129              | 113              | 128                | 124    |
| Peel Incursion (%)  | <5               | <5               | 100              | <5               | 100                |        |
| Peel Locus Of Failure Code  | SIP              | SIP              | AD               | SIP              | AD                 |        |
| Peel NSF Failure Code   | FTB              | FTB              | NON-FTB          | FTB              | NON-FTB            |        |
| Side: B   |                  |                  |                  |                  |                    | Peel B |
| Peel Strength (ppi)   | 126              | 128              | 127              | 125              | 122                | 126    |
| Peel Incursion (%)  | <5               | <5               | <5               | <5               | <5                 |        |
| Peel Locus Of Failure Code  | SIP              | SIP              | SIP              | SIP              | SIP                |        |
| Peel NSF Failure Code   | FTB              | FTB              | FTB              | FTB              | FTB                |        |
| Shear   |                  |                  |                  |                  |                    | Shear  |
| Shear Strength (ppi)  | 144              | 149              | 147              | 147              | 145                | 146    |
| Shear Elongation @ Break (%)  | >50              | >50              | >50              | >50              | >50                |        |
| Sample ID: DS-22   Weld: Heat Fusion<br>Side: A   | 1                |                  |                  |                  |                    | Peel A |
| Peel Strength (ppi)   | 128              | 124              | 133              | 130              | 132                | 129    |
| Peel Incursion (%)  | <5               | <5               | <5               | <5               | <5                 |        |
| Peel Locus Of Failure Code  | SE               | SIP              | SIP              | SIP              | SIP                |        |
|   |                  |                  |                  |                  |                    |        |
| Peel NSF Failure Code   | FTB              | FTB              | FTB              | FTB              | FTB                |        |
|   | FTB              | FTB              | FTB              | FTB              | FTB                | Peel B |
| Side: B   | FTB<br>125       | FTB<br>128       | FTB<br>123       | FTB<br>126       | FTB<br>130         | Peel B |
| Side: B Peel Strength (ppi)   |                  |                  |                  |                  | г                  |        |
| Side: B Peel Strength (ppi) Peel Incursion (%)  | 125              | 128              | 123              | 126              | 130                |        |
| Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code   | 125<br><5        | 128<br><5        | 123<br><5        | 126<br><5        | 130 [<br><5        |        |
| Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code   | 125<br><5<br>SIP | 128<br><5<br>SIP | 123<br><5<br>SIP | 126<br><5<br>SIP | 130 [<br><5<br>SIP |        |
| Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Shear  Shear Strength (ppi) | 125<br><5<br>SIP | 128<br><5<br>SIP | 123<br><5<br>SIP | 126<br><5<br>SIP | 130 [<br><5<br>SIP | 126    |

Date: 2017-06-06

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29404

Material(s) Tested: (11) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29404

### **TEST REPLICATE NUMBER**

|  |         | 1201 NEI EIGHT NOMBEN |         |         |         |        |  |
|--|---------|-----------------------|---------|---------|---------|--------|--|
| PARAMETER                                      | 1       | 2                     | 3       | 4       | 5       | MEAN   |  |
| Sample ID: DS-17A   Weld: Heat Fusi            | ion     |                       |         |         |         |        |  |
| Side: A  |         |                       |         |         |         | Peel A |  |
| Peel Strength (ppi)                            | 120     | 111                   | 120     | 89      | 118     | 112    |  |
| Peel Incursion (%)                             | 100     | 100                   | <5      | 100     | <5      |        |  |
| Peel Locus Of Failure Code                     | AD      | AD                    | SIP     | AD      | SIP     |        |  |
| Peel NSF Failure Code                          | NON-FTB | NON-FTB               | FTB     | NON-FTB | FTB     |        |  |
| Side: B  |         |                       |         |         |         | Peel B |  |
| Peel Strength (ppi)                            | 61      | 101                   | 125     | 108     | 126     | 104    |  |
| Peel Incursion (%)                             | 100     | 100                   | <5      | 100     | <5      |        |  |
| Peel Locus Of Failure Code                     | AD      | AD                    | SIP     | AD      | SE      |        |  |
| Peel NSF Failure Code                          | NON-FTB | NON-FTB               | FTB     | NON-FTB | FTB     |        |  |
| Shear  |         |                       |         |         |         | Shear  |  |
| Shear Strength (ppi)                           | 155     | 160                   | 156     | 159     | 161     | 158    |  |
| Shear Elongation @ Break (%)                   | >50     | >50                   | >50     | >50     | >50     |        |  |
| Sample ID: DS-17B   Weld: Heat Fusi<br>Side: A | ion     |                       |         |         |         | Peel A |  |
| Peel Strength (ppi)                            | 93      | 99                    | 103     | 85      | 81      | 92     |  |
| Peel Incursion (%)                             | 100     | 100                   | 100     | 100     | 100     |        |  |
| Peel Locus Of Failure Code                     | AD      | AD                    | AD      | AD      | AD      |        |  |
| Peel NSF Failure Code                          | NON-FTB | NON-FTB               | NON-FTB | NON-FTB | NON-FTB |        |  |
| Side: B  |         |                       |         |         |         | Peel B |  |
| Peel Strength (ppi)                            | 121     | 123                   | 126     | 121     | 128     | 124    |  |
| Peel Incursion (%)                             | <5      | <5                    | <5      | <5      | <5      |        |  |
| Peel Locus Of Failure Code                     | SIP     | SIP                   | SIP     | SIP     | SIP     |        |  |
| Peel NSF Failure Code                          | FTB     | FTB                   | FTB     | FTB     | FTB     |        |  |
| Shear  |         |                       |         |         |         | Shear  |  |
|  |         |                       |         |         | Г       |        |  |
| Shear Strength (ppi)                           | 161     | 164                   | 160     | 160     | 162     | 161    |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29404

#### TEST REPLICATE NUMBER

|  | TEST REPLICATE NUMBER                      |                                  |  |                                    |                               |                      |
|--|--|----------------------------------|--|------------------------------------|-------------------------------|----------------------|
| PARAMETER  | 1  | 2                                | 3  | 4                                  | 5                             | MEAN                 |
| Sample ID: DS-19A   Weld: Heat Fusio   | n  |                                  |  |                                    |                               |                      |
| Side: A  |  |                                  |  |                                    |                               | Peel A               |
| Peel Strength (ppi)  | 124  | 116                              | 116                                      | 122                                | 114                           | 118                  |
| Peel Incursion (%)   | 100  | 100                              | 100                                      | 100                                | 100                           |                      |
| Peel Locus Of Failure Code   | AD   | AD                               | AD                                       | AD                                 | AD                            |                      |
| Peel NSF Failure Code  | NON-FTB                                    | NON-FTB                          | NON-FTB                                  | NON-FTB                            | NON-FTB                       |                      |
| Side: B  |  |                                  |  |                                    |                               | Peel B               |
| Peel Strength (ppi)  | 122  | 119                              | 116                                      | 121                                | 123                           | 120                  |
| Peel Incursion (%)   | 100  | 100                              | 100                                      | 100                                | 100                           |                      |
| Peel Locus Of Failure Code   | AD   | AD                               | AD                                       | AD                                 | AD                            |                      |
| Peel NSF Failure Code  | NON-FTB                                    | NON-FTB                          | NON-FTB                                  | NON-FTB                            | NON-FTB                       |                      |
| Shear  |  |                                  |  |                                    |                               | Shear                |
| Shear Strength (ppi)   | 158  | 162                              | 159                                      | 159                                | 162                           | 160                  |
| Shear Elongation @ Break (%)   | >50  | >50                              | >50                                      | >50                                | >50                           |                      |
|  |  |                                  |  |                                    |                               |                      |
| ,  | n  |                                  |  |                                    |                               | Peel A               |
| Side: A  | n 133                                      | 120                              | 121                                      | 126                                | 116                           | Peel A               |
| Side: A Peel Strength (ppi)  |  | 120<br>30                        | 121<br>100                               | 126<br><5                          | 116 [<br>100                  |                      |
| Side: A Peel Strength (ppi) Peel Incursion (%)   | 133  |                                  |  |                                    |                               |                      |
| Gide: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | 133<br><5                                  | 30                               | 100                                      | <5                                 | 100                           |                      |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  | 133<br><5<br>SE                            | 30<br>AD-BRK                     | 100<br>AD                                | <5<br>SE                           | 100<br>AD                     |                      |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | 133<br><5<br>SE                            | 30<br>AD-BRK                     | 100<br>AD                                | <5<br>SE                           | 100<br>AD                     | 123                  |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | 133<br><5<br>SE<br>FTB                     | 30<br>AD-BRK<br>FTB              | 100<br>AD<br>NON-FTB                     | <5<br>SE<br>FTB                    | 100<br>AD<br>NON-FTB          | 123                  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)   | 133<br><5<br>SE<br>FTB                     | 30<br>AD-BRK<br>FTB<br>135       | 100<br>AD<br>NON-FTB<br>117              | <5<br>SE<br>FTB                    | 100<br>AD<br>NON-FTB          | 123                  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | 133<br><5<br>SE<br>FTB<br>135<br><5        | 30<br>AD-BRK<br>FTB<br>135<br><5 | 100<br>AD<br>NON-FTB<br>117<br>100       | <5<br>SE<br>FTB<br>132<br><5       | 100<br>AD<br>NON-FTB<br>114 [ | 123                  |
| Fide: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code   | 133<br><5<br>SE<br>FTB<br>135<br><5<br>SIP | 30 AD-BRK FTB  135 <5 SIP        | 100<br>AD<br>NON-FTB<br>117<br>100<br>AD | <5<br>SE<br>FTB<br>132<br><5<br>SE | 100 AD NON-FTB  114 <5 SIP    | 123                  |
| Sample ID: DS-19B   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Shear Strength (ppi) | 133<br><5<br>SE<br>FTB<br>135<br><5<br>SIP | 30 AD-BRK FTB  135 <5 SIP        | 100<br>AD<br>NON-FTB<br>117<br>100<br>AD | <5<br>SE<br>FTB<br>132<br><5<br>SE | 100 AD NON-FTB  114 <5 SIP    | 123<br>Peel B<br>127 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29404

#### TEST REPLICATE NUMBER

|  | TEST REPLICATE NUMBER                    |  |  |  |  |                      |
|--|--|--|--|--|--|----------------------|
| PARAMETER  | 1  | 2  | 3  | 4  | 5  | MEAN                 |
| Sample ID: DS-20A   Weld: Heat Fusio   | n  |  |  |  |  |                      |
| Side: A  |  |  |  |  |  | Peel A               |
| Peel Strength (ppi)  | 94                                       | 125                                      | 92                                       | 128                                      | 114                                      | 111                  |
| Peel Incursion (%)   | <5                                       | <5                                       | <5                                       | <5                                       | <5                                       |                      |
| Peel Locus Of Failure Code   | SE                                       | SE                                       | SIP                                      | SIP                                      | SE                                       |                      |
| Peel NSF Failure Code  | FTB                                      | FTB                                      | FTB                                      | FTB                                      | FTB                                      |                      |
| Side: B  |  |  |  |  |  | Peel B               |
| Peel Strength (ppi)  | 38                                       | 111                                      | 110                                      | 123                                      | 109                                      | 98                   |
| Peel Incursion (%)   | 100                                      | 100                                      | 100                                      | 100                                      | 100                                      |                      |
| Peel Locus Of Failure Code   | AD                                       | AD                                       | AD                                       | AD                                       | AD                                       |                      |
| Peel NSF Failure Code  | NON-FTB                                  | NON-FTB                                  | NON-FTB                                  | NON-FTB                                  | NON-FTB                                  |                      |
| Shear  |  |  |  |  |  | Shear                |
| Shear Strength (ppi)   | 143                                      | 149                                      | 148                                      | 150                                      | 147                                      | 147                  |
| Shear Elongation @ Break (%)   | >50                                      | >50                                      | >50                                      | >50                                      | >50                                      |                      |
| Sample ID: DS-20B   Weld: Heat Fusio<br>Side: A  | n  |  |  |  |  |                      |
|  |  |  |  |  |  | Peel A               |
| Peel Strength (ppi)  | 112                                      | 118                                      | 116                                      | 111                                      | 114                                      | Peel A<br>114        |
| •  | 112<br>100                               | 118<br>100                               | 116<br>100                               | 111<br>100                               | 114 [<br>100                             |                      |
| Peel Incursion (%)   |  |  |  |  | L  |                      |
| Peel Incursion (%) Peel Locus Of Failure Code  | 100                                      | 100                                      | 100                                      | 100                                      | 100                                      |                      |
| Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code  | 100<br>AD                                | 100<br>AD                                | 100<br>AD                                | 100<br>AD                                | 100<br>AD                                |                      |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | 100<br>AD                                | 100<br>AD                                | 100<br>AD                                | 100<br>AD                                | 100<br>AD                                | 114                  |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | 100<br>AD<br>NON-FTB                     | 100<br>AD<br>NON-FTB                     | 100<br>AD<br>NON-FTB                     | 100<br>AD<br>NON-FTB                     | 100<br>AD<br>NON-FTB                     | 114<br>Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%)   | 100<br>AD<br>NON-FTB<br>120              | 100<br>AD<br>NON-FTB                     | 100<br>AD<br>NON-FTB                     | 100<br>AD<br>NON-FTB<br>127              | 100 AD NON-FTB                           | 114<br>Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | 100<br>AD<br>NON-FTB<br>120<br>100       | 100<br>AD<br>NON-FTB<br>126<br>100       | 100<br>AD<br>NON-FTB<br>120<br>100       | 100<br>AD<br>NON-FTB<br>127<br>100       | 100<br>AD<br>NON-FTB<br>125 [<br>100     | 114<br>Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  Peel NSF Failure Code   | 100<br>AD<br>NON-FTB<br>120<br>100<br>AD | 100<br>AD<br>NON-FTB<br>126<br>100<br>AD | 100<br>AD<br>NON-FTB<br>120<br>100<br>AD | 100<br>AD<br>NON-FTB<br>127<br>100<br>AD | 100<br>AD<br>NON-FTB<br>125<br>100<br>AD | 114<br>Peel B        |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | 100<br>AD<br>NON-FTB<br>120<br>100<br>AD | 100<br>AD<br>NON-FTB<br>126<br>100<br>AD | 100<br>AD<br>NON-FTB<br>120<br>100<br>AD | 100<br>AD<br>NON-FTB<br>127<br>100<br>AD | 100<br>AD<br>NON-FTB<br>125<br>100<br>AD | 114<br>Peel B<br>124 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29404

### **TEST REPLICATE NUMBER**

|  | TEST REPLICATE NUMBER |           |              |         |           |            |
|--|-----------------------|-----------|--------------|---------|-----------|------------|
| PARAMETER  | 1                     | 2         | 3            | 4       | 5         | MEAN       |
| Sample ID: DS-21A   Weld: Heat Fusi              | ion                   |           |              |         |           |            |
| Side: A  |                       |           |              |         |           | Peel A     |
| Peel Strength (ppi)                              | 123                   | 134       | 134          | 127     | 128       | 129        |
| Peel Incursion (%)                               | <5                    | <5        | 100          | <5      | <5        |            |
| Peel Locus Of Failure Code                       | SIP                   | SE        | AD           | SIP     | SIP       |            |
| Peel NSF Failure Code                            | FTB                   | FTB       | NON-FTB      | FTB     | FTB       |            |
| Side: B  |                       |           |              |         |           | Peel B     |
| Peel Strength (ppi)                              | 128                   | 122       | 125          | 122     | 120       | 123        |
| Peel Incursion (%)                               | <5                    | <5        | <5           | <5      | <5        |            |
| Peel Locus Of Failure Code                       | SIP                   | SIP       | SIP          | SIP     | SIP       |            |
| Peel NSF Failure Code                            | FTB                   | FTB       | FTB          | FTB     | FTB       |            |
| Shear  |                       |           |              |         |           | Shear      |
| Shear Strength (ppi)                             | 161                   | 163       | 159          | 162     | 158       | 161        |
| Shear Elongation @ Break (%)                     | >50                   | >50       | >50          | >50     | >50       |            |
| Sample ID: DS-21B   Weld: Heat Fusi<br>Side: A   | ion                   |           |              |         |           | Peel A     |
|  | 125                   | 136       | 128          | 122     | 129       | 128        |
| Peel Strength (ppi)                              | 100                   |           |              | 100     |           | 128        |
| Peel Incursion (%)<br>Peel Locus Of Failure Code | AD                    | <5<br>SIP | <5<br>SIP    | AD      | <5<br>SIP |            |
| Peel NSF Failure Code                            | NON-FTB               | FTB       | FTB          | NON-FTB | FTB       |            |
| Side: B  | NON-FIB               | LIP       | LIR          | NON-FIB | FIB       | Peel B     |
|  | 127                   | 100       | 122          | 06      | 101       |            |
| Peel Strength (ppi)                              | 127                   | 109       | 123          | 96      | 131       | 117        |
| Peel Incursion (%)                               | <5                    | <5        | 30<br>AD DDK | <5      | <5        |            |
| Peel Locus Of Failure Code                       | SIP                   | SIP       | AD-BRK       | SIP     | SIP       |            |
| Peel NSF Failure Code                            | FTB                   | FTB       | FTB          | FTB     | FTB       | <b>C</b> 1 |
| Shear  |                       |           |              |         |           | Shear      |
| Shear Strength (ppi)                             | 158                   | 158       | 159          | 160     | 157       | 158        |
| Shear Elongation @ Break (%)                     | >50                   | >50       | >50          | >50     | >50       |            |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29404

### **TEST REPLICATE NUMBER**

|                                      |         | TES | I REPLICATE NU | IMBEK |               |              |
|--------------------------------------|---------|-----|----------------|-------|---------------|--------------|
| PARAMETER                            | 1       | 2   | 3              | 4     | 5             | MEAN         |
| Sample ID: DS-23   Weld: Heat Fusion |         |     |                |       |               |              |
| Side: A                              |         |     |                |       |               | Peel A       |
| Peel Strength (ppi)                  | 115     | 126 | 127            | 134   | 133           | 127          |
| Peel Incursion (%)                   | <5      | <5  | <5             | <5    | <b>&lt;</b> 5 |              |
| Peel Locus Of Failure Code           | SIP     | SIP | SIP            | SE    | SE            |              |
| Peel NSF Failure Code                | FTB     | FTB | FTB            | FTB   | FTB           |              |
| Side: B                              |         |     |                |       |               | Peel B       |
| Peel Strength (ppi)                  | 99      | 126 | 118            | 124   | 127           | 119          |
| Peel Incursion (%)                   | 100     | <5  | 100            | <5    | 70            |              |
| Peel Locus Of Failure Code           | AD      | SIP | AD             | SIP   | AD-BRK        |              |
| Peel NSF Failure Code                | NON-FTB | FTB | NON-FTB        | FTB   | FTB           |              |
| Shear                                |         |     |                |       |               | Shear        |
| Shear Strength (ppi)                 | 155     | 157 | 157            | 154   | 154           | 155          |
| Shear Elongation @ Break (%)         | >50     | >50 | >50            | >50   | >50           |              |
| Sample ID: DS-24   Weld: Heat Fusion | 1       |     |                |       |               |              |
| Side: A                              |         |     |                |       |               | Peel A       |
| Peel Strength (ppi)                  | 134     | 129 | 121            | 124   | 126           | 127          |
| Peel Incursion (%)                   | <5      | <5  | <5             | <5    | د<br><5       |              |
| Peel Locus Of Failure Code           | SE      | SE  | SE             | SE    | SE            |              |
| Peel NSF Failure Code                | FTB     | FTB | FTB            | FTB   | FTB           |              |
| Side: B                              |         |     |                |       |               | Peel B       |
| Peel Strength (ppi)                  | 133     | 119 | 111            | 129   | 133           | 125          |
| Peel Incursion (%)                   | <5      | <5  | <5             | <5    | <5            |              |
| Peel Locus Of Failure Code           | SIP     | SIP | SIP            | SIP   | SIP           |              |
| Peel NSF Failure Code                | FTB     | FTB | FTB            | FTB   | FTB           |              |
|                                      |         |     |                |       |               |              |
| Shear                                |         |     |                |       |               | Shear        |
| Shear Shear Strength (ppi)           | 159     | 164 | 160            | 159   | 163           | Shear<br>161 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29404

### **TEST REPLICATE NUMBER**

|                                      | 1201 1121 21011 2101 12211 |     |     |     |     |        |  |
|--------------------------------------|----------------------------|-----|-----|-----|-----|--------|--|
| PARAMETER                            | 1                          | 2   | 3   | 4   | 5   | MEAN   |  |
| Sample ID: DS-25   Weld: Heat Fusion |                            |     |     |     |     |        |  |
| Side: A                              |                            |     |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 149                        | 145 | 144 | 143 | 144 | 145    |  |
| Peel Incursion (%)                   | <5                         | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                        | SE  | SIP | SE  | SE  |        |  |
| Peel NSF Failure Code                | FTB                        | FTB | FTB | FTB | FTB |        |  |
| Side: B                              |                            |     |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 146                        | 148 | 147 | 143 | 146 | 146    |  |
| Peel Incursion (%)                   | <5                         | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SE                         | SIP | SE  | SIP | SE  |        |  |
| Peel NSF Failure Code                | FTB                        | FTB | FTB | FTB | FTB |        |  |
| Shear                                |                            |     |     |     |     | Shear  |  |
| Shear Strength (ppi)                 | 158                        | 158 | 161 | 160 | 157 | 159    |  |
| Shear Elongation @ Break (%)         | >50                        | >50 | >50 | >50 | >50 | •      |  |

Date: 2017-06-07

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29455

Material(s) Tested: (2) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29455

### **TEST REPLICATE NUMBER**

|                                      | TEST REPLICATE NUMBER |     |     |     |     |        |  |
|--------------------------------------|-----------------------|-----|-----|-----|-----|--------|--|
| PARAMETER                            | 1                     | 2   | 3   | 4   | 5   | MEAN   |  |
| Sample ID: DS-26   Weld: Heat Fusion |                       |     |     |     |     |        |  |
| Side: A                              |                       |     |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 137                   | 143 | 131 | 125 | 123 | 132    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Side: B                              |                       |     |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 115                   | 122 | 129 | 128 | 123 | 123    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Shear                                |                       |     |     |     |     | Shear  |  |
| Shear Strength (ppi)                 | 152                   | 148 | 150 | 152 | 149 | 150    |  |
| Shear Elongation @ Break (%)         | >50                   | >50 | >50 | >50 | >50 |        |  |
|                                      |                       |     |     |     |     |        |  |
| Sample ID: DS-27   Weld: Heat Fusion | 1                     |     |     |     |     |        |  |
| Side: A                              |                       |     |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 106                   | 93  | 118 | 91  | 123 | 106    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SE  | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Side: B                              |                       |     |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 126                   | 113 | 111 | 116 | 115 | 116    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Shear                                |                       |     |     |     |     | Shear  |  |
|                                      |                       |     |     |     |     |        |  |
| Shear Strength (ppi)                 | 154                   | 152 | 155 | 151 | 153 | 153    |  |

Date: 2017-06-09

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29535

Material(s) Tested: (15) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|   | TEST REPLICATE NUMBER |            |            |     |     |              |  |
|---|-----------------------|------------|------------|-----|-----|--------------|--|
| PARAMETER   | 1                     | 2          | 3          | 4   | 5   | MEAN         |  |
| Sample ID: DS-17 A2   Weld: Heat Fus  | sion                  |            |            |     |     |              |  |
| Side: A   |                       |            |            |     |     | Peel A       |  |
| Peel Strength (ppi)   | 131                   | 127        | 142        | 117 | 130 | 129          |  |
| Peel Incursion (%)  | <5                    | <5         | <5         | <5  | <5  | L .          |  |
| Peel Locus Of Failure Code  | SIP                   | SIP        | SIP        | SIP | SIP |              |  |
| Peel NSF Failure Code   | FTB                   | FTB        | FTB        | FTB | FTB |              |  |
| Side: B   |                       |            |            |     |     | Peel B       |  |
| Peel Strength (ppi)   | 123                   | 126        | 132        | 132 | 131 | 129          |  |
| Peel Incursion (%)  | <5                    | <5         | <5         | <5  | <5  |              |  |
| Peel Locus Of Failure Code  | SE                    | SIP        | SIP        | SIP | SIP |              |  |
| Peel NSF Failure Code   | FTB                   | FTB        | FTB        | FTB | FTB |              |  |
| Shear   |                       |            |            |     |     | Shear        |  |
| Shear Strength (ppi)  | 153                   | 154        | 152        | 150 | 155 | 153          |  |
| Shear Elongation @ Break (%)  | >50                   | >50        | >50        | >50 | >50 | L            |  |
|   |                       |            |            |     |     |              |  |
| Sample ID: DS-17 B2   Weld: Heat Fus  | sion                  |            |            |     |     |              |  |
| Side: A   |                       |            |            |     |     | Peel A       |  |
| Peel Strength (ppi)   | 135                   | 130        | 143        | 115 | 132 | 131          |  |
| Peel Incursion (%)  | <5                    | <5         | <5         | <5  | <5  |              |  |
| Peel Locus Of Failure Code  | SIP                   | SIP        | SIP        | SIP | SIP |              |  |
| Peel NSF Failure Code   | FTB                   | FTB        | FTB        | FTB | FTB |              |  |
| Side: B   |                       |            |            |     |     | Peel B       |  |
| Peel Strength (ppi)   | 132                   | 129        | 136        | 136 | 125 | 132          |  |
| Peel Incursion (%)  | <5                    | <5         | <5         | <5  | <5  |              |  |
| Death and Official Code   | SIP                   | SIP        | SIP        | SIP | SIP |              |  |
| Peel Locus Of Fallure Code  |                       |            |            | FTD | ETD |              |  |
|   | FTB                   | FTB        | FTB        | FTB | FTB |              |  |
| Peel NSF Failure Code   | FTB                   | FTB        | FTB        | FIR | FIR | Shear        |  |
| Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | FTB<br>154            | FTB<br>155 | FTB<br>157 | 157 | 155 | Shear<br>156 |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|   | TEST REFLICATE NUMBER |           |           |     |     |              |  |
|---|-----------------------|-----------|-----------|-----|-----|--------------|--|
| PARAMETER   | 1                     | 2         | 3         | 4   | 5   | MEAN         |  |
| Sample ID: DS-19 A2   Weld: Heat Fu                                       | sion                  |           |           |     |     |              |  |
| Side: A   |                       |           |           |     |     | Peel A       |  |
| Peel Strength (ppi)   | 122                   | 126       | 128       | 109 | 128 | 123          |  |
| Peel Incursion (%)  | <5                    | <5        | <5        | <5  | <5  |              |  |
| Peel Locus Of Failure Code  | SE                    | SE        | SIP       | SE  | SE  |              |  |
| Peel NSF Failure Code   | FTB                   | FTB       | FTB       | FTB | FTB |              |  |
| Side: B   |                       |           |           |     |     | Peel B       |  |
| Peel Strength (ppi)   | 120                   | 120       | 112       | 118 | 122 | 118          |  |
| Peel Incursion (%)  | <5                    | <5        | <5        | <5  | <5  |              |  |
| Peel Locus Of Failure Code  | SIP                   | SIP       | SIP       | SIP | SIP |              |  |
| Peel NSF Failure Code   | FTB                   | FTB       | FTB       | FTB | FTB |              |  |
| Shear   |                       |           |           |     |     | Shear        |  |
| Shear Strength (ppi)  | 163                   | 164       | 166       | 168 | 162 | 165          |  |
| Shear Elongation @ Break (%)  | >50                   | >50       | >50       | >50 | >50 |              |  |
| Sample ID: DS-19 B2   Weld: Heat Fus<br>Side: A                           | sion                  |           |           |     |     | Peel A       |  |
| Peel Strength (ppi)   | 134                   | 133       | 112       | 116 | 122 | 123          |  |
| Peel Incursion (%)  | <b>&lt;</b> 5         | <5        | <5        | <5  | <5  |              |  |
| Peel Locus Of Failure Code  | SE                    | SIP       | SIP       | SIP | SE  |              |  |
| Peel NSF Failure Code   | FTB                   | FTB       | FTB       | FTB | FTB |              |  |
| Side: B   |                       |           |           |     |     | Peel B       |  |
| Peel Strength (ppi)   | 138                   | 74        | 126       | 126 | 131 | 119          |  |
|   |                       |           | _         | <5  | <5  | L            |  |
| Peel Incursion (%)  | <5                    | <5        | <5        | ~5  | < 5 |              |  |
| , ,   | <5<br>SIP             | <5<br>SIP | <5<br>SIP | SIP | SIP |              |  |
| Peel Locus Of Failure Code  |                       |           |           |     |     |              |  |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear | SIP                   | SIP       | SIP       | SIP | SIP | Shear        |  |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code                       | SIP                   | SIP       | SIP       | SIP | SIP | Shear<br>165 |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|                                     |         | TEST REPLICATE NUMBER |         |         |         |        |  |
|-------------------------------------|---------|-----------------------|---------|---------|---------|--------|--|
| PARAMETER                           | 1       | 2                     | 3       | 4       | 5       | MEAN   |  |
| Sample ID: DS-20 A2   Weld: Heat Fu | ısion   |                       |         |         |         |        |  |
| Side: A                             |         |                       |         |         |         | Peel A |  |
| Peel Strength (ppi)                 | 119     | 115                   | 120     | 117     | 103     | 115    |  |
| Peel Incursion (%)                  | 100     | 100                   | <5      | 60      | 100     |        |  |
| Peel Locus Of Failure Code          | AD      | AD                    | SIP     | AD-BRK  | AD      |        |  |
| Peel NSF Failure Code               | NON-FTB | NON-FTB               | FTB     | FTB     | NON-FTB |        |  |
| Side: B                             |         |                       |         |         |         | Peel B |  |
| Peel Strength (ppi)                 | 115     | 100                   | 113     | 115     | 109     | 110    |  |
| Peel Incursion (%)                  | 85      | 90                    | <5      | <5      | 100     |        |  |
| Peel Locus Of Failure Code          | AD-BRK  | AD-BRK                | SIP     | SIP     | AD      |        |  |
| Peel NSF Failure Code               | FTB     | FTB                   | FTB     | FTB     | NON-FTB |        |  |
| Shear                               |         |                       |         |         |         | Shear  |  |
| Shear Strength (ppi)                | 156     | 155                   | 152     | 155     | 150     | 154    |  |
| Shear Elongation @ Break (%)        | >50     | >50                   | >50     | >50     | >50     |        |  |
|                                     |         |                       |         |         |         |        |  |
| Sample ID: DS-20 B2   Weld: Heat Fu | ısion   |                       |         |         |         |        |  |
| Side: A                             |         |                       |         |         | _       | Peel A |  |
| Peel Strength (ppi)                 | 110     | 112                   | 113     | 112     | 111     | 112    |  |
| Peel Incursion (%)                  | 90      | 100                   | 100     | 100     | 100     |        |  |
| Peel Locus Of Failure Code          | AD-BRK  | AD                    | AD      | AD      | AD      |        |  |
| Peel NSF Failure Code               | FTB     | NON-FTB               | NON-FTB | NON-FTB | NON-FTB |        |  |
| Side: B                             |         |                       |         |         |         | Peel B |  |
| Peel Strength (ppi)                 | 102     | 102                   | 117     | 128     | 98      | 109    |  |
| Peel Incursion (%)                  | 100     | 100                   | 90      | 90      | 90      |        |  |
| Peel Locus Of Failure Code          | AD      | AD                    | AD-BRK  | AD-BRK  | AD-BRK  |        |  |
| Peel NSF Failure Code               | NON-FTB | NON-FTB               | FTB     | FTB     | FTB     |        |  |
| Shear                               |         |                       |         |         |         | Shear  |  |
| Shear Strength (ppi)                | 152     | 165                   | 158     | 166     | 164     | 161    |  |
|                                     | >50     | >50                   | >50     | >50     | >50     |        |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|  | TEST REPLICATE NUMBER                    |                                      |   |                                      |                                     |                      |  |
|--|--|--------------------------------------|---|--------------------------------------|-------------------------------------|----------------------|--|
| PARAMETER  | 1  | 2                                    | 3                                       | 4                                    | 5                                   | MEAN                 |  |
| Sample ID: DS-21 A2   Weld: Heat Fu  | ısion                                    |                                      |   |                                      |                                     |                      |  |
| Side: A  |  |                                      |   |                                      |                                     | Peel A               |  |
| Peel Strength (ppi)  | 130                                      | 127                                  | 131                                     | 123                                  | 114                                 | 125                  |  |
| Peel Incursion (%)   | <5                                       | <5                                   | <5                                      | <5                                   | <5                                  |                      |  |
| Peel Locus Of Failure Code   | SIP                                      | SIP                                  | SIP                                     | SIP                                  | SIP                                 |                      |  |
| Peel NSF Failure Code  | FTB                                      | FTB                                  | FTB                                     | FTB                                  | FTB                                 |                      |  |
| Side: B  |  |                                      |   |                                      |                                     | Peel B               |  |
| Peel Strength (ppi)  | 114                                      | 114                                  | 118                                     | 116                                  | 128                                 | 118                  |  |
| Peel Incursion (%)   | <5                                       | <5                                   | <5                                      | <5                                   | <5                                  |                      |  |
| Peel Locus Of Failure Code   | SIP                                      | SIP                                  | SIP                                     | SIP                                  | SIP                                 |                      |  |
| Peel NSF Failure Code  | FTB                                      | FTB                                  | FTB                                     | FTB                                  | FTB                                 |                      |  |
| Shear  |  |                                      |   |                                      |                                     | Shear                |  |
| Shear Strength (ppi)   | 160                                      | 159                                  | 158                                     | 161                                  | 160                                 | 160                  |  |
| Shear Elongation @ Break (%)   | >50                                      | >50                                  | >50                                     | >50                                  | >50                                 |                      |  |
| Sample ID: DS-21 B2   Weld: Heat Fu  | ision                                    |                                      |   |                                      |                                     |                      |  |
| Side: A  |  |                                      |   |                                      |                                     | Peel A               |  |
|  | 132                                      | 127                                  | 134                                     | 141                                  | 129                                 | Peel A               |  |
| Peel Strength (ppi)  | 132<br>100                               | 127<br><5                            | 134<br>100                              | 141<br><5                            | 129 [<br>100                        |                      |  |
| Peel Strength (ppi) Peel Incursion (%)   |  |                                      |   |                                      | L                                   |                      |  |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code  | 100                                      | <5                                   | 100                                     | <5                                   | 100                                 |                      |  |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code   | 100<br>AD                                | <5<br>SIP                            | 100<br>AD                               | <5<br>SIP                            | 100<br>AD                           |                      |  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | 100<br>AD                                | <5<br>SIP                            | 100<br>AD                               | <5<br>SIP                            | 100<br>AD                           | 133                  |  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | 100<br>AD<br>NON-FTB                     | <5<br>SIP<br>FTB                     | 100<br>AD<br>NON-FTB                    | <5<br>SIP<br>FTB                     | 100<br>AD<br>NON-FTB                | 133<br>Peel B        |  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)   | 100<br>AD<br>NON-FTB                     | <5<br>SIP<br>FTB                     | 100<br>AD<br>NON-FTB                    | <5<br>SIP<br>FTB                     | 100 AD NON-FTB                      | 133<br>Peel B        |  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | 100<br>AD<br>NON-FTB<br>121<br><5        | <5<br>SIP<br>FTB<br>119<br><5        | 100<br>AD<br>NON-FTB<br>95<br><5        | <5<br>SIP<br>FTB<br>120<br><5        | 100<br>AD<br>NON-FTB<br>125 [<br><5 | 133<br>Peel B        |  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code                                    | 100<br>AD<br>NON-FTB<br>121<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | 100<br>AD<br>NON-FTB<br>95<br><5<br>SIP | <5<br>SIP<br>FTB<br>120<br><5<br>SIP | 100 AD NON-FTB  125 <5 SIP          | 133<br>Peel B        |  |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | 100<br>AD<br>NON-FTB<br>121<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | 100<br>AD<br>NON-FTB<br>95<br><5<br>SIP | <5<br>SIP<br>FTB<br>120<br><5<br>SIP | 100 AD NON-FTB  125 <5 SIP          | 133<br>Peel B<br>116 |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|  |           | TEST REPLICATE NUMBER |           |           |           |        |  |
|--|-----------|-----------------------|-----------|-----------|-----------|--------|--|
| PARAMETER  | 1         | 2                     | 3         | 4         | 5         | MEAN   |  |
| Sample ID: DS-23 A   Weld: Heat Fusio  | n         |                       |           |           |           |        |  |
| Side: A  |           |                       |           |           |           | Peel A |  |
| Peel Strength (ppi)  | 134       | 134                   | 142       | 125       | 133       | 134    |  |
| Peel Incursion (%)   | <5        | <5                    | <5        | <5        | <5        |        |  |
| Peel Locus Of Failure Code   | SIP       | SIP                   | SIP       | SIP       | SIP       |        |  |
| Peel NSF Failure Code  | FTB       | FTB                   | FTB       | FTB       | FTB       |        |  |
| Side: B  |           |                       |           |           |           | Peel B |  |
| Peel Strength (ppi)  | 132       | 128                   | 125       | 134       | 131       | 130    |  |
| Peel Incursion (%)   | <5        | <5                    | <5        | <5        | <5        |        |  |
| Peel Locus Of Failure Code   | SIP       | SIP                   | SIP       | SE        | SE        |        |  |
| Peel NSF Failure Code  | FTB       | FTB                   | FTB       | FTB       | FTB       |        |  |
| Shear  |           |                       |           |           |           | Shear  |  |
| Shear Strength (ppi)   | 156       | 159                   | 159       | 156       | 155       | 157    |  |
| Shear Elongation @ Break (%)   | >50       | >50                   | >50       | >50       | >50       |        |  |
|  |           |                       |           |           |           |        |  |
| Sample ID: DS-23 B   Weld: Heat Fusio  | n         |                       |           |           |           |        |  |
| Side: A  |           |                       |           |           |           | Peel A |  |
| Peel Strength (ppi)  | 130       | 121                   | 127       | 123       | 125       | 125    |  |
| Peel Incursion (%)   | <5        | <5                    | <5        | <5        | <5        |        |  |
| Peel Locus Of Failure Code   | SIP       | SIP                   | SIP       | SIP       | SIP       |        |  |
| Peel NSF Failure Code  | FTB       | FTB                   | FTB       | FTB       | FTB       |        |  |
| Side: B  |           |                       |           |           |           | Peel B |  |
|  |           | 122                   | 125       | 126       | 122       | 126    |  |
| Peel Strength (ppi)  | 126       | 132                   | 123       |           |           | 120    |  |
|  | 126<br><5 | 132<br><5             | <5        | <5        | <5        | 120    |  |
| Peel Incursion (%)   |           |                       |           |           |           | 120    |  |
| Peel Incursion (%)<br>Peel Locus Of Failure Code   | <5        | <5                    | <5        | <5        | <5        | 120    |  |
| Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code  | <5<br>SIP | <5<br>SIP             | <5<br>SIP | <5<br>SIP | <5<br>SIP | Shear  |  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | <5<br>SIP | <5<br>SIP             | <5<br>SIP | <5<br>SIP | <5<br>SIP |        |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|   | TEST REFLICATE NUMBER |           |           |           |           |        |  |
|---|-----------------------|-----------|-----------|-----------|-----------|--------|--|
| PARAMETER   | 1                     | 2         | 3         | 4         | 5         | MEAN   |  |
| Sample ID: DS-28   Weld: Heat Fusion  | Ì                     |           |           |           |           |        |  |
| Side: A   |                       |           |           |           |           | Peel A |  |
| Peel Strength (ppi)   | 127                   | 126       | 122       | 127       | 129       | 126    |  |
| Peel Incursion (%)  | <5                    | <5        | <5        | <5        | <5        |        |  |
| Peel Locus Of Failure Code  | SE                    | SIP       | SIP       | SIP       | SIP       |        |  |
| Peel NSF Failure Code   | FTB                   | FTB       | FTB       | FTB       | FTB       |        |  |
| Side: B   |                       |           |           |           |           | Peel B |  |
| Peel Strength (ppi)   | 129                   | 135       | 135       | 138       | 127       | 133    |  |
| Peel Incursion (%)  | <5                    | <5        | <5        | <5        | <5        |        |  |
| Peel Locus Of Failure Code  | SE                    | SIP       | SIP       | SE        | SIP       |        |  |
| Peel NSF Failure Code   | FTB                   | FTB       | FTB       | FTB       | FTB       |        |  |
| Shear   |                       |           |           |           |           | Shear  |  |
| Shear Strength (ppi)  | 156                   | 158       | 156       | 154       | 157       | 156    |  |
| Shear Elongation @ Break (%)  | >50                   | >50       | >50       | >50       | >50       |        |  |
| Sample ID: DS-29   Weld: Heat Fusion  | 1                     |           |           |           |           |        |  |
| Side: A   |                       |           |           |           |           | Peel A |  |
| Peel Strength (ppi)   | 113                   | 121       | 118       | 116       | 117       | 117    |  |
| Peel Incursion (%)  | <5                    | <5        | <5        | <5        | <5        |        |  |
| Peel Locus Of Failure Code  | SIP                   | SE        | SIP       | SE        | SIP       |        |  |
| Peel NSF Failure Code   | FTB                   | FTB       | FTB       | FTB       | FTB       |        |  |
|   |                       |           |           |           |           |        |  |
| Side: B   |                       |           |           |           |           | Peel B |  |
| <b>Side: B</b> Peel Strength (ppi)  | 114                   | 122       | 123       | 119       | 122       | Peel B |  |
| Peel Strength (ppi)   | 114<br><5             | 122<br><5 | 123<br><5 | 119<br><5 | 122<br><5 |        |  |
| Peel Strength (ppi) Peel Incursion (%)  |                       |           |           |           |           |        |  |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code                 | <5                    | <5        | <5        | <5        | <5        |        |  |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code | <5<br>SIP             | <5<br>SE  | <5<br>SIP | <5<br>SIP | <5<br>SIP |        |  |
|   | <5<br>SIP             | <5<br>SE  | <5<br>SIP | <5<br>SIP | <5<br>SIP | 120    |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|  |            |     | KEI LICAIL II | OFFIDER |     |              |
|--|------------|-----|---------------|---------|-----|--------------|
| PARAMETER  | 1          | 2   | 3             | 4       | 5   | MEAN         |
| Sample ID: DS-30   Weld: Heat Fusior               | 1          |     |               |         |     |              |
| Side: A  |            |     |               |         |     | Peel A       |
| Peel Strength (ppi)                                | 108        | 109 | 116           | 97      | 92  | 104          |
| Peel Incursion (%)                                 | <5         | <5  | <5            | <5      | <5  |              |
| Peel Locus Of Failure Code                         | SIP        | SIP | SIP           | SIP     | SIP |              |
| Peel NSF Failure Code                              | FTB        | FTB | FTB           | FTB     | FTB |              |
| Side: B  |            |     |               |         |     | Peel B       |
| Peel Strength (ppi)                                | 138        | 139 | 133           | 134     | 137 | 136          |
| Peel Incursion (%)                                 | <5         | <5  | <5            | <5      | <5  |              |
| Peel Locus Of Failure Code                         | SIP        | SIP | SIP           | SIP     | SIP |              |
| Peel NSF Failure Code                              | FTB        | FTB | FTB           | FTB     | FTB |              |
| Shear  |            |     |               |         |     | Shear        |
| Shear Strength (ppi)                               | 157        | 159 | 155           | 158     | 155 | 157          |
| Shear Elongation @ Break (%)                       | >50        | >50 | >50           | >50     | >50 |              |
| Sample ID: DS-31   Weld: Heat Fusior<br>Side: A    | 1          |     |               |         |     | Peel A       |
| Peel Strength (ppi)                                | 130        | 134 | 133           | 121     | 129 | 129          |
| Peel Incursion (%)                                 | <5         | <5  | <5            | <5      | <5  |              |
| Peel Locus Of Failure Code                         | SE         | SE  | SE            | SIP     | SE  |              |
| Peel NSF Failure Code                              | FTB        | FTB | FTB           | FTB     | FTB |              |
| Side: B  |            |     |               |         |     | Peel B       |
| Peel Strength (ppi)                                | 128        | 126 | 122           | 119     | 115 | 122          |
| Peel Incursion (%)                                 | <5         | <5  | <5            | <5      | <5  |              |
| Peel Locus Of Failure Code                         | SIP        | SIP | SIP           | SIP     | SIP |              |
|  |            | ETD | FTB           | FTB     | FTB |              |
| Peel NSF Failure Code                              | FTB        | FTB |               |         |     |              |
|  | FTB        | FIR | 115           |         |     | Shear        |
| Peel NSF Failure Code  Shear  Shear Strength (ppi) | FTB<br>155 | 160 | 156           | 157     | 157 | Shear<br>157 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29535

### **TEST REPLICATE NUMBER**

|                                      | 1201 1121 2101 1121 1101 1221 |     |     |     |     |        |  |
|--------------------------------------|-------------------------------|-----|-----|-----|-----|--------|--|
| PARAMETER                            | 1                             | 2   | 3   | 4   | 5   | MEAN   |  |
| Sample ID: DS-32   Weld: Heat Fusion |                               |     |     |     |     |        |  |
| Side: A                              |                               |     |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 112                           | 125 | 123 | 118 | 119 | 119    |  |
| Peel Incursion (%)                   | <5                            | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SE                            | SE  | SE  | SE  | SIP |        |  |
| Peel NSF Failure Code                | FTB                           | FTB | FTB | FTB | FTB |        |  |
| Side: B                              |                               |     |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 124                           | 127 | 116 | 119 | 119 | 121    |  |
| Peel Incursion (%)                   | <5                            | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                           | SIP | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                           | FTB | FTB | FTB | FTB |        |  |
| Shear                                |                               |     |     |     |     | Shear  |  |
| Shear Strength (ppi)                 | 153                           | 152 | 153 | 150 | 153 | 152    |  |
| Shear Elongation @ Break (%)         | >50                           | >50 | >50 | >50 | >50 |        |  |

Date: 2017-06-12

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29577

Material(s) Tested: (2) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29577

### **TEST REPLICATE NUMBER**

|   |            | TEST | REPLICATE N | UMBEK      |            |              |
|---|------------|------|-------------|------------|------------|--------------|
| PARAMETER   | 1          | 2    | 3           | 4          | 5          | MEAN         |
| Sample ID: DS-33   Weld: Heat Fusion  |            |      |             |            |            |              |
| Side: A   |            |      |             |            |            | Peel A       |
| Peel Strength (ppi)   | 112        | 115  | 111         | 113        | 112        | 113          |
| Peel Incursion (%)  | <5         | <5   | <5          | <5         | <5         |              |
| Peel Locus Of Failure Code  | SE         | SE   | SE          | SE         | SIP        |              |
| Peel NSF Failure Code   | FTB        | FTB  | FTB         | FTB        | FTB        |              |
| Side: B   |            |      |             |            |            | Peel B       |
| Peel Strength (ppi)   | 115        | 108  | 107         | 109        | 111        | 110          |
| Peel Incursion (%)  | <5         | <5   | <5          | <5         | <5         |              |
| Peel Locus Of Failure Code  | SE         | SIP  | SIP         | SIP        | SIP        |              |
| Peel NSF Failure Code   | FTB        | FTB  | FTB         | FTB        | FTB        |              |
| Shear   |            |      |             |            |            | Shear        |
| Shear Strength (ppi)  | 143        | 144  | 145         | 146        | 145        | 145          |
| Shear Elongation @ Break (%)  | >50        | >50  | >50         | >50        | >50        |              |
|   |            |      |             |            |            |              |
| Sample ID: DS-34   Weld: Heat Fusion  |            |      |             |            |            |              |
| Side: A   |            |      |             |            |            | Peel A       |
| Peel Strength (ppi)   | 129        | 121  | 113         | 120        | 128        | 122          |
| Peel Incursion (%)  | <5         | <5   | <5          | <5         | <5         |              |
| Peel Locus Of Failure Code  | SE         | SE   | SIP         | SE         | SE         |              |
| Peel NSF Failure Code   | FTB        | FTB  | FTB         | FTB        | FTB        |              |
| Side: B   |            |      |             |            |            | Peel B       |
| Peel Strength (ppi)   | 129        | 125  | 123         | 122        | 108        | 121          |
| Peel Incursion (%)  | <5         | <5   | <5          | <5         | <5         |              |
|   |            | SIP  | SIP         | SIP        | SIP        |              |
| Peel Locus Of Failure Code  | SIP        | SIP  |             |            |            |              |
|   | SIP<br>FTB | FTB  | FTB         | FTB        | FTB        |              |
| Peel NSF Failure Code   |            |      | FTB         | FTB        | FTB        | Shear        |
| Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) |            |      | FTB<br>158  | FTB<br>155 | FTB<br>157 | Shear<br>156 |

Date: 2017-06-13

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29617

Material(s) Tested: (12) Heat Fusion Weld Seam(s)

(1) Single Extrusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge. SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29617

### **TEST REPLICATE NUMBER**

|                                     | TEST REPLICATE NUMBER |         |         |        |         |        |  |
|-------------------------------------|-----------------------|---------|---------|--------|---------|--------|--|
| PARAMETER                           | 1                     | 2       | 3       | 4      | 5       | MEAN   |  |
| Sample ID: DS-20 A3   Weld: Heat Fu | sion                  |         |         |        |         |        |  |
| Side: A                             |                       |         |         |        |         | Peel A |  |
| Peel Strength (ppi)                 | 129                   | 131     | 128     | 134    | 134     | 131    |  |
| Peel Incursion (%)                  | <5                    | <5      | <5      | <5     | 100     |        |  |
| Peel Locus Of Failure Code          | SE                    | SE      | SE      | SIP    | AD      |        |  |
| Peel NSF Failure Code               | FTB                   | FTB     | FTB     | FTB    | NON-FTB |        |  |
| Side: B                             |                       |         |         |        |         | Peel B |  |
| Peel Strength (ppi)                 | 117                   | 74      | 113     | 112    | 43      | 92     |  |
| Peel Incursion (%)                  | 90                    | 100     | 90      | 30     | 100     |        |  |
| Peel Locus Of Failure Code          | AD-BRK                | AD      | AD-BRK  | AD-BRK | AD      |        |  |
| Peel NSF Failure Code               | FTB                   | NON-FTB | FTB     | FTB    | NON-FTB |        |  |
| Shear                               |                       |         |         |        |         | Shear  |  |
| Shear Strength (ppi)                | 157                   | 157     | 154     | 154    | 154     | 155    |  |
| Shear Elongation @ Break (%)        | >50                   | >50     | >50     | >50    | >50     |        |  |
|                                     |                       |         |         |        |         |        |  |
| Sample ID: DS-20 B3   Weld: Heat Fu | sion                  |         |         |        |         |        |  |
| Side: A                             |                       |         |         |        | _       | Peel A |  |
| Peel Strength (ppi)                 | 121                   | 112     | 114     | 114    | 115     | 115    |  |
| Peel Incursion (%)                  | 90                    | 40      | 100     | 40     | 90      |        |  |
| Peel Locus Of Failure Code          | AD-BRK                | AD-BRK  | AD      | AD-BRK | AD-BRK  |        |  |
| Peel NSF Failure Code               | FTB                   | FTB     | NON-FTB | FTB    | FTB     |        |  |
| Side: B                             |                       |         |         |        |         | Peel B |  |
| Peel Strength (ppi)                 | 130                   | 122     | 117     | 117    | 135     | 124    |  |
| Peel Incursion (%)                  | 90                    | 100     | 100     | 90     | 90      |        |  |
| Peel Locus Of Failure Code          | AD-BRK                | AD      | AD      | AD-BRK | AD-BRK  |        |  |
| Peel NSF Failure Code               | FTB                   | NON-FTB | NON-FTB | FTB    | FTB     |        |  |
| Shear                               |                       |         |         |        |         | Shear  |  |
| Shear Strength (ppi)                | 158                   | 166     | 159     | 165    | 165     | 163    |  |
| Shear Elongation @ Break (%)        | >50                   | >50     | >50     | >50    | >50     |        |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29617

### **TEST REPLICATE NUMBER**

|  | TEST NEI EIGATE NOMBER        |                                |                                     |                               |                                  |               |
|--|-------------------------------|--------------------------------|-------------------------------------|-------------------------------|----------------------------------|---------------|
| PARAMETER  | 1                             | 2                              | 3                                   | 4                             | 5                                | MEAN          |
| Sample ID: DS-21 B3   Weld: Heat Fu  | ısion                         |                                |                                     |                               |                                  |               |
| Side: A  |                               |                                |                                     |                               |                                  | Peel A        |
| Peel Strength (ppi)  | 120                           | 142                            | 128                                 | 125                           | 144                              | 132           |
| Peel Incursion (%)   | 100                           | <5                             | 100                                 | <5                            | 100                              |               |
| Peel Locus Of Failure Code   | AD                            | SIP                            | AD                                  | SIP                           | AD                               |               |
| Peel NSF Failure Code  | NON-FTB                       | FTB                            | NON-FTB                             | FTB                           | NON-FTB                          |               |
| Side: B  |                               |                                |                                     |                               |                                  | Peel B        |
| Peel Strength (ppi)  | 112                           | 80                             | 98                                  | 98                            | 123                              | 102           |
| Peel Incursion (%)   | 90                            | 90                             | 90                                  | 90                            | 90                               |               |
| Peel Locus Of Failure Code   | AD-BRK                        | AD-BRK                         | AD-BRK                              | AD-BRK                        | AD-BRK                           |               |
| Peel NSF Failure Code  | FTB                           | FTB                            | FTB                                 | FTB                           | FTB                              |               |
| Shear  |                               |                                |                                     |                               |                                  | Shear         |
| Shear Strength (ppi)   | 161                           | 164                            | 165                                 | 165                           | 164                              | 164           |
| Shear Elongation @ Break (%)   | >50                           | >50                            | >50                                 | >50                           | >50                              |               |
| Sample ID: DS-35   Weld: Heat Fusio<br>Side: A   | 'n                            |                                |                                     |                               |                                  | Peel A        |
| Peel Strength (ppi)  | 141                           | 139                            | 140                                 | 143                           | 128                              |               |
|  |                               |                                |                                     |                               |                                  | 138           |
| Peel Incursion (%)   | <5                            | <5                             | <5                                  | <5                            | <5                               | 138           |
| ` ,  | <5<br>SE                      | <5<br>SIP                      |                                     | <5<br>SE                      | <5<br>SIP                        | 138           |
| Peel Locus Of Failure Code   |                               |                                | <5                                  |                               |                                  | 138           |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code  | SE                            | SIP                            | <5<br>SE                            | SE                            | SIP                              | 138 Peel B    |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B   | SE                            | SIP                            | <5<br>SE                            | SE                            | SIP                              |               |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)  | SE<br>FTB                     | SIP<br>FTB                     | <5<br>SE<br>FTB                     | SE<br>FTB                     | SIP<br>FTB                       | Peel B        |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)  | SE<br>FTB                     | SIP<br>FTB                     | <5<br>SE<br>FTB                     | SE<br>FTB                     | SIP<br>FTB                       | Peel B        |
| Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code   | SE<br>FTB<br>123<br><5        | SIP<br>FTB<br>123<br><5        | <5<br>SE<br>FTB<br>121<br><5        | SE<br>FTB<br>124<br><5        | SIP<br>FTB<br>119 [              | Peel B        |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code   | SE<br>FTB<br>123<br><5<br>SIP | SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SE<br>FTB<br>121<br><5<br>SIP | SE<br>FTB<br>124<br><5<br>SIP | SIP<br>FTB<br>119 (<br><5<br>SIP | Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | SE<br>FTB<br>123<br><5<br>SIP | SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SE<br>FTB<br>121<br><5<br>SIP | SE<br>FTB<br>124<br><5<br>SIP | SIP<br>FTB<br>119 (<br><5<br>SIP | Peel B<br>122 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29617

### **TEST REPLICATE NUMBER**

|                                      | TEST REPLICATE NUMBER |     |     |     |     |        |
|--------------------------------------|-----------------------|-----|-----|-----|-----|--------|
| PARAMETER                            | 1                     | 2   | 3   | 4   | 5   | MEAN   |
| Sample ID: DS-36   Weld: Heat Fusion | )                     |     |     |     |     |        |
| Side: A                              |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                  | 121                   | 118 | 120 | 116 | 113 | 118    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                              |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                  | 116                   | 121 | 118 | 117 | 122 | 119    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Shear                                |                       |     |     |     |     | Shear  |
| Shear Strength (ppi)                 | 161                   | 162 | 160 | 160 | 161 | 161    |
| Shear Elongation @ Break (%)         | >50                   | >50 | >50 | >50 | >50 |        |
|                                      |                       |     |     |     |     |        |
| Sample ID: DS-37   Weld: Heat Fusion | 1                     |     |     |     |     |        |
| Side: A                              |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                  | 119                   | 112 | 114 | 125 | 131 | 120    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SE  | SE  |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                              |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                  | 127                   | 121 | 112 | 118 | 117 | 119    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Shear                                |                       |     |     |     |     | Shear  |
|                                      |                       |     |     |     |     |        |
| Shear Strength (ppi)                 | 160                   | 160 | 158 | 155 | 155 | 158    |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29617

### **TEST REPLICATE NUMBER**

|                                      | TEST REPLICATE NUMBER |     |     |     |     |        |
|--------------------------------------|-----------------------|-----|-----|-----|-----|--------|
| PARAMETER                            | 1                     | 2   | 3   | 4   | 5   | MEAN   |
| Sample ID: DS-38   Weld: Heat Fusion | 1                     |     |     |     |     |        |
| Side: A                              |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                  | 130                   | 131 | 128 | 127 | 129 | 129    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SE  | SE  | SIP | SE  |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                              |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                  | 128                   | 132 | 127 | 131 | 127 | 129    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Shear                                |                       |     |     |     |     | Shear  |
| Shear Strength (ppi)                 | 162                   | 164 | 163 | 166 | 166 | 164    |
| Shear Elongation @ Break (%)         | >50                   | >50 | >50 | >50 | >50 |        |
|                                      |                       |     |     |     |     |        |
| Sample ID: DS-39   Weld: Heat Fusion | 1                     |     |     |     |     |        |
| Side: A                              |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                  | 123                   | 122 | 129 | 117 | 119 | 122    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SE  | SIP | SIP |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                              |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                  | 127                   | 128 | 119 | 121 | 133 | 126    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SE                    | SE  | SIP | SIP | SE  |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Shear                                |                       |     |     |     |     | Shear  |
|                                      |                       |     |     |     |     |        |
| Shear Strength (ppi)                 | 165                   | 163 | 162 | 163 | 165 | 164    |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29617

### **TEST REPLICATE NUMBER**

|                                      | TEST REPLICATE NUMBER |     |     |     |     |        |
|--------------------------------------|-----------------------|-----|-----|-----|-----|--------|
| PARAMETER                            | 1                     | 2   | 3   | 4   | 5   | MEAN   |
| Sample ID: DS-41   Weld: Heat Fusion | Ì                     |     |     |     |     |        |
| Side: A                              |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                  | 127                   | 131 | 127 | 127 | 133 | 129    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SE  | SE  | SE  |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                              |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                  | 122                   | 112 | 121 | 119 | 120 | 119    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SE  |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Shear                                |                       |     |     |     |     | Shear  |
| Shear Strength (ppi)                 | 149                   | 154 | 153 | 151 | 152 | 152    |
| Shear Elongation @ Break (%)         | >50                   | >50 | >50 | >50 | >50 | L      |
|                                      |                       |     |     |     |     |        |
| Sample ID: DS-42   Weld: Heat Fusion | 1                     |     |     |     |     |        |
| Side: A                              |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                  | 119                   | 119 | 113 | 122 | 114 | 117    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                              |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                  | 115                   | 116 | 123 | 127 | 128 | 122    |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |
| Shear                                |                       |     |     |     |     | Shear  |
|                                      |                       |     |     |     |     |        |
| Shear Strength (ppi)                 | 154                   | 156 | 154 | 152 | 152 | 154    |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29617

### **TEST REPLICATE NUMBER**

| PARAMETER   | 1                                    | 2                                    | 3                                    | 4                                    | 5                                    | MEAN          |
|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Sample ID: DS-43   Weld: Heat Fusion  |                                      |                                      |                                      |                                      |                                      |               |
| Side: A   |                                      |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)   | 140                                  | 138                                  | 133                                  | 144                                  | 135                                  | 138           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SE                                   | SIP                                  | SIP                                  | SE                                   |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B   |                                      |                                      |                                      |                                      |                                      | Peel B        |
| Peel Strength (ppi)   | 126                                  | 137                                  | 134                                  | 140                                  | 127                                  | 133           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Shear   |                                      |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)  | 163                                  | 164                                  | 164                                  | 165                                  | 165                                  | 164           |
| Shear Elongation @ Break (%)  | >50                                  | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-44   Weld: Heat Fusion<br>Side: A   | 1                                    |                                      |                                      |                                      |                                      | Peel A        |
|   |                                      |                                      |                                      |                                      |                                      |               |
| Peel Strength (ppi)   | 128                                  | 125                                  | 124                                  | 127                                  | 127                                  | 126           |
|   | 128<br><5                            | 125<br><5                            | 124<br><5                            | 127<br><5                            | 127<br><5                            | 126           |
| Peel Incursion (%)  |                                      |                                      |                                      |                                      |                                      | 126           |
| Peel Incursion (%)<br>Peel Locus Of Failure Code  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   | 126           |
| Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code   | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 126<br>Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B   | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%)  | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code   | <5<br>SIP<br>FTB<br>119<br><5        | <5<br>SIP<br>FTB<br>115<br><5        | <5<br>SIP<br>FTB<br>118<br><5        | <5<br>SIP<br>FTB<br>122<br><5        | <5<br>SIP<br>FTB<br>119<br><5        | Peel B        |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code   | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | <5<br>SIP<br>FTB<br>115<br><5<br>SIP | <5<br>SIP<br>FTB<br>118<br><5<br>SIP | <5<br>SIP<br>FTB<br>122<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | Peel B        |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | <5<br>SIP<br>FTB<br>115<br><5<br>SIP | <5<br>SIP<br>FTB<br>118<br><5<br>SIP | <5<br>SIP<br>FTB<br>122<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | Peel B<br>119 |

### DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS - SINGLE TRACK TRI Client: Feezor Engineering. Inc.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29617

### **TEST REPLICATE NUMBER**

| PARAMETER                             | 1     | 2   | 3   | 4   | 5   | MEAN  |
|---------------------------------------|-------|-----|-----|-----|-----|-------|
| Sample ID: DS-40   Weld: Single Extru | ision |     |     |     |     |       |
| Side: Peel                            |       |     |     |     |     | Peel  |
| Peel Strength (ppi)                   | 136   | 140 | 135 | 117 | 129 | 131   |
| Peel Incursion (%)                    | <5    | <5  | <5  | <5  | <5  |       |
| Peel Locus Of Failure Code            | SE    | SE  | SE  | SE  | SE  |       |
| Peel NSF Failure Code                 | FTB   | FTB | FTB | FTB | FTB |       |
| Shear                                 |       |     |     |     |     | Shear |
| Shear Strength (ppi)                  | 170   | 166 | 162 | 145 | 122 | 153   |
| Shear Elongation @ Break (%)          | >50   | 28  | 25  | 23  | 22  |       |
|                                       |       |     |     |     |     |       |

Date: 2017-06-15

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29693

Material(s) Tested: (7) Heat Fusion Weld Seam(s)

(1) Single Extrusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge. SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29693

### **TEST REPLICATE NUMBER**

| PARAMETER  | 1  | 2                                       | 3                                      | 4                                       | 5                            | MEAN                |
|--|--|---|--|---|------------------------------|---------------------|
| Sample ID: DS-20 A4   Weld: Heat Fu  | sion   |   |  |   |                              |                     |
| Side: A  |  |   |  |   |                              | Peel A              |
| Peel Strength (ppi)  | 123  | 117                                     | 126                                    | 120                                     | 123                          | 122                 |
| Peel Incursion (%)   | 100  | 100                                     | 20                                     | 100                                     | <5                           |                     |
| Peel Locus Of Failure Code   | AD   | AD                                      | AD-BRK                                 | AD                                      | SIP                          |                     |
| Peel NSF Failure Code  | NON-FTB  | NON-FTB                                 | FTB                                    | NON-FTB                                 | FTB                          |                     |
| Side: B  |  |   |  |   |                              | Peel B              |
| Peel Strength (ppi)  | 54   | 117                                     | 107                                    | 116                                     | 111                          | 101                 |
| Peel Incursion (%)   | 100  | 100                                     | <5                                     | 100                                     | <5                           |                     |
| Peel Locus Of Failure Code   | AD   | AD                                      | SIP                                    | AD                                      | SIP                          |                     |
| Peel NSF Failure Code  | NON-FTB  | NON-FTB                                 | FTB                                    | NON-FTB                                 | FTB                          |                     |
| Shear  |  |   |  |   |                              | Shear               |
| Shear Strength (ppi)   | 157  | 157                                     | 157                                    | 157                                     | 155                          | 157                 |
| Shear Elongation @ Break (%)   | >50  | >50                                     | >50                                    | >50                                     | >50                          |                     |
|  |  |   |  |   |                              |                     |
| Sample ID: DC 20 B4   Wold: Heat Eu  | clan   |   |  |   |                              |                     |
| · · · · · · · · · · · · · · · · · · ·  | sion   |   |  |   |                              | Peel A              |
| Side: A  | sion 109                                       | 82                                      | 109                                    | 85                                      | 63                           | Peel A              |
| Side: A Peel Strength (ppi)  | 109  | 82<br>90                                | 109<br>90                              | 85<br>90                                | 63 [<br>90                   |                     |
| Side: A Peel Strength (ppi) Peel Incursion (%)   |  |   |  |   | L                            |                     |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | 109<br>90                                      | 90                                      | 90                                     | 90                                      | 90                           |                     |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  | 109<br>90<br>AD-BRK                            | 90<br>AD-BRK                            | 90<br>AD-BRK                           | 90<br>AD-BRK                            | 90<br>AD-BRK                 |                     |
| Sample ID: DS-20 B4   Weld: Heat Fu<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)                     | 109<br>90<br>AD-BRK                            | 90<br>AD-BRK                            | 90<br>AD-BRK                           | 90<br>AD-BRK                            | 90<br>AD-BRK                 | 90                  |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | 109<br>90<br>AD-BRK<br>FTB                     | 90<br>AD-BRK<br>FTB                     | 90<br>AD-BRK<br>FTB                    | 90<br>AD-BRK<br>FTB                     | 90<br>AD-BRK<br>FTB          | 90<br>Peel B        |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)   | 109<br>90<br>AD-BRK<br>FTB<br>106              | 90<br>AD-BRK<br>FTB<br>119              | 90<br>AD-BRK<br>FTB<br>142             | 90<br>AD-BRK<br>FTB<br>117              | 90<br>AD-BRK<br>FTB          | 90<br>Peel B        |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | 109<br>90<br>AD-BRK<br>FTB<br>106<br>100       | 90<br>AD-BRK<br>FTB<br>119<br>100       | 90<br>AD-BRK<br>FTB<br>142<br><5       | 90<br>AD-BRK<br>FTB<br>117<br>100       | 90<br>AD-BRK<br>FTB<br>132 [ | 90<br>Peel B        |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code | 109<br>90<br>AD-BRK<br>FTB<br>106<br>100<br>AD | 90<br>AD-BRK<br>FTB<br>119<br>100<br>AD | 90<br>AD-BRK<br>FTB<br>142<br><5<br>SE | 90<br>AD-BRK<br>FTB<br>117<br>100<br>AD | 90 AD-BRK FTB  132 60 AD-BRK | 90<br>Peel B        |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code                        | 109<br>90<br>AD-BRK<br>FTB<br>106<br>100<br>AD | 90<br>AD-BRK<br>FTB<br>119<br>100<br>AD | 90<br>AD-BRK<br>FTB<br>142<br><5<br>SE | 90<br>AD-BRK<br>FTB<br>117<br>100<br>AD | 90 AD-BRK FTB  132 60 AD-BRK | 90<br>Peel B<br>123 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29693

### **TEST REPLICATE NUMBER**

|                                      | IESI REPLICATE NUMBER |     |     |     |     |        |  |
|--------------------------------------|-----------------------|-----|-----|-----|-----|--------|--|
| PARAMETER                            | 1                     | 2   | 3   | 4   | 5   | MEAN   |  |
| Sample ID: DS-21 B4   Weld: Heat Fus | sion                  |     |     |     |     |        |  |
| Side: A                              |                       |     |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 132                   | 130 | 137 | 133 | 136 | 134    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SE                    | SIP | SE  | SE  | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Side: B                              |                       |     |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 107                   | 117 | 123 | 129 | 103 | 116    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Shear                                |                       |     |     |     |     | Shear  |  |
| Shear Strength (ppi)                 | 161                   | 165 | 165 | 165 | 160 | 163    |  |
| Shear Elongation @ Break (%)         | >50                   | >50 | >50 | >50 | >50 |        |  |
|                                      |                       |     |     |     |     |        |  |
| Sample ID: DS-45   Weld: Heat Fusion | 1                     |     |     |     |     |        |  |
| Side: A                              |                       |     |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 115                   | 123 | 108 | 111 | 109 | 113    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SE                    | SE  | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Side: B                              |                       |     |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 119                   | 115 | 125 | 118 | 109 | 117    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  | •      |  |
| Peel Locus Of Failure Code           | SE                    | SE  | SE  | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Shear                                |                       |     |     |     |     | Shear  |  |
| Share Charactle (c. c.)              | 166                   | 167 | 166 | 165 | 168 | 166    |  |
| Shear Strength (ppi)                 | 100                   |     |     |     |     |        |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29693

### **TEST REPLICATE NUMBER**

|                                      | TEST REPLICATE NUMBER |      |     |     |     |        |  |
|--------------------------------------|-----------------------|------|-----|-----|-----|--------|--|
| PARAMETER                            | 1                     | 2    | 3   | 4   | 5   | MEAN   |  |
| Sample ID: DS-46   Weld: Heat Fusion |                       |      |     |     |     |        |  |
| Side: A                              |                       |      |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 143                   | 152  | 151 | 146 | 149 | 148    |  |
| Peel Incursion (%)                   | <5                    | <5   | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SE                    | SE   | SE  | SE  | SE  |        |  |
| Peel NSF Failure Code                | FTB                   | FTB  | FTB | FTB | FTB |        |  |
| Side: B                              |                       |      |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 153                   | 152  | 151 | 159 | 152 | 153    |  |
| Peel Incursion (%)                   | <5                    | <5   | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SE   | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB  | FTB | FTB | FTB |        |  |
| Shear                                |                       |      |     |     |     | Shear  |  |
| Shear Strength (ppi)                 | 179                   | 179  | 178 | 176 | 177 | 178    |  |
| Shear Elongation @ Break (%)         | >50                   | >50  | >50 | >50 | >50 |        |  |
|                                      |                       |      |     |     |     |        |  |
| Sample ID: DS-48   Weld: Heat Fusion | 1                     |      |     |     |     |        |  |
| Side: A                              |                       |      |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 131                   | 131  | 126 | 134 | 130 | 130    |  |
| Peel Incursion (%)                   | <5                    | <5   | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP  | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB  | FTB | FTB | FTB |        |  |
| Side: B                              |                       |      |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 101                   | 123  | 110 | 98  | 108 | 108    |  |
| Peel Incursion (%)                   | <5                    | <5   | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP  | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB  | FTB | FTB | FTB |        |  |
| Shear                                |                       |      |     |     |     | Shear  |  |
|                                      |                       | 1.05 | 165 | 166 | 166 | 165    |  |
| Shear Strength (ppi)                 | 161                   | 165  | 103 | 100 | 100 | 103    |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29693

### **TEST REPLICATE NUMBER**

|                                      | TEST REFLICATE NUMBER |     |     |     |     |        |  |
|--------------------------------------|-----------------------|-----|-----|-----|-----|--------|--|
| PARAMETER                            | 1                     | 2   | 3   | 4   | 5   | MEAN   |  |
| Sample ID: DS-49   Weld: Heat Fusion |                       |     |     |     |     |        |  |
| Side: A                              |                       |     |     |     |     | Peel A |  |
| Peel Strength (ppi)                  | 125                   | 129 | 129 | 131 | 132 | 129    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Side: B                              |                       |     |     |     |     | Peel B |  |
| Peel Strength (ppi)                  | 125                   | 131 | 125 | 151 | 134 | 133    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5  | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB | FTB | FTB |        |  |
| Shear                                |                       |     |     |     |     | Shear  |  |
| Shear Strength (ppi)                 | 176                   | 178 | 176 | 174 | 176 | 176    |  |
| Shear Elongation @ Break (%)         | >50                   | >50 | >50 | >50 | >50 |        |  |

### DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS - SINGLE TRACK TRI Client: Feezor Engineering. Inc.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29693

### **TEST REPLICATE NUMBER**

| PARAMETER                                 | 1      | 2       | 3      | 4      | 5      | MEAN  |
|---|--------|---------|--------|--------|--------|-------|
| Sample ID: DS-47   Weld: Single Extrusion |        |         |        |        |        |       |
| Side: Peel                                |        |         |        |        |        | Peel  |
| Peel Strength (ppi)                       | 87     | 79      | 76     | 86     | 83     | 82    |
| Peel Incursion (%)                        | 20     | 100     | 30     | 20     | 90     |       |
| Peel Locus Of Failure Code                | AD-BRK | AD      | AD-BRK | AD-BRK | AD-BRK |       |
| Peel NSF Failure Code                     | FTB    | NON-FTB | FTB    | FTB    | FTB    |       |
| Shear                                     |        |         |        |        |        | Shear |
| Shear Strength (ppi)                      | 167    | 164     | 168    | 168    | 165    | 166   |
| Shear Elongation @ Break (%)              | >50    | >50     | >50    | >50    | >50    |       |

Date: 2017-06-19

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29799

Material(s) Tested: (8) Heat Fusion Weld Seam(s)

(2) Single Extrusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge. SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29799

### **TEST REPLICATE NUMBER**

|                                      | TEST REPLICATE NUMBER |     |         |     |     |        |  |
|--------------------------------------|-----------------------|-----|---------|-----|-----|--------|--|
| PARAMETER                            | 1                     | 2   | 3       | 4   | 5   | MEAN   |  |
| Sample ID: DS-20 A6   Weld: Heat Fus | sion                  |     |         |     |     |        |  |
| Side: A                              |                       |     |         |     |     | Peel A |  |
| Peel Strength (ppi)                  | 120                   | 130 | 98      | 116 | 120 | 117    |  |
| Peel Incursion (%)                   | <5                    | <5  | 100     | <5  | <5  | l      |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | AD      | SE  | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | NON-FTB | FTB | FTB |        |  |
| Side: B                              |                       |     |         |     |     | Peel B |  |
| Peel Strength (ppi)                  | 113                   | 114 | 114     | 112 | 115 | 114    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5      | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP     | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB     | FTB | FTB |        |  |
| Shear                                |                       |     |         |     |     | Shear  |  |
| Shear Strength (ppi)                 | 155                   | 156 | 153     | 154 | 154 | 154    |  |
| Shear Elongation @ Break (%)         | >50                   | >50 | >50     | >50 | >50 |        |  |
|                                      |                       |     |         |     |     |        |  |
| Sample ID: DS-50   Weld: Heat Fusion | 1                     |     |         |     |     |        |  |
| Side: A                              |                       |     |         |     |     | Peel A |  |
| Peel Strength (ppi)                  | 126                   | 99  | 141     | 142 | 132 | 128    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5      | <5  | <5  |        |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP     | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB     | FTB | FTB |        |  |
| Side: B                              |                       |     |         |     |     | Peel B |  |
| Peel Strength (ppi)                  | 132                   | 142 | 134     | 138 | 138 | 137    |  |
| Peel Incursion (%)                   | <5                    | <5  | <5      | <5  | <5  | •      |  |
| Peel Locus Of Failure Code           | SIP                   | SIP | SIP     | SIP | SIP |        |  |
| Peel NSF Failure Code                | FTB                   | FTB | FTB     | FTB | FTB |        |  |
| Shear                                |                       |     |         |     |     | Shear  |  |
|                                      | 150                   | 164 | 164     | 167 | 163 | 163    |  |
| Shear Strength (ppi)                 | 158                   | 104 | 104     | 107 | 103 | -03    |  |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29799

### **TEST REPLICATE NUMBER**

| PARAMETER  | 1                                    | 2                                    | 3                                    | 4                                    | 5                                    | MEAN          |
|--|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Sample ID: DS-51   Weld: Heat Fusion   |                                      |                                      |                                      |                                      |                                      |               |
| Side: A  |                                      |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)  | 134                                  | 130                                  | 129                                  | 144                                  | 132                                  | 134           |
| Peel Incursion (%)   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code   | SE                                   | SIP                                  | SIP                                  | SE                                   | SIP                                  |               |
| Peel NSF Failure Code  | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B  |                                      |                                      |                                      |                                      |                                      | Peel B        |
| Peel Strength (ppi)  | 134                                  | 131                                  | 131                                  | 133                                  | 131                                  | 132           |
| Peel Incursion (%)   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code   | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code  | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Shear  |                                      |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)   | 161                                  | 162                                  | 160                                  | 161                                  | 159                                  | 161           |
| Shear Elongation @ Break (%)   | >50                                  | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-53   Weld: Heat Fusion   |                                      |                                      |                                      |                                      |                                      |               |
| Side: A  |                                      |                                      |                                      |                                      |                                      | DIA           |
|  |                                      |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)  | 111                                  | 120                                  | 110                                  | 119                                  | 117                                  | 115           |
|  | 111<br><5                            | 120<br><5                            | 110<br><5                            | 119<br><5                            | 117<br><5                            |               |
| Peel Incursion (%)   |                                      |                                      |                                      |                                      |                                      |               |
| Peel Incursion (%)<br>Peel Locus Of Failure Code   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code  | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 115           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 115<br>Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 115<br>Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | <5<br>SIP<br>FTB<br>123<br><5        | <5<br>SIP<br>FTB<br>121<br><5        | <5<br>SIP<br>FTB<br>128<br><5        | <5<br>SIP<br>FTB<br>129<br><5        | <5<br>SIP<br>FTB<br>119<br><5        | 115<br>Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  | <5<br>SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SIP<br>FTB<br>121<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>129<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | 115<br>Peel B |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | <5<br>SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SIP<br>FTB<br>121<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>129<br><5<br>SIP | <5<br>SIP<br>FTB<br>119<br><5<br>SIP | Peel B<br>124 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29799

### **TEST REPLICATE NUMBER**

| PARAMETER   | 1                                    | 2                                    | 3  | 4                                    | 5                                    | MEAN          |
|---|--------------------------------------|--------------------------------------|--|--------------------------------------|--------------------------------------|---------------|
| Sample ID: DS-54   Weld: Heat Fusion  |                                      |                                      |  |                                      |                                      |               |
| Side: A   |                                      |                                      |  |                                      |                                      | Peel A        |
| Peel Strength (ppi)   | 126                                  | 122                                  | 130                                      | 122                                  | 114                                  | 123           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                       | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                      | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                      | FTB                                  | FTB                                  |               |
| Side: B   |                                      |                                      |  |                                      |                                      | Peel B        |
| Peel Strength (ppi)   | 118                                  | 125                                  | 108                                      | 116                                  | 120                                  | 117           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                       | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                      | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                      | FTB                                  | FTB                                  |               |
| Shear   |                                      |                                      |  |                                      |                                      | Shear         |
| Shear Strength (ppi)  | 160                                  | 161                                  | 160                                      | 158                                  | 157                                  | 159           |
| Shear Elongation @ Break (%)  | >50                                  | >50                                  | >50                                      | >50                                  | >50                                  |               |
| Sample ID: DS-55   Weld: Heat Fusion<br>Side: A   | <u> </u>                             |                                      |  |                                      |                                      |               |
|   |                                      |                                      |  |                                      |                                      | Peel A        |
| Peel Strength (ppi)   | 124                                  | 123                                  | 122                                      | 132                                  | 133                                  | Peel A<br>127 |
|   | 124<br><5                            | 123<br><5                            | 122<br>100                               | 132<br><5                            | 133<br><5                            |               |
| Peel Incursion (%)  |                                      |                                      |  |                                      |                                      |               |
| Peel Incursion (%)<br>Peel Locus Of Failure Code  | <5                                   | <5                                   | 100                                      | <5                                   | <5                                   |               |
| Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code   | <5<br>SIP                            | <5<br>SIP                            | 100<br>AD                                | <5<br>SIP                            | <5<br>SIP                            |               |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SIP                            | <5<br>SIP                            | 100<br>AD                                | <5<br>SIP                            | <5<br>SIP                            | 127           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 100<br>AD<br>NON-FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 127           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 100<br>AD<br>NON-FTB<br>116              | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 127           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code                         | <5<br>SIP<br>FTB<br>136<br><5        | <5<br>SIP<br>FTB<br>125<br><5        | 100<br>AD<br>NON-FTB<br>116<br><5        | <5<br>SIP<br>FTB<br>128<br><5        | <5<br>SIP<br>FTB<br>116<br><5        | 127           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code | <5<br>SIP<br>FTB<br>136<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | 100<br>AD<br>NON-FTB<br>116<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>116<br><5<br>SIP | 127           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)  | <5<br>SIP<br>FTB<br>136<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | 100<br>AD<br>NON-FTB<br>116<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>116<br><5<br>SIP | Peel B        |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29799

### **TEST REPLICATE NUMBER**

|                                     | TEST REPLICATE NUMBER |         |         |         |               |        |
|-------------------------------------|-----------------------|---------|---------|---------|---------------|--------|
| PARAMETER                           | 1                     | 2       | 3       | 4       | 5             | MEAN   |
| Sample ID: DS-56   Weld: Heat Fusio | n                     |         |         |         |               |        |
| Side: A                             |                       |         |         |         |               | Peel A |
| Peel Strength (ppi)                 | 118                   | 103     | 107     | 124     | 105           | 111    |
| Peel Incursion (%)                  | <5                    | <5      | <5      | <5      | <5            |        |
| Peel Locus Of Failure Code          | SE                    | SIP     | SIP     | SIP     | SIP           |        |
| Peel NSF Failure Code               | FTB                   | FTB     | FTB     | FTB     | FTB           |        |
| Side: B                             |                       |         |         |         |               | Peel B |
| Peel Strength (ppi)                 | 110                   | 112     | 106     | 105     | 115           | 110    |
| Peel Incursion (%)                  | <5                    | <5      | <5      | <5      | <b>&lt;</b> 5 |        |
| Peel Locus Of Failure Code          | SIP                   | SIP     | SIP     | SIP     | SIP           |        |
| Peel NSF Failure Code               | FTB                   | FTB     | FTB     | FTB     | FTB           |        |
| Shear                               |                       |         |         |         |               | Shear  |
| Shear Strength (ppi)                | 149                   | 154     | 152     | 151     | 152           | 152    |
| Shear Elongation @ Break (%)        | >50                   | >50     | >50     | >50     | >50           |        |
|                                     |                       |         |         |         |               |        |
| Sample ID: DS-57   Weld: Heat Fusio | n                     |         |         |         |               |        |
| Side: A                             |                       |         |         |         | _             | Peel A |
| Peel Strength (ppi)                 | 130                   | 132     | 131     | 136     | 119           | 130    |
| Peel Incursion (%)                  | 100                   | 100     | <5      | 100     | 100           |        |
| Peel Locus Of Failure Code          | AD                    | AD      | SIP     | AD      | AD            |        |
| Peel NSF Failure Code               | NON-FTB               | NON-FTB | FTB     | NON-FTB | NON-FTB       |        |
| Side: B                             |                       |         |         |         | _             | Peel B |
| Peel Strength (ppi)                 | 67                    | 59      | 80      | 75      | 71            | 70     |
| Peel Incursion (%)                  | <5                    | 100     | 100     | 100     | 100           |        |
| Peel Locus Of Failure Code          | SIP                   | AD      | AD      | AD      | AD            |        |
| Peel NSF Failure Code               | FTB                   | NON-FTB | NON-FTB | NON-FTB | NON-FTB       |        |
| Shear                               |                       |         |         |         |               | Shear  |
| Shear Strength (ppi)                | 152                   | 158     | 148     | 154     | 148           | 152    |
| Shear Elongation @ Break (%)        | >50                   | >50     | >50     | >50     | >50           |        |

### TRI Client: Feezor Engineering. Inc.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29799

### **TEST REPLICATE NUMBER**

|                                       | TEST REPLICATE NUMBER |         |     |     |       |       |  |
|---------------------------------------|-----------------------|---------|-----|-----|-------|-------|--|
| PARAMETER                             | 1                     | 2       | 3   | 4   | 5     | MEAN  |  |
| Sample ID: DS-47 B   Weld: Single Ext | trusion               |         |     |     |       |       |  |
| Side: Peel                            |                       |         |     |     |       | Peel  |  |
| Peel Strength (ppi)                   | 124                   | 129     | 122 | 134 | 150   | 132   |  |
| Peel Incursion (%)                    | <5                    | <5      | <5  | <5  | <5    |       |  |
| Peel Locus Of Failure Code            | SIP                   | SIP     | SIP | SIP | SIP   |       |  |
| Peel NSF Failure Code                 | FTB                   | FTB     | FTB | FTB | FTB   |       |  |
| Shear                                 |                       |         |     |     |       | Shear |  |
| Shear Strength (ppi)                  | 167                   | 171     | 172 | 171 | 169   | 170   |  |
| Shear Elongation @ Break (%)          | >50                   | >50     | >50 | >50 | >50   |       |  |
| Sample ID: DS-52   Weld: Single Extru | ısion                 |         |     |     |       |       |  |
| Side: Peel                            |                       |         |     |     |       | Peel  |  |
| Peel Strength (ppi)                   | 127                   | 81      | 142 | 119 | 89    | 112   |  |
| Peel Incursion (%)                    | <5                    | 100     | <5  | <5  | <5    |       |  |
| Peel Locus Of Failure Code            | SIP                   | AD      | SIP | SIP | SIP   |       |  |
| Peel NSF Failure Code                 | FTB                   | NON-FTB | FTB | FTB | FTB   |       |  |
| Shear                                 |                       |         |     |     |       | Shear |  |
| Shear Strength (ppi)                  | 161                   | 163     | 159 | 160 | 143   | 157   |  |
| Shear Elongation @ Break (%)          | >50                   | >50     | >50 | >50 | 20.87 |       |  |

Date: 2017-06-21

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29875

Material(s) Tested: (4) Heat Fusion Weld Seam(s)

(1) Single Extrusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge. SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29875

### **TEST REPLICATE NUMBER**

| PARAMETER  | 1                              | 2                              | 3                              | 4                              | 5                              | MEAN   |
|--|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------|
| Sample ID: DS-20 A7   Weld: Heat Fus   | ion                            |                                |                                |                                |                                |        |
| Side: A  |                                |                                |                                |                                |                                | Peel A |
| Peel Strength (ppi)  | 140                            | 138                            | 140                            | 109                            | 148                            | 135    |
| Peel Incursion (%)   | <5                             | <5                             | <5                             | <5                             | <5                             | l .    |
| Peel Locus Of Failure Code   | SIP                            | SIP                            | SIP                            | SIP                            | SIP                            |        |
| Peel NSF Failure Code  | FTB                            | FTB                            | FTB                            | FTB                            | FTB                            |        |
| Side: B  |                                |                                |                                |                                |                                | Peel B |
| Peel Strength (ppi)  | 141                            | 139                            | 132                            | 139                            | 149                            | 140    |
| Peel Incursion (%)   | <5                             | <5                             | <5                             | <5                             | <5                             |        |
| Peel Locus Of Failure Code   | SE                             | SIP                            | SIP                            | SIP                            | SIP                            |        |
| Peel NSF Failure Code  | FTB                            | FTB                            | FTB                            | FTB                            | FTB                            |        |
| Shear  |                                |                                |                                |                                |                                | Shear  |
| Shear Strength (ppi)   | 165                            | 166                            | 163                            | 161                            | 163                            | 164    |
| Shear Elongation @ Break (%)   | >50                            | >50                            | >50                            | >50                            | >50                            |        |
| Sample ID: DS-55 B   Weld: Heat Fusi<br>Side: A  | on                             |                                |                                |                                |                                | Peel A |
| Peel Strength (ppi)  | 145                            | 130                            | 140                            | 137                            | 135                            |        |
| •  |                                |                                |                                |                                |                                | 137    |
| Peer incursion (%)   | <5                             | <5                             | <5                             | <5                             | <5                             | 137    |
| , ,  | <5<br>SIP                      | <5<br>SIP                      | <5<br>SIP                      | <5<br>SIP                      | <5<br>SIP                      | 137    |
| Peel Locus Of Failure Code   |                                |                                |                                |                                |                                | 137    |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code  | SIP                            | SIP                            | SIP                            | SIP                            | SIP                            | Peel B |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B   | SIP                            | SIP                            | SIP                            | SIP                            | SIP                            |        |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)  | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | Peel B |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)  | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | Peel B |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code   | SIP<br>FTB<br>140<br><5        | SIP<br>FTB<br>138<br><5        | SIP<br>FTB<br>140<br><5        | SIP<br>FTB<br>146<br><5        | SIP<br>FTB<br>140<br><5        | Peel B |
| Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code   | SIP<br>FTB<br>140<br><5<br>SIP | SIP<br>FTB<br>138<br><5<br>SIP | SIP<br>FTB<br>140<br><5<br>SIP | SIP<br>FTB<br>146<br><5<br>SIP | SIP<br>FTB<br>140<br><5<br>SIP | Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | SIP<br>FTB<br>140<br><5<br>SIP | SIP<br>FTB<br>138<br><5<br>SIP | SIP<br>FTB<br>140<br><5<br>SIP | SIP<br>FTB<br>146<br><5<br>SIP | SIP<br>FTB<br>140<br><5<br>SIP | Peel B |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29875

### **TEST REPLICATE NUMBER**

|  |                   | TEST                           |                                |                                |                                |               |
|--|-------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|---------------|
| PARAMETER  | 1                 | 2                              | 3                              | 4                              | 5                              | MEAN          |
| Sample ID: DS-57 B   Weld: Heat Fusi   | on                |                                |                                |                                |                                |               |
| Side: A  |                   |                                |                                |                                |                                | Peel A        |
| Peel Strength (ppi)  | 138               | 138                            | 138                            | 143                            | 137                            | 139           |
| Peel Incursion (%)   | <5                | <5                             | <5                             | <5                             | <5                             |               |
| Peel Locus Of Failure Code   | SIP               | SIP                            | SIP                            | SIP                            | SIP                            |               |
| Peel NSF Failure Code  | FTB               | FTB                            | FTB                            | FTB                            | FTB                            |               |
| Side: B  |                   |                                |                                |                                |                                | Peel B        |
| Peel Strength (ppi)  | 144               | 140                            | 140                            | 146                            | 147                            | 143           |
| Peel Incursion (%)   | <5                | <5                             | <5                             | <5                             | <5                             |               |
| Peel Locus Of Failure Code   | SIP               | SIP                            | SIP                            | SIP                            | SIP                            |               |
| Peel NSF Failure Code  | FTB               | FTB                            | FTB                            | FTB                            | FTB                            |               |
| Shear  |                   |                                |                                |                                |                                | Shear         |
| Shear Strength (ppi)   | 160               | 164                            | 162                            | 161                            | 164                            | 162           |
| Shear Elongation @ Break (%)   | >50               | >50                            | >50                            | >50                            | >50                            |               |
| Sample ID: DS-58   Weld: Heat Fusion<br>Side: A  | 1                 |                                |                                |                                |                                | Peel A        |
| Peel Strength (ppi)  | 131               | 133                            | 137                            | 132                            | 134                            | 133           |
| Peel Incursion (%)   | <5                | <5                             | <5                             | <5                             | _                              |               |
|  |                   | ~5                             | < 5                            | < 5                            | <5                             |               |
| Peel Locus Of Failure Code   | SIP               | SIP                            | <5<br>SIP                      | SIP                            | <5<br>SIP                      |               |
|  | SIP<br>FTB        |                                |                                |                                |                                |               |
| Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B   |                   | SIP                            | SIP                            | SIP                            | SIP                            | Peel B        |
| Peel NSF Failure Code  |                   | SIP                            | SIP                            | SIP                            | SIP                            | Peel B<br>134 |
| Peel NSF Failure Code Side: B  | FTB               | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     |               |
| Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  | FTB               | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     | SIP<br>FTB                     |               |
| Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code                        | FTB<br>134<br><5  | SIP<br>FTB<br>129<br><5        | SIP<br>FTB<br>134<br><5        | SIP<br>FTB<br>133<br><5        | SIP<br>FTB<br>138<br><5        |               |
| Peel NSF Failure Code  Side: B  Peel Strength (ppi)  | FTB  134  <5  SIP | SIP<br>FTB<br>129<br><5<br>SIP | SIP<br>FTB<br>134<br><5<br>SIP | SIP<br>FTB<br>133<br><5<br>SIP | SIP<br>FTB<br>138<br><5<br>SIP |               |
| Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code | FTB  134  <5  SIP | SIP<br>FTB<br>129<br><5<br>SIP | SIP<br>FTB<br>134<br><5<br>SIP | SIP<br>FTB<br>133<br><5<br>SIP | SIP<br>FTB<br>138<br><5<br>SIP | 134           |

### DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS - SINGLE TRACK TRI Client: Feezor Engineering. Inc.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29875

### **TEST REPLICATE NUMBER**

| PARAMETER                              | 1     | 2   | 3   | 4   | 5   | MEAN  |
|--|-------|-----|-----|-----|-----|-------|
| Sample ID: DS-52 B   Weld: Single Extr | usion |     |     |     |     |       |
| Side: Peel                             |       |     |     |     |     | Peel  |
| Peel Strength (ppi)                    | 133   | 127 | 133 | 72  | 137 | 120   |
| Peel Incursion (%)                     | <5    | <5  | <5  | <5  | <5  |       |
| Peel Locus Of Failure Code             | SIP   | SIP | SIP | SIP | SIP |       |
| Peel NSF Failure Code                  | FTB   | FTB | FTB | FTB | FTB |       |
| Shear                                  |       |     |     |     |     | Shear |
| Shear Strength (ppi)                   | 170   | 174 | 169 | 169 | 166 | 170   |
| Shear Elongation @ Break (%)           | >50   | >50 | >50 | >50 | >50 |       |

### TESTING, RESEARCH, CONSULTING AND FIELD SERVICES AUSTIN, TX - USA | ANAHEIM, CA - USA | ANDERSON, SC - USA | GOLD COAST - AUSTRALIA | SUZHOU - CHINA

Date: 2017-06-23

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29945

Material(s) Tested: (4) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29945

### **TEST REPLICATE NUMBER**

|  | TEST REFERENCE NOTIFIER |     |     |     |     |              |
|--|-------------------------|-----|-----|-----|-----|--------------|
| PARAMETER  | 1                       | 2   | 3   | 4   | 5   | MEAN         |
| Sample ID: DS-59   Weld: Heat Fusior               | 1                       |     |     |     |     |              |
| Side: A  |                         |     |     |     |     | Peel A       |
| Peel Strength (ppi)                                | 94                      | 130 | 111 | 125 | 132 | 118          |
| Peel Incursion (%)                                 | <5                      | <5  | <5  | <5  | <5  | l            |
| Peel Locus Of Failure Code                         | SIP                     | SIP | SIP | SIP | SIP |              |
| Peel NSF Failure Code                              | FTB                     | FTB | FTB | FTB | FTB |              |
| Side: B  |                         |     |     |     |     | Peel B       |
| Peel Strength (ppi)                                | 116                     | 107 | 123 | 116 | 116 | 116          |
| Peel Incursion (%)                                 | <5                      | <5  | <5  | <5  | <5  |              |
| Peel Locus Of Failure Code                         | SIP                     | SIP | SIP | SIP | SIP |              |
| Peel NSF Failure Code                              | FTB                     | FTB | FTB | FTB | FTB |              |
| Shear  |                         |     |     |     |     | Shear        |
| Shear Strength (ppi)                               | 151                     | 152 | 155 | 151 | 151 | 152          |
| Shear Elongation @ Break (%)                       | >50                     | >50 | >50 | >50 | >50 |              |
| Sample ID: DS-60   Weld: Heat Fusior<br>Side: A    | 1                       |     |     |     |     | Peel A       |
| Peel Strength (ppi)                                | 125                     | 128 | 126 | 129 | 129 | 127          |
| Peel Incursion (%)                                 | <5                      | <5  | <5  | <5  | <5  |              |
| Peel Locus Of Failure Code                         | SIP                     | SIP | SIP | SIP | SIP |              |
| Peel NSF Failure Code                              | FTB                     | FTB | FTB | FTB | FTB |              |
| Side: B  |                         |     |     |     |     | Peel B       |
| Peel Strength (ppi)                                | 118                     | 119 | 117 | 121 | 119 | 119          |
| Peel Incursion (%)                                 | <5                      | <5  | <5  | <5  | <5  |              |
| Peel Locus Of Failure Code                         | SIP                     | SIP | SIP | SIP | SIP |              |
|  | FTB                     | FTB | FTB | FTB | FTB |              |
| Peel NSF Failure Code                              | FID                     |     |     |     |     |              |
|  | ГІБ                     |     |     |     |     | Shear        |
| Peel NSF Failure Code  Shear  Shear Strength (ppi) | 152                     | 152 | 153 | 154 | 153 | Shear<br>153 |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29945

### **TEST REPLICATE NUMBER**

| PARAMETER  | 1                                    | 2                                    | 3                                    | 4                                    | 5                                    | MEAN          |
|--|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Sample ID: DS-61   Weld: Heat Fusion   |                                      |                                      |                                      |                                      |                                      |               |
| Side: A  |                                      |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)  | 109                                  | 116                                  | 114                                  | 106                                  | 108                                  | 111           |
| Peel Incursion (%)   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code   | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code  | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B  |                                      |                                      |                                      |                                      |                                      | Peel B        |
| Peel Strength (ppi)  | 108                                  | 90                                   | 98                                   | 117                                  | 120                                  | 107           |
| Peel Incursion (%)   | <5                                   | 100                                  | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code   | SIP                                  | AD                                   | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code  | FTB                                  | NON-FTB                              | FTB                                  | FTB                                  | FTB                                  |               |
| Shear  |                                      |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)   | 158                                  | 156                                  | 158                                  | 155                                  | 153                                  | 156           |
| Shear Elongation @ Break (%)   | >50                                  | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-62   Weld: Heat Fusion<br>Side: A  |                                      |                                      |                                      |                                      |                                      | Peel A        |
|  |                                      |                                      |                                      |                                      |                                      |               |
| Peel Strength (ppi)  | 125                                  | 124                                  | 125                                  | 122                                  | 132                                  | 126           |
|  | 125<br><5                            | 124<br><5                            | 125<br><5                            | 122<br><5                            | 132<br><5                            |               |
| Peel Incursion (%)   |                                      |                                      |                                      |                                      |                                      |               |
| Peel Incursion (%)<br>Peel Locus Of Failure Code   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B  | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 126           |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)  | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 126<br>Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 126<br>Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B  Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code  | <5<br>SIP<br>FTB<br>142<br><5        | <5<br>SIP<br>FTB<br>128<br><5        | <5<br>SIP<br>FTB<br>140<br><5        | <5<br>SIP<br>FTB<br>139<br><5        | <5<br>SIP<br>FTB<br>141<br><5        | 126<br>Peel B |
| Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code   | <5<br>SIP<br>FTB<br>142<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>140<br><5<br>SIP | <5<br>SIP<br>FTB<br>139<br><5<br>SIP | <5<br>SIP<br>FTB<br>141<br><5<br>SIP | 126<br>Peel B |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Shear Shear Strength (ppi) | <5<br>SIP<br>FTB<br>142<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>140<br><5<br>SIP | <5<br>SIP<br>FTB<br>139<br><5<br>SIP | <5<br>SIP<br>FTB<br>141<br><5<br>SIP | Peel B<br>138 |

Date: 2017-06-26

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 29992

Material(s) Tested: (6) Heat Fusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29992

#### TEST REPLICATE NUMBER

| PARAMETER   | 1                                    | 2                                    | 3                                    | 4                                    | 5                                    | MEAN          |
|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Sample ID: DS-63   Weld: Heat Fusion  |                                      |                                      |                                      |                                      |                                      |               |
| Side: A   |                                      |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)   | 133                                  | 132                                  | 126                                  | 128                                  | 122                                  | 128           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B   |                                      |                                      |                                      |                                      |                                      | Peel B        |
| Peel Strength (ppi)   | 130                                  | 137                                  | 123                                  | 137                                  | 134                                  | 132           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Shear   |                                      |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)  | 160                                  | 161                                  | 160                                  | 159                                  | 158                                  | 160           |
| Shear Elongation @ Break (%)  | >50                                  | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-64   Weld: Heat Fusion<br>Side: A   | <u> </u>                             |                                      |                                      |                                      |                                      |               |
| Jidei A   |                                      |                                      |                                      |                                      |                                      | Peel A        |
|   | 124                                  | 125                                  | 124                                  | 126                                  | 124                                  | Peel A        |
| Peel Strength (ppi) Peel Incursion (%)  | 124<br><5                            | 125<br><5                            | 124<br><5                            | 126<br><5                            | 124<br><5                            |               |
| Peel Strength (ppi) Peel Incursion (%)  |                                      |                                      |                                      |                                      |                                      |               |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code  | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Peel Strength (ppi)   | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 125           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 125<br>Peel B |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)  | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 125           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code                       | <5<br>SIP<br>FTB<br>126<br><5        | <5<br>SIP<br>FTB<br>127<br><5        | <5<br>SIP<br>FTB<br>132<br><5        | <5<br>SIP<br>FTB<br>131<br><5        | <5<br>SIP<br>FTB<br>128<br><5        | 125           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code | <5<br>SIP<br>FTB<br>126<br><5<br>SIP | <5<br>SIP<br>FTB<br>127<br><5<br>SIP | <5<br>SIP<br>FTB<br>132<br><5<br>SIP | <5<br>SIP<br>FTB<br>131<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | 125<br>Peel B |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B   | <5<br>SIP<br>FTB<br>126<br><5<br>SIP | <5<br>SIP<br>FTB<br>127<br><5<br>SIP | <5<br>SIP<br>FTB<br>132<br><5<br>SIP | <5<br>SIP<br>FTB<br>131<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | Peel B 129    |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29992

#### TEST REPLICATE NUMBER

|   |                                      | TEST                                 |                                      |                                      |                                      |               |
|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| PARAMETER   | 1                                    | 2                                    | 3                                    | 4                                    | 5                                    | MEAN          |
| Sample ID: DS-65   Weld: Heat Fusion  |                                      |                                      |                                      |                                      |                                      |               |
| Side: A   |                                      |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)   | 130                                  | 138                                  | 143                                  | 146                                  | 142                                  | 140           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B   |                                      |                                      |                                      |                                      |                                      | Peel B        |
| Peel Strength (ppi)   | 138                                  | 149                                  | 149                                  | 147                                  | 147                                  | 146           |
| Peel Incursion (%)  | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP                                  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB                                  | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Shear   |                                      |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)  | 162                                  | 163                                  | 164                                  | 165                                  | 167                                  | 164           |
| Shear Elongation @ Break (%)  | >50                                  | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-66   Weld: Heat Fusion  |                                      |                                      |                                      |                                      |                                      |               |
| Side: A   |                                      |                                      |                                      |                                      |                                      | Peel A        |
|   | 118                                  | 119                                  | 125                                  | 124                                  | 123                                  | Peel A<br>122 |
| Peel Strength (ppi)   | 118<br><5                            | 119<br><5                            | 125<br><5                            | 124<br><5                            | 123<br><5                            |               |
| Peel Strength (ppi) Peel Incursion (%)  |                                      |                                      |                                      |                                      |                                      |               |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code   | <5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code  | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 122           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi)   | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 122           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%)  | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 122           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code                      | <5<br>SIP<br>FTB<br>128<br><5        | <5<br>SIP<br>FTB<br>126<br><5        | <5<br>SIP<br>FTB<br>133<br><5        | <5<br>SIP<br>FTB<br>128<br><5        | <5<br>SIP<br>FTB<br>131<br><5        | 122           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>126<br><5<br>SIP | <5<br>SIP<br>FTB<br>133<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>131<br><5<br>SIP | 122           |
| Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B   | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>126<br><5<br>SIP | <5<br>SIP<br>FTB<br>133<br><5<br>SIP | <5<br>SIP<br>FTB<br>128<br><5<br>SIP | <5<br>SIP<br>FTB<br>131<br><5<br>SIP | Peel B 129    |

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 29992

### **TEST REPLICATE NUMBER**

|                                       | TEST REPLICATE NOMBER |     |     |     |     |        |
|---------------------------------------|-----------------------|-----|-----|-----|-----|--------|
| PARAMETER                             | 1                     | 2   | 3   | 4   | 5   | MEAN   |
| Sample ID: DS-61A   Weld: Heat Fusion | on                    |     |     |     |     |        |
| Side: A                               |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                   | 107                   | 94  | 100 | 107 | 116 | 105    |
| Peel Incursion (%)                    | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code            | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                 | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                               |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                   | 92                    | 106 | 79  | 126 | 114 | 103    |
| Peel Incursion (%)                    | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code            | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                 | FTB                   | FTB | FTB | FTB | FTB |        |
| Shear                                 |                       |     |     |     |     | Shear  |
| Shear Strength (ppi)                  | 156                   | 150 | 156 | 154 | 159 | 155    |
| Shear Elongation @ Break (%)          | >50                   | >50 | >50 | >50 | >50 |        |
| Sample ID: DS-61B   Weld: Heat Fusio  | on                    |     |     |     |     |        |
| Side: A                               |                       |     |     |     |     | Peel A |
| Peel Strength (ppi)                   | 112                   | 136 | 127 | 108 | 128 | 122    |
| Peel Incursion (%)                    | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code            | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                 | FTB                   | FTB | FTB | FTB | FTB |        |
| Side: B                               |                       |     |     |     |     | Peel B |
| Peel Strength (ppi)                   | 118                   | 120 | 124 | 123 | 110 | 119    |
| Peel Incursion (%)                    | <5                    | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code            | SIP                   | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                 | FTB                   | FTB | FTB | FTB | FTB |        |
|                                       |                       |     |     |     |     | Shear  |
| Shear                                 |                       |     |     |     |     |        |
| Shear<br>Shear Strength (ppi)         | 161                   | 160 | 159 | 161 | 162 | 161    |

Date: 2017-06-27

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 30058

Material(s) Tested: (2) Single Extrusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

### TRI Client: Feezor Engineering. Inc.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 30058

### **TEST REPLICATE NUMBER**

|                                      |        | 1531 | REPLICATE N | UMBEK |     |       |
|--------------------------------------|--------|------|-------------|-------|-----|-------|
| PARAMETER                            | 1      | 2    | 3           | 4     | 5   | MEAN  |
| Sample ID: DS-67   Weld: Single Extr | usion  |      |             |       |     |       |
| Side: Peel                           |        |      |             |       |     | Peel  |
| Peel Strength (ppi)                  | 72     | 119  | 103         | 99    | 84  | 95    |
| Peel Incursion (%)                   | 70     | <5   | <5          | <5    | <5  |       |
| Peel Locus Of Failure Code           | AD-BRK | SIP  | SIP         | SIP   | SIP |       |
| Peel NSF Failure Code                | FTB    | FTB  | FTB         | FTB   | FTB |       |
| Shear                                |        |      |             |       |     | Shear |
| Shear Strength (ppi)                 | 156    | 155  | 152         | 152   | 156 | 154   |
| Shear Elongation @ Break (%)         | >50    | >50  | >50         | >50   | >50 |       |
| Sample ID: DS-68   Weld: Single Extr | usion  |      |             |       |     |       |
| Side: Peel                           |        |      |             |       |     | Peel  |
| Peel Strength (ppi)                  | 113    | 118  | 83          | 98    | 95  | 101   |
| Peel Incursion (%)                   | <5     | <5   | <5          | <5    | <5  |       |
| Peel Locus Of Failure Code           | SIP    | SIP  | SIP         | SIP   | SIP |       |
| Peel NSF Failure Code                | FTB    | FTB  | FTB         | FTB   | FTB |       |
| Shear                                |        |      |             |       |     | Shear |
| Shear Strength (ppi)                 | 155    | 155  | 157         | 156   | 158 | 156   |
| Shear Elongation @ Break (%)         | >50    | >50  | >50         | >50   | >50 |       |
|                                      |        |      |             |       |     |       |

Date: 2017-06-28

Mail To: Bill To:

**Arron Weber** 

Feezor Engineering. Inc.

Feezor Engineering. Inc.

, ,

e-mail:

aweber@feezorengineering.com dfeezor@feezorengineering.com bvits@feezorengineering.com

Dear Mr. Weber,

Thank you for consulting with TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

TRI Job Reference Number: 30104

Material(s) Tested: (3) Single Extrusion Weld Seam(s)

Test(s) Requested: SAME DAY Peel and Shear

(ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

Codes:

AD Adhesion Failure (100% Peel)

BRK Break in sheeting away from Seam edge.
SE Break in sheeting at edge of seam.

AD-BRK Break in sheeting after some adhesion failure - partial peel.

SIP Separation in the plane of the sheet (leaving the bond intact).

FTB Film tearing bond (all non "AD" failures).

NON-FTB 100% peel.

If you have any questions or require any additional information, please call us at 1-800-880-8378. Sincerely,

Brian Anderson Project Manager

Geosynthetic Services Division

http://www.geosyntheticstestinc.com

### **DESTRUCTIVE SEAM QUALITY ASSURANCE TEST RESULTS - SINGLE TRACK** TRI Client: Feezor Engineering. Inc.

Project: Bridgeton Landfill - N. Quarry Phase 1A and 1B Cap

Material: 60 mil. HDPE

Shear Elongation @ Break (%)

SAME DAY Peel and Shear (ASTM D 6392/GRI GM19/D 4437/NSF 54/882 mod.)

TRI Log#: 30104

| TRI Log#: 30104                      |         |      |             |       |     |       |
|--------------------------------------|---------|------|-------------|-------|-----|-------|
|                                      |         | TEST | REPLICATE N | UMBER |     |       |
| PARAMETER                            | 1       | 2    | 3           | 4     | 5   | MEAN  |
| Sample ID: DS-67A   Weld: Single Ex  | trusion |      |             |       |     |       |
| Side: Peel                           |         |      |             |       |     | Peel  |
| Peel Strength (ppi)                  | 92      | 104  | 110         | 103   | 124 | 107   |
| Peel Incursion (%)                   | 100     | <5   | <5          | <5    | <5  |       |
| Peel Locus Of Failure Code           | AD      | SIP  | SIP         | SIP   | SIP |       |
| Peel NSF Failure Code                | NON-FTB | FTB  | FTB         | FTB   | FTB |       |
| Shear                                |         |      |             |       |     | Shear |
| Shear Strength (ppi)                 | 161     | 168  | 161         | 164   | 160 | 163   |
| Shear Elongation @ Break (%)         | >50     | >50  | >50         | >50   | >50 |       |
| Sample ID: DS-67B   Weld: Single Ex  | trusion |      |             |       |     |       |
| Side: Peel                           |         |      |             |       |     | Peel  |
| Peel Strength (ppi)                  | 99      | 91   | 94          | 120   | 106 | 102   |
| Peel Incursion (%)                   | <5      | <5   | <5          | <5    | <5  |       |
| Peel Locus Of Failure Code           | SE      | SE   | SE          | SE    | SE  |       |
| Peel NSF Failure Code                | FTB     | FTB  | FTB         | FTB   | FTB |       |
| Shear                                |         |      |             |       |     | Shear |
| Shear Strength (ppi)                 | 157     | 163  | 155         | 149   | 154 | 156   |
| Shear Elongation @ Break (%)         | >50     | >50  | >50         | >50   | >50 |       |
| Sample ID: DS-69   Weld: Single Extr | rusion  |      |             |       |     |       |
| Side: Peel                           |         |      |             |       |     | Peel  |
| Peel Strength (ppi)                  | 148     | 118  | 99          | 148   | 145 | 132   |
| Peel Incursion (%)                   | <5      | <5   | <5          | <5    | <5  |       |
| Peel Locus Of Failure Code           | SIP     | SE   | SE          | SIP   | SIP |       |
| Peel NSF Failure Code                | FTB     | FTB  | FTB         | FTB   | FTB |       |
| Shear                                |         |      |             |       |     | Shear |
| Shear Strength (ppi)                 | 159     | 160  | 159         | 161   | 157 | 159   |
|                                      |         |      |             |       |     |       |

The testing herein is based upon accepted industry practice as well as the test method listed. Test results reported herein do not apply to samples other than those tested. TRI neither accepts responsibility for nor makes claim as to the final use and purpose of the material. TRI observes and maintains client confidentiality. TRI limits reproduction of this report, except in full, without prior approval of TRI.

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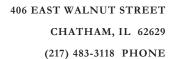
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### Sub-Appendix C.7.3

### **Memorandum Concerning Destructive Failure Tracking**





| MEMC   | DRANDUM                   |                |
|--|---------------------------|----------------|
| TO:<br>Dan Feezor                              | FROM:<br>Brad Vits        |                |
| COMPANY: . Feezor Engineering, Inc.            | DATE: 8/22/2017           |                |
| PROJECT NAME: Phase 1A and 1B EVOH Final Cover | PROJECT NUMBER:<br>BT-125 |                |
| RE: Project Seaming – Destructive Failures     | CC:                       |                |
| URGENT FOR REVIEW PLEASE CO                    | DMMENT PLEASE REPLY       | PLEASE RECYCLE |
| NOTES/COMMENTS:                                |                           |                |

Acceptance criteria for destructive testing was obtained both from the Cornerstone Work Plan entitled *Re: Response to October 19, 2016 Comments for EVOH Cover System Work Plan, North Quarry, Bridgeton Landfill, Bridgeton, Missouri Revision 2* dated October 20, 2016. Page 36 of this document specifies strength requirements for both Hot Wedge Seams and Extrusion Fillet Seams.

| Minimum value |
|---------------|
| 80            |
| 60            |
|               |
| 80            |
| 52            |
|               |

In addition to these strength requirements, standard acceptance criteria from the Geosynthetic Research Institute specification *GRI Test Method GM19* was utilized to for determination of acceptable break codes with the exception of Separation in Plane (SIP) which is identified by the manufacturer to be an acceptable break code for the EVOH material. Language from this specification states that a test should be acceptable if 4 out of 5 specimens meet the minimum required value and the fifth sample meets 80% of the required strength. It also states that a code AD-Brk should only be deemed as a failure if it is >25%.

This was the pass-fail criteria that was used in evaluating seams.

Out of 69 destructive samples that were obtained, 11 of these samples did not meet the above mentioned pass-fail criteria and were bound in accordance with the Project CQA Plan that was included with the Cornerstone Work Plan.

The following lists failing samples and the corrective action that was taken for bounding the failing sample:

**DS-17**DS-17 was noted as a failure due to 2 specimens exhibiting full peel incursion.

| Sample ID: DS-17   Weld: Heat Fusion | 1   |         |     |     |         |        |
|--------------------------------------|-----|---------|-----|-----|---------|--------|
| Side: A                              |     |         |     |     |         | Peel A |
| Peel Strength (ppi)                  | 121 | 95      | 112 | 114 | 115     | 111    |
| Peel Incursion (%)                   | <5  | 100     | <5  | <5  | 100     |        |
| Peel Locus Of Failure Code           | SIP | AD      | SIP | SIP | AD      |        |
| Peel NSF Failure Code                | FTB | NON-FTB | FTB | FTB | NON-FTB |        |
| Side: B                              |     |         |     |     |         | Peel B |
| Peel Strength (ppi)                  | 127 | 131     | 117 | 124 | 114     | 123    |
| Peel Incursion (%)                   | <5  | <5      | <5  | <5  | <5      |        |
| Peel Locus Of Failure Code           | SIP | SIP     | SIP | SIP | SIP     |        |
| Peel NSF Failure Code                | FTB | FTB     | FTB | FTB | FTB     |        |
| Shear                                |     |         |     |     |         | Shear  |
| Shear Strength (ppi)                 | 154 | 154     | 150 | 154 | 150     | 152    |
| Shear Elongation @ Break (%)         | >50 | >50     | >50 | >50 | >50     |        |

This specimen was eventually bound to samples DS-17B2 (before initial sample) and DS-17A2 (after initial sample).

|   | sion  |                                      |                                      |                                      |                                      |               |
|---|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Side: A   |   |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)   | 131   | 127                                  | 142                                  | 117                                  | 130                                  | 129           |
| Peel Incursion (%)  | <5  | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SIP   | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB   | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B   |   |                                      |                                      |                                      |                                      | Peel E        |
| Peel Strength (ppi)   | 123   | 126                                  | 132                                  | 132                                  | 131                                  | 129           |
| Peel Incursion (%)  | <5  | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code  | SE  | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code   | FTB   | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Shear   |   |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)  | 153   | 154                                  | 152                                  | 150                                  | 155                                  | 153           |
| Shear Elongation @ Break (%)  | >50   | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-17 B2   Weld: Heat Fus  | sion  |                                      |                                      |                                      |                                      |               |
| <u> </u>  | sion  |                                      |                                      |                                      |                                      | Peel A        |
| Side: A   | sion<br>135                                 | 130                                  | 143                                  | 115                                  | 132                                  | Peel <i>J</i> |
| Side: A<br>Peel Strength (ppi)  |   | 130<br><5                            | 143<br><5                            | 115<br><5                            | 132<br><5                            |               |
| Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)  | 135   |                                      |                                      |                                      |                                      |               |
| Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code  | 135<br><5                                   | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code   | 135<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 131           |
| Sample ID: DS-17 B2   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)           | 135<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  | 135<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 131           |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)   | 135<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 131           |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code               | 135<br><5<br>SIP<br>FTB<br>132<br><5        | <5<br>SIP<br>FTB<br>129<br><5        | <5<br>SIP<br>FTB<br>136<br><5        | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 131           |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code | 135<br><5<br>SIP<br>FTB<br>132<br><5<br>SIP | <5<br>SIP<br>FTB<br>129<br><5<br>SIP | <5<br>SIP<br>FTB<br>136<br><5<br>SIP | <5<br>SIP<br>FTB<br>136<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | Peel E        |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)   | 135<br><5<br>SIP<br>FTB<br>132<br><5<br>SIP | <5<br>SIP<br>FTB<br>129<br><5<br>SIP | <5<br>SIP<br>FTB<br>136<br><5<br>SIP | <5<br>SIP<br>FTB<br>136<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | 131           |

All seam between DS-17B2 and DS-17A2 was capped with and non-destructively tested in its entirety.

### **DS-19**

DS-19 was noted as a failure due to 3 specimens exhibiting a partial peel incursion >25% and 1 specimen exhibiting full peel incursion.

| Sample ID: DS-19   Weld: Heat Fusio | n      |        |         |     |     |        |
|-------------------------------------|--------|--------|---------|-----|-----|--------|
| Side: A                             |        |        |         |     |     | Peel A |
| Peel Strength (ppi)                 | 127    | 110    | 126     | 120 | 132 | 123    |
| Peel Incursion (%)                  | <5     | <5     | 100     | <5  | <5  |        |
| Peel Locus Of Failure Code          | SE     | SE     | AD      | SE  | SE  |        |
| Peel NSF Failure Code               | FTB    | FTB    | NON-FTB | FTB | FTB |        |
| Side: B                             |        |        |         |     |     | Peel B |
| Peel Strength (ppi)                 | 81     | 123    | 96      | 125 | 121 | 109    |
| Peel Incursion (%)                  | 90     | 90     | 90      | <5  | <5  |        |
| Peel Locus Of Failure Code          | AD-BRK | AD-BRK | AD-BRK  | SE  | SE  |        |
| Peel NSF Failure Code               | FTB    | FTB    | FTB     | FTB | FTB |        |
| Shear                               |        |        |         |     |     | Shear  |
| Shear Strength (ppi)                | 157    | 156    | 154     | 153 | 153 | 155    |
| Shear Elongation @ Break (%)        | >50    | >50    | >50     | >50 | >50 |        |

This specimen was eventually bound to samples DS-19B2 (before initial sample) and DS-19A2 (after initial sample).

| Side: A  |           |           |           |           |           | Peel A       |
|--|-----------|-----------|-----------|-----------|-----------|--------------|
| Peel Strength (ppi)  | 122       | 126       | 128       | 109       | 128       | 123          |
| Peel Incursion (%)   | <5        | <5        | <5        | <5        | <5        |              |
| Peel Locus Of Failure Code   | SE        | SE        | SIP       | SE        | SE        |              |
| Peel NSF Failure Code  | FTB       | FTB       | FTB       | FTB       | FTB       |              |
| Side: B  |           |           |           |           |           | Peel E       |
| Peel Strength (ppi)  | 120       | 120       | 112       | 118       | 122       | 118          |
| Peel Incursion (%)   | <5        | <5        | <5        | <5        | <5        |              |
| Peel Locus Of Failure Code   | SIP       | SIP       | SIP       | SIP       | SIP       |              |
| Peel NSF Failure Code  | FTB       | FTB       | FTB       | FTB       | FTB       |              |
| Shear  |           |           |           |           |           | Shear        |
| Shear Strength (ppi)   | 163       | 164       | 166       | 168       | 162       | 165          |
| Shear Elongation @ Break (%)   | >50       | >50       | >50       | >50       | >50       |              |
| Sample ID: DS-19 B2   Weld: Heat Fusio   | on        |           |           |           |           |              |
| Side: A  |           |           |           |           |           | Peel A       |
| Peel Strength (ppi)  | 134       | 133       | 112       | 116       | 122       | 123          |
| Peel Incursion (%)   | <5        | <5        | <5        | <5        | <5        |              |
| Peel Locus Of Failure Code   | SE        | SIP       | SIP       | SIP       | SE        |              |
| Peel NSF Failure Code  | FTB       | FTB       | FTB       | FTB       | FTB       |              |
|  |           |           |           |           |           | Peel E       |
| Side: B  |           |           |           |           |           |              |
|  | 138       | 74        | 126       | 126       | 131       | 119          |
| Peel Strength (ppi)  | 138<br><5 | 74<br><5  | 126<br><5 | 126<br><5 | 131<br><5 | 119          |
| Peel Strength (ppi)  |           |           |           |           |           | 119          |
| Peel Strength (ppi)<br>Peel Incursion (%)  | <5        | <5        | <5        | <5        | <5        | 119          |
| Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code | <5<br>SIP | <5<br>SIP | <5<br>SIP | <5<br>SIP | <5<br>SIP | 119<br>Shear |
|  | <5<br>SIP | <5<br>SIP | <5<br>SIP | <5<br>SIP | <5<br>SIP |              |

All seam between DS-19B2 and DS-19A2 was capped and non-destructively tested in its entirety.

### **DS-20**

DS-20 was noted as a failure due to 6 specimens exhibiting partial peel incursion >25% and 3 specimens exhibiting full peel incursion.

| Sample ID: DS-20   Weld: Heat Fusio | n      |        |         |         |         |        |
|-------------------------------------|--------|--------|---------|---------|---------|--------|
| Side: A                             |        |        |         |         |         | Peel A |
| Peel Strength (ppi)                 | 82     | 129    | 63      | 65      | 55      | 79     |
| Peel Incursion (%)                  | 90     | 90     | 100     | 100     | 100     |        |
| Peel Locus Of Failure Code          | AD-BRK | AD-BRK | AD      | AD      | AD      |        |
| Peel NSF Failure Code               | FTB    | FTB    | NON-FTB | NON-FTB | NON-FTB |        |
| Side: B                             |        |        |         |         |         | Peel B |
| Peel Strength (ppi)                 | 121    | 132    | 138     | 100     | 98      | 118    |
| Peel Incursion (%)                  | 90     | 90     | 20      | 90      | 90      |        |
| Peel Locus Of Failure Code          | AD-BRK | AD-BRK | AD-BRK  | AD-BRK  | AD-BRK  |        |
| Peel NSF Failure Code               | FTB    | FTB    | FTB     | FTB     | FTB     |        |
| Shear                               |        |        | ı       |         |         | Shear  |
| Shear Strength (ppi)                | 156    | 154    | 153     | 155     | 140     | 152    |
| Shear Elongation @ Break (%)        | >50    | >50    | >50     | >50     | >50     |        |

This specimen was eventually bound to sample DS-20A7 (after initial sample). No passing sample was able to be obtained from seaming produced prior to the failing sample.

| Side: A                      |     |     |     |     |     | Peel A |
|------------------------------|-----|-----|-----|-----|-----|--------|
| Peel Strength (ppi)          | 140 | 138 | 140 | 109 | 148 | 135    |
| Peel Incursion (%)           | <5  | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code   | SIP | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code        | FTB | FTB | FTB | FTB | FTB |        |
| Side: B                      |     |     |     |     |     | Peel E |
| Peel Strength (ppi)          | 141 | 139 | 132 | 139 | 149 | 140    |
| eel Incursion (%)            | <5  | <5  | <5  | <5  | <5  |        |
| eel Locus Of Failure Code    | SE  | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code        | FTB | FTB | FTB | FTB | FTB |        |
| Shear                        |     |     |     |     |     | Shear  |
| Shear Strength (ppi)         | 165 | 166 | 163 | 161 | 163 | 164    |
| Shear Elongation @ Break (%) | >50 | >50 | >50 | >50 | >50 |        |

All seaming between the beginning of production for this technician/machine and DS-20A7 was capped and non-destructively tested in its entirety.

### **DS-21**

DS-21 was noted as a failure due to 2 specimens exhibiting full peel incursion.

| Side: A                      |     |     |         |     |         | Peel A |
|------------------------------|-----|-----|---------|-----|---------|--------|
| Peel Strength (ppi)          | 122 | 126 | 129     | 113 | 128     | 124    |
| Peel Incursion (%)           | <5  | <5  | 100     | <5  | 100     |        |
| Peel Locus Of Failure Code   | SIP | SIP | AD      | SIP | AD      |        |
| Peel NSF Failure Code        | FTB | FTB | NON-FTB | FTB | NON-FTB |        |
| Side: B                      |     |     |         |     |         | Peel B |
| eel Strength (ppi)           | 126 | 128 | 127     | 125 | 122     | 126    |
| eel Incursion (%)            | <5  | <5  | <5      | <5  | <5      |        |
| eel Locus Of Failure Code    | SIP | SIP | SIP     | SIP | SIP     |        |
| Peel NSF Failure Code        | FTB | FTB | FTB     | FTB | FTB     |        |
| Shear                        |     |     |         |     |         | Shear  |
| Shear Strength (ppi)         | 144 | 149 | 147     | 147 | 145     | 146    |
| Shear Elongation @ Break (%) | >50 | >50 | >50     | >50 | >50     |        |

This specimen was eventually bound to sample DS-21B4 (before initial sample) and DS-21A2 (after initial sample).

| Side: A   |  |   |  |  |   | Peel A         |
|---|--|---|--|--|---|----------------|
| Peel Strength (ppi)   | 130  | 127   | 131  | 123  | 114   | 125            |
| Peel Incursion (%)  | <5   | <5  | <5   | <5   | <5  |                |
| Peel Locus Of Failure Code  | SIP  | SIP   | SIP  | SIP  | SIP   |                |
| Peel NSF Failure Code   | FTB  | FTB   | FTB  | FTB  | FTB   |                |
| Side: B   |  |   |  |  |   | Peel B         |
| Peel Strength (ppi)   | 114  | 114   | 118  | 116  | 128   | 118            |
| Peel Incursion (%)  | <5   | <5  | <5   | <5   | <5  |                |
| Peel Locus Of Failure Code  | SIP  | SIP   | SIP  | SIP  | SIP   |                |
| Peel NSF Failure Code   | FTB  | FTB   | FTB  | FTB  | FTB   |                |
| Shear   |  |   |  |  |   | Shear          |
| Shear Strength (ppi)  | 160  | 159   | 158  | 161  | 160   | 160            |
| el el e.e. l (e)  |  | - 50  | - 50                                       | - 50                                       |   |                |
| -   | >50  | >50   | >50  | >50  | >50   |                |
| Sample ID: DS-21 B4   Weld: Heat Fus  |  | >50   | >50  | >50  | >50   | Peel A         |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: <b>A</b>  |  | 130   | 137  | 133  | 136   | Peel A         |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: <b>A</b><br>Peel Strength (ppi)   | ion  |   |  |  |   |                |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: <b>A</b><br>Peel Strength (ppi)<br>Peel Incursion (%)   | ion<br>132                                 | 130   | 137  | 133  | 136   |                |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code  | ion<br>132<br><5                           | 130<br><5                                   | 137<br><5                                  | 133  | 136<br><5                                   |                |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code   | ion<br>132<br><5<br>SE                     | 130<br><5<br>SIP                            | 137<br><5<br>SE                            | 133<br><5<br>SE                            | 136<br><5<br>SIP                            |                |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B  | ion<br>132<br><5<br>SE                     | 130<br><5<br>SIP                            | 137<br><5<br>SE                            | 133<br><5<br>SE                            | 136<br><5<br>SIP                            | 134            |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)   | 132<br><5<br>SE<br>FTB                     | 130<br><5<br>SIP<br>FTB                     | 137<br><5<br>SE<br>FTB                     | 133<br><5<br>SE<br>FTB                     | 136<br><5<br>SIP<br>FTB                     | 134<br>Peel B  |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)   | 132<br><5<br>SE<br>FTB                     | 130<br><5<br>SIP<br>FTB                     | 137<br><5<br>SE<br>FTB                     | 133<br><5<br>SE<br>FTB                     | 136<br><5<br>SIP<br>FTB                     | 134<br>Peel B  |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)<br>Peel Incursion (%)   | 132<br><5<br>SE<br>FTB<br>107<br><5        | 130<br><5<br>SIP<br>FTB<br>117<br><5        | 137<br><5<br>SE<br>FTB                     | 133<br><5<br>SE<br>FTB<br>129<br><5        | 136<br><5<br>SIP<br>FTB<br>103<br><5        | 134<br>Peel B  |
| Sample ID: DS-21 B4   Weld: Heat Fus<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code   | 132<br><5<br>SE<br>FTB<br>107<br><5<br>SIP | 130<br><5<br>SIP<br>FTB<br>117<br><5<br>SIP | 137<br><5<br>SE<br>FTB<br>123<br><5<br>SIP | 133<br><5<br>SE<br>FTB<br>129<br><5<br>SIP | 136<br><5<br>SIP<br>FTB<br>103<br><5<br>SIP | 134<br>Peel B  |
| Shear Elongation @ Break (%)  Sample ID: DS-21 B4   Weld: Heat Fus  Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Shear  Shear Strength (ppi) | 132<br><5<br>SE<br>FTB<br>107<br><5<br>SIP | 130<br><5<br>SIP<br>FTB<br>117<br><5<br>SIP | 137<br><5<br>SE<br>FTB<br>123<br><5<br>SIP | 133<br><5<br>SE<br>FTB<br>129<br><5<br>SIP | 136<br><5<br>SIP<br>FTB<br>103<br><5<br>SIP | 134 Peel B 116 |

All seam between DS-21B4 and DS-21A2 was capped and non-destructively tested in its entirety.

**DS-23** 

DS-23 was noted as a failure due to 1 specimen exhibiting a partial peel incursion of >25% and 2 specimens exhibiting full peel incursion.

| Side: A                      |         |     |         |     |        | Peel A |
|------------------------------|---------|-----|---------|-----|--------|--------|
| Peel Strength (ppi)          | 115     | 126 | 127     | 134 | 133    | 127    |
| Peel Incursion (%)           | <5      | <5  | <5      | <5  | <5     |        |
| Peel Locus Of Failure Code   | SIP     | SIP | SIP     | SE  | SE     |        |
| Peel NSF Failure Code        | FTB     | FTB | FTB     | FTB | FTB    |        |
| Side: B                      |         |     |         |     |        | Peel B |
| Peel Strength (ppi)          | 99      | 126 | 118     | 124 | 127    | 119    |
| Peel Incursion (%)           | 100     | <5  | 100     | <5  | 70     |        |
| Peel Locus Of Failure Code   | AD      | SIP | AD      | SIP | AD-BRK |        |
| Peel NSF Failure Code        | NON-FTB | FTB | NON-FTB | FTB | FTB    |        |
| Shear                        |         |     |         |     |        | Shear  |
| Shear Strength (ppi)         | 155     | 157 | 157     | 154 | 154    | 155    |
| Shear Elongation @ Break (%) | >50     | >50 | >50     | >50 | >50    |        |

This specimen was bound to sample DS-23B (before initial sample) and DS-23A (after initial sample)

| Side: A  |   |   |                                      |                                      |                                      | Peel A         |
|--|---|---|--------------------------------------|--------------------------------------|--------------------------------------|----------------|
| Peel Strength (ppi)  | 134   | 134   | 142                                  | 125                                  | 133                                  | 134            |
| Peel Incursion (%)   | <5  | <5  | <5                                   | <5                                   | <5                                   |                |
| Peel Locus Of Failure Code   | SIP   | SIP   | SIP                                  | SIP                                  | SIP                                  |                |
| Peel NSF Failure Code  | FTB   | FTB   | FTB                                  | FTB                                  | FTB                                  |                |
| Side: B  |   |   |                                      |                                      |                                      | Peel B         |
| Peel Strength (ppi)  | 132   | 128   | 125                                  | 134                                  | 131                                  | 130            |
| Peel Incursion (%)   | <5  | <5  | <5                                   | <5                                   | <5                                   |                |
| Peel Locus Of Failure Code   | SIP   | SIP   | SIP                                  | SE                                   | SE                                   |                |
| Peel NSF Failure Code  | FTB   | FTB   | FTB                                  | FTB                                  | FTB                                  |                |
| Shear  |   |   |                                      |                                      |                                      | Shear          |
| Shear Strength (ppi)   | 156   | 159   | 159                                  | 156                                  | 155                                  | 157            |
| Shear Elongation @ Break (%)   | >50   | >50   | >50                                  | >50                                  | >50                                  |                |
| Sample ID: DS-23 B   Weld: Heat Fusion   | on  |   |                                      |                                      |                                      |                |
|  | on  |   |                                      |                                      |                                      | Peel A         |
| Sample ID: DS-23 B   Weld: Heat Fusion   | on<br>130                                   | 121   | 127                                  | 123                                  | 125                                  | Peel A         |
| Sample ID: DS-23 B   Weld: Heat Fusion   |   |   | 127<br><5                            | 123<br><5                            | 125<br><5                            |                |
| Sample ID: DS-23 B   Weld: Heat Fusion Side: A Peel Strength (ppi)   | 130   | 121   |                                      |                                      |                                      |                |
| Sample ID: DS-23 B   Weld: Heat Fusion<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)   | 130<br><5                                   | 121 <5                                      | <5                                   | <5                                   | <5                                   |                |
| Sample ID: DS-23 B   Weld: Heat Fusion<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code   | 130<br><5<br>SIP                            | 121<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |                |
| Sample ID: DS-23 B   Weld: Heat Fusion<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code  | 130<br><5<br>SIP                            | 121<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 125            |
| Sample ID: DS-23 B   Weld: Heat Fusion<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B   | 130<br><5<br>SIP<br>FTB                     | 121<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 125            |
| Sample ID: DS-23 B   Weld: Heat Fusion<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)                          | 130<br><5<br>SIP<br>FTB                     | 121<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 125            |
| Sample ID: DS-23 B   Weld: Heat Fusion<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)<br>Peel Incursion (%)    | 130<br><5<br>SIP<br>FTB<br>126<br><5        | 121<br><5<br>SIP<br>FTB<br>132<br><5        | <5<br>SIP<br>FTB<br>125<br><5        | <5<br>SIP<br>FTB<br>126<br><5        | <5<br>SIP<br>FTB                     | 125            |
| Sample ID: DS-23 B   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code | 130<br><5<br>SIP<br>FTB<br>126<br><5<br>SIP | 121<br><5<br>SIP<br>FTB<br>132<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | <5<br>SIP<br>FTB<br>126<br><5<br>SIP | <5<br>SIP<br>FTB<br>122<br><5<br>SIP | 125 Peel B 126 |
| Sample ID: DS-23 B   Weld: Heat Fusion Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code Side: B Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code | 130<br><5<br>SIP<br>FTB<br>126<br><5<br>SIP | 121<br><5<br>SIP<br>FTB<br>132<br><5<br>SIP | <5<br>SIP<br>FTB<br>125<br><5<br>SIP | <5<br>SIP<br>FTB<br>126<br><5<br>SIP | <5<br>SIP<br>FTB<br>122<br><5<br>SIP | 125            |

All seam between DS-23B and DS-23A was capped and non-destructively tested in its entirety.

#### **DS-47**

DS-47 was noted as a failure due to 2 specimens exhibiting partial peel incursion >25% and 1 specimen exhibiting full peel incursion.

| Side: Peel                   |        |         |        |        |        | Peel  |
|------------------------------|--------|---------|--------|--------|--------|-------|
| Peel Strength (ppi)          | 87     | 79      | 76     | 86     | 83     | 82    |
| Peel Incursion (%)           | 20     | 100     | 30     | 20     | 90     |       |
| Peel Locus Of Failure Code   | AD-BRK | AD      | AD-BRK | AD-BRK | AD-BRK |       |
| Peel NSF Failure Code        | FTB    | NON-FTB | FTB    | FTB    | FTB    |       |
| Shear                        |        |         |        |        |        | Shear |
| Shear Strength (ppi)         | 167    | 164     | 168    | 168    | 165    | 166   |
| Shear Elongation @ Break (%) | >50    | >50     | >50    | >50    | >50    |       |

This specimen was bound to sample DS-47B (before initial sample). Due to the proximity of the initial sample to the end of the technican/machine production, no sample was obtained after the initial sample.

| Side: Peel                   |     |     |     |     |     | Peel  |
|------------------------------|-----|-----|-----|-----|-----|-------|
| Peel Strength (ppi)          | 124 | 129 | 122 | 134 | 150 | 132   |
| Peel Incursion (%)           | <5  | <5  | <5  | <5  | <5  |       |
| Peel Locus Of Failure Code   | SIP | SIP | SIP | SIP | SIP |       |
| Peel NSF Failure Code        | FTB | FTB | FTB | FTB | FTB |       |
| Shear                        |     |     |     |     |     | Shear |
| Shear Strength (ppi)         | 167 | 171 | 172 | 171 | 169 | 170   |
| Shear Elongation @ Break (%) | >50 | >50 | >50 | >50 | >50 |       |

All seam between DS-47B and the end of production for this particular technician/machine combination was capped and non-destructively tested in its entirety.

**DS-52** 

DS-52 was noted as a failure due to 1 specimen exhibiting full peel incursion.

| Sample ID: DS-52   Weld: Single Extru | ısion |         |     |     |       |       |
|---------------------------------------|-------|---------|-----|-----|-------|-------|
| Side: Peel                            |       |         |     |     |       | Peel  |
| Peel Strength (ppi)                   | 127   | 81      | 142 | 119 | 89    | 112   |
| Peel Incursion (%)                    | <5    | 100     | <5  | <5  | <5    |       |
| Peel Locus Of Failure Code            | SIP   | AD      | SIP | SIP | SIP   |       |
| Peel NSF Failure Code                 | FTB   | NON-FTB | FTB | FTB | FTB   |       |
| Shear                                 |       |         |     |     |       | Shear |
| Shear Strength (ppi)                  | 161   | 163     | 159 | 160 | 143   | 157   |
| Shear Elongation @ Break (%)          | >50   | >50     | >50 | >50 | 20.87 |       |

This specimen was bound to sample DS-52B (before initial sample). Due to the proximity of the initial sample to the end of the technician/machine production, no sample was obtained after the initial sample.

| Sample ID: DS-52 B   Weld: Single Ext | rusion | •   | •   | •   | •   | •     |
|---------------------------------------|--------|-----|-----|-----|-----|-------|
| Side: Peel                            |        |     |     |     |     | Peel  |
| Peel Strength (ppi)                   | 133    | 127 | 133 | 72  | 137 | 120   |
| Peel Incursion (%)                    | <5     | <5  | <5  | <5  | <5  |       |
| Peel Locus Of Failure Code            | SIP    | SIP | SIP | SIP | SIP |       |
| Peel NSF Failure Code                 | FTB    | FTB | FTB | FTB | FTB |       |
| Shear                                 |        |     |     |     |     | Shear |
| Shear Strength (ppi)                  | 170    | 174 | 169 | 169 | 166 | 170   |
| Shear Elongation @ Break (%)          | >50    | >50 | >50 | >50 | >50 |       |

All seam between DS-52B and the end of production for this particular technician/machine combination was capped and non-destructively tested in its entirety.

DS-55

DS-55 was noted as a failure due to 1 specimen exhibiting full peel incursion.

| Side: A                      |     |     |         |     |     | Peel A |
|------------------------------|-----|-----|---------|-----|-----|--------|
| Peel Strength (ppi)          | 124 | 123 | 122     | 132 | 133 | 127    |
| Peel Incursion (%)           | <5  | <5  | 100     | <5  | <5  |        |
| Peel Locus Of Failure Code   | SIP | SIP | AD      | SIP | SIP |        |
| Peel NSF Failure Code        | FTB | FTB | NON-FTB | FTB | FTB |        |
| Side: B                      |     |     |         |     |     | Peel E |
| Peel Strength (ppi)          | 136 | 125 | 116     | 128 | 116 | 124    |
| Peel Incursion (%)           | <5  | <5  | <5      | <5  | <5  |        |
| Peel Locus Of Failure Code   | SIP | SIP | SIP     | SIP | SIP |        |
| Peel NSF Failure Code        | FTB | FTB | FTB     | FTB | FTB |        |
| Shear                        |     |     |         |     |     | Shear  |
| Shear Strength (ppi)         | 154 | 158 | 151     | 155 | 151 | 154    |
| Shear Elongation @ Break (%) | >50 | >50 | >50     | >50 | >50 |        |

This specimen was bound to sample DS-55B (before initial sample). Due to proximity of the initial sample to the end of the technician/machine production, no sample was obtained after the initial sample.

| Sample ID: DS-55 B   Weld: Heat Fusion | on  |     |     |     |     |        |
|--|-----|-----|-----|-----|-----|--------|
| Side: A                                |     |     |     |     |     | Peel A |
| Peel Strength (ppi)                    | 145 | 130 | 140 | 137 | 135 | 137    |
| Peel Incursion (%)                     | <5  | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code             | SIP | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code                  | FTB | FTB | FTB | FTB | FTB |        |
| ide: B                                 |     |     |     |     |     | Peel B |
| eel Strength (ppi)                     | 140 | 138 | 140 | 146 | 140 | 141    |
| eel Incursion (%)                      | <5  | <5  | <5  | <5  | <5  |        |
| eel Locus Of Failure Code              | SIP | SIP | SIP | SIP | SIP |        |
| eel NSF Failure Code                   | FTB | FTB | FTB | FTB | FTB |        |
| Shear                                  |     |     |     |     |     | Shear  |
| hear Strength (ppi)                    | 160 | 163 | 161 | 166 | 157 | 161    |
| Shear Elongation @ Break (%)           | >50 | >50 | >50 | >50 | >50 |        |

All seam between DS-55B and the end of production for this particular technician/machine combination was capped and non-destructively tested in its entirety.

**DS-57**DS-57 was noted as a failure due to 8 specimens exhibiting full peel incursion.

| Sample ID: DS-57   Weld: Heat Fusio | n       |         |         |         |         |        |
|-------------------------------------|---------|---------|---------|---------|---------|--------|
| Side: A                             |         |         |         |         |         | Peel A |
| Peel Strength (ppi)                 | 130     | 132     | 131     | 136     | 119     | 130    |
| Peel Incursion (%)                  | 100     | 100     | <5      | 100     | 100     |        |
| Peel Locus Of Failure Code          | AD      | AD      | SIP     | AD      | AD      |        |
| Peel NSF Failure Code               | NON-FTB | NON-FTB | FTB     | NON-FTB | NON-FTB |        |
| Side: B                             |         |         | l       |         |         | Peel B |
| Peel Strength (ppi)                 | 67      | 59      | 80      | 75      | 71      | 70     |
| Peel Incursion (%)                  | <5      | 100     | 100     | 100     | 100     |        |
| Peel Locus Of Failure Code          | SIP     | AD      | AD      | AD      | AD      |        |
| Peel NSF Failure Code               | FTB     | NON-FTB | NON-FTB | NON-FTB | NON-FTB |        |
| Shear                               |         |         |         |         |         | Shear  |
| Shear Strength (ppi)                | 152     | 158     | 148     | 154     | 148     | 152    |
| Shear Elongation @ Break (%)        | >50     | >50     | >50     | >50     | >50     |        |

This specimen was bound to sample DS-57B (before initial sample). Due to proximity of the initial sample to the end of the technician/machine production, no sample was obtained after the initial sample.

| Side: A                      |     |     |     |     |     | Peel A |
|------------------------------|-----|-----|-----|-----|-----|--------|
| Peel Strength (ppi)          | 138 | 138 | 138 | 143 | 137 | 139    |
| Peel Incursion (%)           | <5  | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code   | SIP | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code        | FTB | FTB | FTB | FTB | FTB |        |
| Side: B                      |     |     |     |     |     | Peel E |
| Peel Strength (ppi)          | 144 | 140 | 140 | 146 | 147 | 143    |
| Peel Incursion (%)           | <5  | <5  | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code   | SIP | SIP | SIP | SIP | SIP |        |
| Peel NSF Failure Code        | FTB | FTB | FTB | FTB | FTB |        |
| Shear                        |     |     |     |     |     | Shear  |
| Shear Strength (ppi)         | 160 | 164 | 162 | 161 | 164 | 162    |
| Shear Elongation @ Break (%) | >50 | >50 | >50 | >50 | >50 |        |

All seam between DS-57B and the end of production for this particular technician/machine combination was capped and non-destructively tested in its entirety.

#### **DS-61**

DS-61 was noted as a failure due to 1 specimen exhibiting full peel incursion.

| Sample ID: DS-61   Weld: Heat Fusion | 1   |         |     |     |     |        |
|--------------------------------------|-----|---------|-----|-----|-----|--------|
| Side: A                              |     |         |     |     |     | Peel A |
| Peel Strength (ppi)                  | 109 | 116     | 114 | 106 | 108 | 111    |
| Peel Incursion (%)                   | <5  | <5      | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP | SIP     | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB | FTB     | FTB | FTB | FTB |        |
| Side: B                              |     |         |     |     |     | Peel B |
| Peel Strength (ppi)                  | 108 | 90      | 98  | 117 | 120 | 107    |
| Peel Incursion (%)                   | <5  | 100     | <5  | <5  | <5  |        |
| Peel Locus Of Failure Code           | SIP | AD      | SIP | SIP | SIP |        |
| Peel NSF Failure Code                | FTB | NON-FTB | FTB | FTB | FTB |        |
| Shear                                |     |         |     |     |     | Shear  |
| Shear Strength (ppi)                 | 158 | 156     | 158 | 155 | 153 | 156    |
| Shear Elongation @ Break (%)         | >50 | >50     | >50 | >50 | >50 |        |

The specimen was bound to samples DS-61B (before initial specimen) and DS-61A (after initial specimen).

|  | n   |                                      |                                      |                                      |                                      |               |
|--|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Side: A  |   |                                      |                                      |                                      |                                      | Peel A        |
| Peel Strength (ppi)  | 107   | 94                                   | 100                                  | 107                                  | 116                                  | 105           |
| Peel Incursion (%)   | <5  | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code   | SIP   | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code  | FTB   | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Side: B  |   |                                      |                                      |                                      |                                      | Peel B        |
| Peel Strength (ppi)  | 92  | 106                                  | 79                                   | 126                                  | 114                                  | 103           |
| Peel Incursion (%)   | <5  | <5                                   | <5                                   | <5                                   | <5                                   |               |
| Peel Locus Of Failure Code   | SIP   | SIP                                  | SIP                                  | SIP                                  | SIP                                  |               |
| Peel NSF Failure Code  | FTB   | FTB                                  | FTB                                  | FTB                                  | FTB                                  |               |
| Shear  |   |                                      |                                      |                                      |                                      | Shear         |
| Shear Strength (ppi)   | 156   | 150                                  | 156                                  | 154                                  | 159                                  | 155           |
| Shear Elongation @ Break (%)   | >50   | >50                                  | >50                                  | >50                                  | >50                                  |               |
| Sample ID: DS-61B   Weld: Heat Fusio   | on .  |                                      |                                      |                                      |                                      |               |
| <u> </u>   | on  |                                      |                                      |                                      |                                      | Peel A        |
| Side: A  | on 112                                      | 136                                  | 127                                  | 108                                  | 128                                  | Peel A        |
| Side: A<br>Peel Strength (ppi)   |   | 136<br><5                            | 127<br><5                            | 108<br><5                            | 128<br><5                            |               |
| Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)   | 112   |                                      |                                      |                                      |                                      |               |
| Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code   | 112<br><5                                   | <5                                   | <5                                   | <5                                   | <5                                   | Peel A        |
| Side: A Peel Strength (ppi) Peel Incursion (%) Peel Locus Of Failure Code Peel NSF Failure Code  | 112<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            |               |
| Sample ID: DS-61B   Weld: Heat Fusion<br>Side: A<br>Peel Strength (ppi)<br>Peel Incursion (%)<br>Peel Locus Of Failure Code<br>Peel NSF Failure Code<br>Side: B<br>Peel Strength (ppi)                   | 112<br><5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | <5<br>SIP                            | 122           |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B   | 112<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 122<br>Peel B |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  | 112<br><5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | <5<br>SIP<br>FTB                     | 122<br>Peel B |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code                        | 112<br><5<br>SIP<br>FTB<br>118<br><5        | <5<br>SIP<br>FTB<br>120<br><5        | <5<br>SIP<br>FTB<br>124<br><5        | <5<br>SIP<br>FTB<br>123<br><5        | <5<br>SIP<br>FTB                     | 122<br>Peel B |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code | 112<br><5<br>SIP<br>FTB<br>118<br><5<br>SIP | <5<br>SIP<br>FTB<br>120<br><5<br>SIP | <5<br>SIP<br>FTB<br>124<br><5<br>SIP | <5<br>SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SIP<br>FTB<br>110<br><5<br>SIP | Peel B        |
| Side: A  Peel Strength (ppi)  Peel Incursion (%)  Peel Locus Of Failure Code  Peel NSF Failure Code  Side: B  Peel Strength (ppi)  Peel Incursion (%)  | 112<br><5<br>SIP<br>FTB<br>118<br><5<br>SIP | <5<br>SIP<br>FTB<br>120<br><5<br>SIP | <5<br>SIP<br>FTB<br>124<br><5<br>SIP | <5<br>SIP<br>FTB<br>123<br><5<br>SIP | <5<br>SIP<br>FTB<br>110<br><5<br>SIP | 122<br>Peel B |

All seam between DS-61B and DS-61B was capped and non-destructively tested in its entirety.

#### **DS-67**

DS-67 was noted as a failure due to 1 specimen exhibiting partial peel incursion 25%.

| Side: Peel                   |        |     |     |     |     | Peel  |
|------------------------------|--------|-----|-----|-----|-----|-------|
| Peel Strength (ppi)          | 72     | 119 | 103 | 99  | 84  | 95    |
| Peel Incursion (%)           | 70     | <5  | <5  | <5  | <5  |       |
| Peel Locus Of Failure Code   | AD-BRK | SIP | SIP | SIP | SIP |       |
| Peel NSF Failure Code        | FTB    | FTB | FTB | FTB | FTB |       |
| Shear                        |        |     |     |     |     | Shear |
| Shear Strength (ppi)         | 156    | 155 | 152 | 152 | 156 | 154   |
| Shear Elongation @ Break (%) | >50    | >50 | >50 | >50 | >50 |       |

This specimen was bound to sample DS-67B (before initial sample). Due to proximity of the initial sample to the end of the technician/machine production, no sample was obtained after the initial sample.

| Side: Peel                   |     |     |     |     |     | Peel  |
|------------------------------|-----|-----|-----|-----|-----|-------|
| Peel Strength (ppi)          | 99  | 91  | 94  | 120 | 106 | 102   |
| Peel Incursion (%)           | <5  | <5  | <5  | <5  | <5  |       |
| Peel Locus Of Failure Code   | SE  | SE  | SE  | SE  | SE  |       |
| Peel NSF Failure Code        | FTB | FTB | FTB | FTB | FTB |       |
| Shear                        |     |     |     |     |     | Shear |
| Shear Strength (ppi)         | 157 | 163 | 155 | 149 | 154 | 156   |
| Shear Elongation @ Break (%) | >50 | >50 | >50 | >50 | >50 |       |

All seam between DS-67B and the end of production for this particular technician/machine combination was capped and non-destructively tested in its entirety.

#### Sub-Appendix C.8

|     |         |         |            |          | N          | /larked    |         |              |       |           |       | Repai  | red   |      |      |           | Teste | d     |           |     | Notes              |
|-----|---------|---------|------------|----------|------------|------------|---------|--------------|-------|-----------|-------|--------|-------|------|------|-----------|-------|-------|-----------|-----|--------------------|
| Num | Panel 1 | Panel 2 | Panel 3    | Panel 4  | Panel 5    | Panel 6    | Station | Station End  | Type  | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /    | DS# | Comments           |
| 1   | 3       | 4       | T direct 5 | · unc. · | T direct 5 | T dilici 0 | 39      | Station Line | PATCH | 5/17/2017 | 14:00 | 2      | 1     | PH   | 211  | 5/22/2017 | BS    | AW    | Fail<br>P |     | Comments           |
| 2   | 3       | 4       |            |          |            |            | 73      |              | PATCH | 5/17/2017 | 14:10 | 4      | 2     | PH   | 211  | 5/22/2017 | BS    | AW    | P         | 1   |                    |
| 3   | 20      | 21      |            |          |            |            | 0       | 25           | PATCH | 5/18/2017 | 17:00 | 25     | 2     | MAY  | 211  | 5/22/2017 | BS    | AW    | P         | 1   |                    |
| 4   | 1       | 18      |            |          |            |            | 13      | 25           | PATCH | 5/22/2017 | 9:05  | 2      | 2     | MAY  | 211  | 5/22/2017 | BS    | AW    | P         |     |                    |
| 5   | 33      | 35      |            |          |            |            | 15      |              | PATCH | 5/25/2017 | 11:27 | 3      | 2     | AG   | 112  | 5/26/2017 | MAM   | AW    | P         |     |                    |
| 6   | 37      | 39      |            |          |            |            | 74      |              | PATCH | 5/25/2017 | 13:05 | 2      | 1     | AG   | 112  | 5/26/2017 | MAM   | AW    | P         |     |                    |
| 7   | 48      | 49      | 50         |          |            |            | 0       |              | PATCH | 5/25/2017 | 14:12 | 3      | 2     | AG   | 112  | 5/26/2017 | MAM   | AW    | P         |     |                    |
| 8   | 49      | 50      | 51         |          |            |            | 0       |              | PATCH | 5/25/2017 | 14:20 | 3      | 2     | AG   | 112  | 5/26/2017 | MAM   | AW    | P         |     |                    |
| 9   | 1       | 18      | 19         |          |            |            | 0       |              | PATCH | 5/22/2017 | 9:10  | 2      | 1     | MAY  | 211  | 5/22/2017 | BS    | AW    | P         |     |                    |
| 10  | 5       | 6       | 13         |          |            |            | 93      |              | PATCH | 5/17/2017 | 14:05 | 4      | 2     | PH   | 211  | 6/16/2017 | BS    | AW    | P         | 2   |                    |
| 11  | 9       | -       |            |          |            |            | 42      |              | PATCH | 5/18/2017 | 16:10 | 5      | 5     | MAY  | 211  | 6/28/2017 | PP    | AW    | P         | 2   |                    |
| 12  | 11      | 12      | 13         |          |            |            | 0       |              | PATCH | 5/18/2017 | 16:25 | 2      | 2     | MAY  | 211  | 6/28/2017 | PP    | AW    | P         |     |                    |
| 13  | 12      | 13      | 14         |          |            |            | 0       |              | PATCH | 5/18/2017 | 16:30 | 2      | 2     | MAY  | 211  | 6/28/2017 | PP    | AW    | P         |     |                    |
| 14  | 21      | 22      | 177        |          |            |            | 61      |              | PATCH | 5/18/2017 | 17:28 | 5      | 5     | MAY  | 211  | 5/26/2017 | WE    | AW    | P         |     |                    |
| 15  | 24      | 25      |            |          |            |            | 70      |              | PATCH | 5/22/2017 | 11:05 | 4      | 2     | MAY  | 211  | 5/26/2017 | WE    | AW    | P         | 5   |                    |
| 16  | 25      | 26      | 27         |          |            |            | 55      | 63           | PATCH | 5/22/2017 | 11:30 | 8      | 3     | MAY  | 211  | 5/26/2017 | WE    | AW    | P         | ,   |                    |
| 17  | 27      | 28      |            |          |            |            | 31      | 03           | PATCH | 5/25/2017 | 9:40  | 5      | 5     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                    |
| 18  | 27      | 28      |            |          |            |            | 35      |              | PATCH | 5/25/2017 | 9:50  | 4      | 4     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                    |
| 19  | 27      | 28      |            |          |            |            | 43      |              | PATCH | 5/25/2017 | 10:18 | 5      | 3     | AG   | 112  | 5/26/2017 | WE    | AW    | P         | 7   |                    |
| 20  | 28      | 29      |            |          |            |            | 33      |              | PATCH | 5/25/2017 | 10:20 | 5      | 3     | AG   | 112  | 5/26/2017 | WE    | AW    | P         | ,   |                    |
| 21  | 27      | 28      | 29         |          |            |            |         |              | PATCH | 5/25/2017 | 10:25 | 5      | 4     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                    |
| 22  | 28      | 29      |            |          |            |            | 26      |              | PATCH | 5/25/2017 | 9:52  | 2      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                    |
| 23  | 28      | 29      | 32         |          |            |            |         |              | PATCH | 5/25/2017 | 10:36 | 3      | 2     | AG   | 112  | 5/26/2017 | BS    | AW    | P         |     |                    |
| 24  | 28      | 31      | 32         |          |            |            |         |              | PATCH | 5/25/2017 | 10:47 | 2      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                    |
| 25  | 33      | 34      | 35         |          |            |            |         |              | PATCH | 5/25/2017 | 10:51 | 2      | 2     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                    |
| 26  | 34      | 35      | 36         |          |            |            |         |              | PATCH | 5/25/2017 | 11:00 | 2      | 2     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                    |
| 27  | 38      | 39      |            |          |            |            | 40      |              | PATCH | 5/25/2017 | 11:53 | 5      | 2     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                    |
| 28  | 38      |         |            |          |            |            | 40      |              | PATCH | 5/25/2017 | 11:53 | 4      | 4     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                    |
| 29  | 36      | 37      | 38         |          |            |            |         |              | PATCH | 5/25/2017 | 11:10 | 5      | 3     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                    |
| 30  | 37      | 38      | 39         |          |            |            |         |              | PATCH | 5/25/2017 | 11:17 | 2      | 2     | AG   | 112  | 6/28/2017 | PP    | AW    | Р         |     |                    |
| 31  | 40      | 41      |            |          |            |            | 107     |              | PATCH | 5/25/2017 | 13:09 | 4      | 2     | AG   | 112  | 6/28/2017 | PP    | AW    | Р         | 9   |                    |
| 32  | 43      |         |            |          |            |            | 23      |              | PATCH | 5/25/2017 | 16:01 | 1      | 1     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                    |
| 33  | 41      | 43      |            |          |            |            | 24      | 26           | PATCH | 5/25/2017 | 15:50 | 2      | 2     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     | CAPS 41/43 24'-26' |
| 34  | 41      | 42      | 43         |          |            |            | 0       | 8            | PATCH | 5/25/2017 | 15:50 | 5      | 3     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     | CAPS 42/43 8'-16'  |
| 35  | 42      | 43      | 46         |          |            |            | 8       | 16           | PATCH | 5/25/2017 | 15:50 | 9      | 2     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     | CAPS 42/43 0'-8'   |
| 36  | 42      | 45      | 46         |          |            |            |         |              | PATCH | 5/25/2017 | 16:20 | 3      | 2     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                    |
| 37  | 42      | 44      | 45         |          |            |            | 2       | 16           | PATCH | 5/25/2017 | 15:02 | 3      | 14    | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     | CAPS 45/44 2'-16'  |
| 38  | 44      | 45      | 47         |          |            |            | 0       | 2            | PATCH | 5/25/2017 | 15:02 | 6      | 3     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     | CAPS 45/44 0'-2'   |
| 39  | 44      | 47      |            |          |            |            | 5       |              | PATCH | 5/25/2017 | 15:02 | 3      | 6     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                    |
| 40  | 44      | 47      |            |          |            |            | 9       |              | PATCH | 5/25/2017 | 15:02 | 4      | 3     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                    |



|     |         |         |         |         | N       | // Aarked |         |             |           |           |       | Repair | red   |      |      |           | Teste | d     |           |     | Notes             |
|-----|---------|---------|---------|---------|---------|-----------|---------|-------------|-----------|-----------|-------|--------|-------|------|------|-----------|-------|-------|-----------|-----|-------------------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6   | Station | Station End | Туре      | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /    | DS# | Comments          |
| 41  | 47      | 48      |         |         |         |           | 53      |             | PATCH     | 5/25/2017 | 13:50 | 4      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | Fail<br>P | 10  | <u> </u>          |
| 42  | 51      | 52      | 53      |         |         |           | 33      |             | PATCH     | 5/26/2017 | 9:47  | 2      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | P P       | 10  |                   |
| 43  | 53      | 54      | 55      |         |         |           | 54      |             | PATCH     | 5/26/2017 | 9:40  | 6      | 4     | AG   | 112  | 5/26/2017 | WE    | AW    | P P       |     |                   |
| 44  | 51      | 53      | 54      |         |         |           | 54      |             | PATCH     | 5/26/2017 | 9:52  | 3      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                   |
| 45  | 49      | 51      | 54      |         |         |           |         |             | PATCH     | 5/26/2017 | 9:55  | 3      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                   |
| 46  | 49      | 54      | 55      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:00 | 2      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                   |
| 46  | 48      | 49      | 55      |         |         |           |         |             | PATCH     |           | 10:05 | 5      | 2     | AG   | 112  | 5/26/2017 | WE    |       | P         | 42  |                   |
|     |         |         |         |         |         |           |         |             |           | 5/26/2017 |       |        |       |      |      |           |       | AW    |           | 12  |                   |
| 48  | 48      | 55      | 56      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:10 | 2      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                   |
| 49  | 48      | 56      | 58      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:15 | 3      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                   |
| 50  | 47      | 48      | 58      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:20 | 4      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 51  | 47      | 58      | 59      |         |         |           |         |             | PATCH     | 5/26/2017 | 11:01 | 3      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | P         |     |                   |
| 52  | 56      | 57      | 58      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:30 | 1      | 1     | AG   | 112  | 6/28/2017 | PP    | AW    | Р         |     |                   |
| 53  | 57      | 58      | 59      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:35 | 1      | 1     | AG   | 112  | 6/28/2017 | PP    | AW    | Р         |     |                   |
| 54  | 47      | 59      | 60      |         |         |           |         |             | PATCH     | 5/26/2017 | 11:06 | 2      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 55  | 45      | 47      | 60      |         |         |           |         |             | PATCH     | 5/26/2017 | 11:14 | 3      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 56  | 45      | 46      | 60      | 61      |         |           |         |             | PATCH     | 5/26/2017 | 11:20 | 2      | 1     | AG   | 112  | 5/26/2017 | BS    | AW    | Р         |     |                   |
| 57  | 61      |         |         |         |         |           | 50'S    | 8'E         | PATCH     | 5/26/2017 | 13:20 | 5      | 5     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 58  | 61      | 62      |         |         |         |           | 70      |             | PATCH     | 5/26/2017 | 11:47 | 5      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         | 13  |                   |
| 59  | 46      | 61      | 65      | 62      |         |           |         |             | PATCH     | 5/26/2017 | 11:34 | 2      | 4     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 60  | 62      | 63      | 65      |         |         |           |         |             | PATCH     | 5/26/2017 | 11:36 | 2      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 61  | 43      | 46      | 65      |         |         |           |         |             | PATCH     | 5/26/2017 | 13:15 | 2      | 3     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 62  | 43      | 63      | 65      |         |         |           |         |             | PATCH     | 5/26/2017 | 13:45 | 2      | 1     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 63  | 41      | 43      | 63      |         |         |           |         |             | PATCH     | 5/26/2017 | 11:36 | 2      | 3     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 64  | 41      | 63      | 64      | 68      |         |           |         |             | PATCH     | 5/26/2017 | 11:30 | 5      | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 65  | 64      | 66      | 68      | 69      |         |           |         |             | PATCH     | 5/26/2017 | 11:49 | 4      | 3     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 66  | 40      | 41      | 68      |         |         |           |         |             | PATCH     | 5/26/2017 | 11:20 | 4      | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 67  | 39      | 40      | 68      | 69      |         |           |         |             | PATCH     | 5/26/2017 | 11:15 | 12     | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     | CAPS 39/68        |
| 68  | 38      | 39      | 69      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:59 | 10     | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     | CAPS 39/69 0'-10' |
| 69  | 70      | 72      |         |         |         |           | 21      |             | PATCH     | 5/26/2017 | 15:20 | 8      | 3     | MAY  | 60   | 6/23/2017 | WE    | AW    | Р         |     |                   |
| 70  | 71      | 72      |         |         |         |           | 9       |             | PIPE BOOT | 5/26/2017 | 16:30 | 11     | 7     | AG   | 112  | 6/24/2017 | WE    | AW    | Р         |     |                   |
| 71  | 67      | 70      | 71      | 72      |         |           |         |             | PIPE BOOT | 5/26/2017 | 14:00 | 7      | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         | 15  |                   |
| 72  | 66      | 67      | 69      | 70      |         |           |         |             | PATCH     | 5/26/2017 | 13:15 | 5      | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 73  | 66      | 67      |         |         |         |           | 120     |             | PATCH     | 5/26/2017 | 13:20 | 2      | 1     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 74  | 66      |         |         |         |         |           | 120 N   | 8 E         | PATCH     | 5/26/2017 | 13:25 | 2      | 1     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 75  | 67      |         |         |         |         |           | 25 N    | 4 E         | PATCH     | 5/26/2017 | 14:25 | 5      | 5     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 76  | 71      | 73      |         |         |         |           | 35      |             | PATCH     | 5/26/2017 | 15:24 | 2      | 8     | AG   | 112  | 5/26/2017 | WE    | AW    | Р         |     |                   |
| 77  | 73      | 74      |         |         |         |           | 33      |             | PATCH     | 5/26/2017 | 15:26 | 1      | 1     | AG   | 112  | 6/1/2017  | WE    | AW    | Р         |     |                   |
| 78  | 73      | 74      | 75      |         |         |           |         |             | PATCH     | 5/26/2017 | 15:29 | 3      | 2     | AG   | 112  | 6/1/2017  | WE    | AW    | Р         |     |                   |
| 79  | 71      | 73      |         |         |         |           | 108     |             | PATCH     | 5/26/2017 | 14:25 | 4      | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         | 16  |                   |
| 80  | 71      | 72      | 73      |         |         |           |         |             | PATCH     | 5/26/2017 | 10:13 | 2      | 1     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р         |     |                   |



| 111         29         30         WT         19         21         PATCH         5/30/2017         13:25         3         3         AG         211         5/30/2017         WE         AW         P           112         30         WT         8         10         PATCH         5/30/2017         13:15         5         2         AG         211         5/30/2017         WE         AW         P           113         30         33         WT         0         3         PATCH         5/30/2017         13:48         4         2         AG         211         5/30/2017         WE         AW         P           114         33         35         WT         0         2         PATCH         5/30/2017         13:52         2         1         AG         211         5/30/2017         WE         AW         P           115         35         36         WT         0         2         PATCH         5/30/2017         13:55         3         2         AG         211         5/30/2017         WE         AW         P           116         36         37         WT         15         18         PATCH         5/30/2017   | $\overline{}$ |         |         |         |         | N       | Marked  |         |             |       |           |       | Repair | red   |      |      |           | Teste | d     |     |     | Notes                                  |
|--|---------------|---------|---------|---------|---------|---------|---------|---------|-------------|-------|-----------|-------|--------|-------|------|------|-----------|-------|-------|-----|-----|--|
|  | um .          | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Type  | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | OA ID |     | DS# | Comments                               |
| 18   | _             |         |         |         |         |         |         |         |             | **    | <u> </u>  |       |        |       |      |      |           |       | 1     |     |     |  |
|  |               |         |         | 76      |         |         |         | -       | 0           |       |           |       |        |       |      |      |           |       |       |     |     |  |
| Mathematical Content of the conten   |               |         |         | VA/T    |         |         |         | 5       | 9           |       |           |       |        |       |      |      |           |       |       | - ' |     |  |
| 1  |               |         |         | VVI     |         |         |         | -       |             |       |           |       |        |       |      |      |           |       |       | - ' |     |  |
| 1  | -             |         |         |         |         |         |         |         | 16          |       |           |       |        |       |      |      |           |       |       |     |     |  |
| 1  |               |         |         |         |         |         |         |         |             |       |           |       |        |       |      |      |           |       |       |     |     |  |
| 1  |               |         |         |         |         |         |         | 13      | 16          |       |           |       |        |       |      |      |           |       |       |     |     |  |
| 1  |               |         |         |         |         |         |         |         |             |       |           |       |        |       |      |      |           |       |       |     |     |  |
| 1  | -             |         |         |         |         |         |         |         |             |       |           |       |        |       |      |      |           |       |       |     |     |  |
| 1  |               |         |         | 7       | WT      |         |         |         |             |       |           |       |        |       |      |      |           |       |       |     |     | CAPS 6-WT                              |
| 1  |               |         |         |         |         |         |         | 15      |             |       |           |       |        |       |      |      |           |       |       |     |     |  |
| 1  |               |         |         | WT      |         |         |         |         |             |       |           |       |        |       |      |      |           |       |       | - ' |     |  |
| 94   95   97   98   98   98   98   98   98   98  |               |         |         |         |         |         |         | 6       |             |       |           |       |        |       |      |      |           |       |       |     |     |  |
| 98   |               |         |         | WT      |         |         |         |         |             |       |           |       |        |       |      |      |           |       |       |     |     |  |
| Part      | 94            | -       | WT      |         |         |         |         | -       |             |       |           | 13:20 |        |       | AG   | 112  |           |       | AW    | - 1 |     |  |
| 98 11  |               |         |         | WT      |         |         |         |         |             |       |           |       |        |       |      |      |           |       |       |     | 15  |  |
| 98   | 96            | 10      | WT      |         |         |         |         | 6       |             | PATCH | 5/27/2017 | 13:30 | 1      | 1     | AG   | 112  | 5/30/2017 | WE    | AW    | P   |     |  |
| 1  | 97            | 10      | 11      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 13:35 | 1      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 100  | 98            | 11      | 12      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 8:30  | 6      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 101 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1  | 99            | 12      | 14      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 8:35  | 7      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 102   16   17   WT   WT   WT   WT   WT   WT   WT   W   | .00           | 14      | 15      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 8:49  | 6      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 103 17 20 WT   | .01           | 15      | 16      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 9:09  | 8      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 104   20   21  | .02           | 16      | 17      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 9:15  | 6      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 105   21   22   WT   2   0   0   4   PATCH   5/30/2017   10:35   5   2   AG   211   5/30/2017   WE   AW   P   0   0   0   0   0   0   0   0   0  | 03            | 17      | 20      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 9:45  | 6      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | P   |     |  |
| 106   22   23   WT   C   C   C   C   C   C   C   C   C   | ւ04           | 20      | 21      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 10:08 | 6      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | P   |     |  |
| 107 23 24 WT   | 05            | 21      | 22      | WT      |         |         |         | 0       | 4           | PATCH | 5/30/2017 | 10:35 | 5      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 108  | 106           | 22      | 23      | WT      |         |         |         | 0       | 5           | PATCH | 5/30/2017 | 10:55 | 6      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 109   25   WT   S   W | 107           | 23      | 24      | WT      |         |         |         | 0       | 4           | PATCH | 5/30/2017 | 11:00 | 5      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 110 26 27 29 WT  | 108           | 24      | 25      | WT      |         |         |         | 0       | 4           | PATCH | 5/30/2017 | 11:05 | 5      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | P   |     |  |
| 111 29 30 WT   | 109           | 25      | WT      |         |         |         |         | 3       | 5           | PATCH | 5/30/2017 | 11:20 | 2      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | P   |     |  |
| 112 30 WT  | 110           | 26      | 27      | 29      | WT      |         |         |         |             | PATCH | 5/30/2017 | 11:35 | 9      | 3     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     | CAPS 26-WT 0'-3'// 27-WT 0'-4'// 29-WT |
| 113 30 33 WT 8 9 0 3 PATCH 5/30/2017 13:52 2 1 AG 211 5/30/2017 WE AW P S S S S S S S S S S S S S S S S S S  | 111           | 29      | 30      | WT      |         |         |         | 19      | 21          | PATCH | 5/30/2017 | 13:25 | 3      | 3     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 114 33 35 WT   | 112           | 30      | WT      |         |         |         |         | 8       | 10          | PATCH | 5/30/2017 | 13:15 | 5      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 115 35 36 WT W W W W W W W W W W W W W W W W W W   | 113           | 30      | 33      | WT      |         |         |         | 0       | 3           | PATCH | 5/30/2017 | 13:48 | 4      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 116     36     37     WT     15     18     PATCH     5/30/2017     14:02     4     2     AG     211     5/30/2017     WE     AW     P       117     32     31     WT     0     3     PATCH     5/30/2017     13:38     4     2     AG     211     5/30/2017     WE     AW     P       118     39     40     WT     PATCH     5/30/2017     14:11     3     2     AG     211     5/30/2017     WE     AW     P  | 114           | 33      | 35      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 13:52 | 2      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 117     32     31     WT     0     3     PATCH     5/30/2017     13:38     4     2     AG     211     5/30/2017     WE     AW     P       118     39     40     WT     PATCH     5/30/2017     14:11     3     2     AG     211     5/30/2017     WE     AW     P  | 115           | 35      | 36      | WT      |         |         |         | 0       | 2           | PATCH | 5/30/2017 | 13:55 | 3      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 118 39 40 WT PATCH 5/30/2017 14:11 3 2 AG 211 5/30/2017 WE AW P  | 116           | 36      | 37      | WT      |         |         |         | 15      | 18          | PATCH | 5/30/2017 | 14:02 | 4      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
|  | 117           | 32      | 31      | WT      |         |         |         | 0       | 3           | PATCH | 5/30/2017 | 13:38 | 4      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
|  | 118           | 39      | 40      | WT      |         |         |         |         |             | PATCH | 5/30/2017 | 14:11 | 3      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 113   40   41   WI   | 119           | 40      | 41      | WT      |         |         |         | 0       | 6           | PATCH | 5/30/2017 | 14:32 | 7      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р   |     |  |
| 120 41 42 WT 0 3 PATCH 5/30/2017 14:35 4 2 AG 211 5/30/2017 WE AW P  |               |         |         |         |         |         |         |         |             |       |           |       | 4      |       |      |      |           |       |       | P   |     |  |



|     |         |         |         |           | N       | /larked |         |             |           |           |       | Repair | red   |      |      |           | Teste | d     |           |     | Notes                                       |
|-----|---------|---------|---------|-----------|---------|---------|---------|-------------|-----------|-----------|-------|--------|-------|------|------|-----------|-------|-------|-----------|-----|---|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4   | Panel 5 | Panel 6 | Station | Station End | Туре      | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /    | DS# | Comments                                    |
| 121 | 42      | 44      | WT      | 1 - 1 - 1 |         |         | 0       | 3           | PATCH     | 5/30/2017 | 14:45 | 4      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Fail<br>P |     |   |
| 122 | 44      | 47      | WT      |           |         |         | 0       | 2           | PATCH     | 5/30/2017 | 15:01 | 3      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | P         |     |   |
| 123 | 47      | 48      | WT      |           |         |         | 0       | 4           | PATCH     | 5/30/2017 | 15:14 | 5      | 3     | AG   | 211  | 5/30/2017 | WE    | AW    | P P       |     |   |
| 124 | 48      | WT      | VV I    |           |         |         | 14      | 4           | PATCH     | 5/30/2017 | 15:14 | 1      | 5     | AG   | 211  | 5/30/2017 | WE    | AW    | P         |     |   |
| 125 | 48      | 49      | WT      |           |         |         | 14      |             | PATCH     | 5/30/2017 | 15:24 | 2      | 1     | AG   | 211  | 5/30/2017 | WE    | AW    | P         |     |   |
| 126 | 50      | 51      | WT      |           |         |         | 0       | 3           | PATCH     | 5/30/2017 | 15:31 | 4      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | P         | 11  |   |
| 127 | 51      | 52      | WT      |           |         |         | 23      | 28          | PATCH     | 5/30/2017 | 15:49 | 8      | 3     | AG   | 211  | 5/30/2017 | WE    | AW    | P         | 18  |   |
| 128 | 52      | 53      | WT      |           |         |         | 23      | 20          | PATCH     | 5/30/2017 | 15:42 | 3      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | P         | 10  |   |
| 129 | 53      | WT      | ***     |           |         |         | 7       | 11          | PATCH     | 5/30/2017 | 16:02 | 3      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | P         |     |   |
| 130 | 53      | 54      | WT      |           |         |         | 54      | 22          | PATCH     | 5/30/2017 | 16:01 | 3      | 2     | MAY  | 60   | 5/30/2017 | WE    | AW    | P         |     |   |
| 131 | 54      | PS PS   | VV I    |           |         |         | 7       | 10          | PATCH     | 5/30/2017 | 15:40 | 4      | 2     | MAY  | 60   | 5/30/2017 | WE    | AW    | P         |     |   |
| 132 | 54      | 55      | PS      |           |         |         | ,       | 10          | PATCH     | 5/30/2017 | 15:35 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | AW    | P         |     |   |
| 133 | 55      | 56      | PS      |           |         |         |         |             | PATCH     | 5/30/2017 | 15:32 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | AW    | P         |     |   |
| 134 | 56      | 57      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 15:59 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 135 | 57      | 59      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 15:27 | 1      | 2     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 136 | 59      | 60      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 15:22 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 137 | 60      | 61      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 15:20 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 138 | 61      | 62      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 15:15 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 139 | 62      | 63      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 15:10 | 3      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 140 | 62      | 63      | 13      |           |         |         | 2       |             | T-CAP     | 5/26/2017 | 13:50 | 4      | 2     | AG   | 112  | 5/30/2017 | WE    | BD    | P         | 14  |   |
| 141 | 63      | 64      | PS      |           |         |         | -       |             | T-CAP     | 5/26/2017 | 15:05 | 3      | 2     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         | 14  |   |
| 142 | 64      | 66      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:57 | 2      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 143 | 66      | 67      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:55 | 2      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 144 | 67      | 71      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:53 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 145 | 71      | PS      | 13      |           |         |         | 10      |             | PATCH     | 5/30/2017 | 14:52 | 2      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 146 | 71      | 73      | PS      |           |         |         | 10      |             | T-CAP     | 5/30/2017 | 14:50 | 2      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 147 | 73      | 74      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:46 | 2      | 2     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 148 | 74      | 76      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:43 | 4      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 149 | 76      | 77      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:40 | 2      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 150 | 77      | 78      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:37 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 151 | 78      | 79      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:33 | 1      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 152 | 79      | 80      | PS      |           |         |         |         |             | T-CAP     | 5/30/2017 | 14:30 | 2      | 1     | MAY  | 60   | 5/30/2017 | WE    | BD    | P         |     |   |
| 153 | 80      | 81      | PS      |           |         |         |         |             | T-CAP     | 6/1/2017  | 12:00 | 5      | 6     | AG   | 211  | 6/2/2017  | CC    | BD    | P         |     |   |
| 154 | 81      | 82      | .5      |           |         |         | 6       |             | PIPE BOOT | 5/31/2017 | 16:24 | 4      | 5     | AG   | 211  | 6/2/2017  | cc    | BD    | P         |     |   |
| 155 | 80      | 81      | 82      |           |         |         |         |             | T-CAP     | 6/1/2017  | 11:45 | 2      | 7     | AG   | 211  | 6/2/2017  | cc    | BD    | P         |     |   |
| 156 | 80      | 82      | 83      |           |         |         |         |             | T-CAP     | 6/1/2017  | 11:31 | 3      | 1     | AG   | 211  | 6/2/2017  | cc    | BD    | P         |     |   |
| 157 | 79      | 80      | 83      |           |         |         |         |             | T-CAP     | 6/1/2017  | 11:28 | 5      | 2     | AG   | 211  | 6/2/2017  | cc    | BD    | P         |     |   |
| 158 | 83      | 55      | 00      |           |         |         |         |             | PATCH     | 6/1/2017  | 10:54 | 2      | 1     | AG   | 211  | 6/2/2017  | cc    | BD    | P         |     | SE 75 ( E from 83/84 and S from 79/83)      |
| 159 | 79      | 83      | 84      |           |         |         |         |             | T-CAP     | 6/1/2017  | 10:55 | 3      | 2     | AG   | 211  | 6/2/2017  | СС    | BD    | P         |     | 32 /3 ( E 110111 03/04 aliu 3 110111 /3/03) |
| 160 | 78      | 79      | 84      |           |         |         |         |             | T-CAP     | 6/1/2017  | 10:49 | 3      | 2     | AG   | 211  | 6/2/2017  | cc    | BD    | P         |     |   |
| 100 | 70      | 13      | 04      |           |         |         |         |             | I-CAP     | 0/1/201/  | 10.49 | 3      | 2     | AU   | 211  | 0/2/201/  | ···   | טט    | ۳         |     | l .   |



|     |         |         |         |         | N       | Marked  |         |             |           |           |       | Repair | red   |       |      |           | Teste | ed    |        |     | Notes                                  |
|-----|---------|---------|---------|---------|---------|---------|---------|-------------|-----------|-----------|-------|--------|-------|-------|------|-----------|-------|-------|--------|-----|--|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Туре      | Date      | Time  | Length | Width | Tech  | Mach | Date      | Tech  | QA ID | Pass / | DS# | Comments                               |
| 161 | 84      | 85      |         |         |         |         | 14      |             | PATCH     |           |       |        |       |       |      |           |       |       | Fail   | 19  | COVERED BY R626                        |
| 162 | 78      | 84      | 85      |         |         |         | 14      |             | T-CAP     | 6/1/2017  | 10:45 | 5      | 2     | AG    | 211  | 6/2/2017  | СС    | BD    | P      | 15  | COVERED BY ROZU                        |
| 163 | 85      | 86      | 85      |         |         |         | 16      |             | PIPE BOOT | 5/31/2017 | 15:37 | 4      | 7     | AG    | 211  | 6/2/2017  | СС    | BD    | P      |     |  |
| 164 | 78      | 85      | 86      |         |         |         | 10      |             | T-CAP     | 6/1/2017  | 10:30 | 2      | 4     | AG    | 211  | 6/2/2017  | cc    | BD    | P      |     |  |
| 165 | 86      | 05      | 00      |         |         |         |         |             | PIPE BOOT | 5/31/2017 | 15:24 | 7      | 4     | AG    | 211  | 6/2/2017  | СС    | BD    | P      |     | 100 75 (5 from 77/96 and 5 from 96/97) |
| 166 | 77      | 78      | 86      |         |         |         |         |             | T-CAP     | 6/1/2017  | 10:22 | 3      | 2     | AG    | 211  | 6/2/2017  | СС    | BD    | P      |     | 10S 7E (S from 77/86 and E from 86/87) |
| 167 | 77      | 86      | 87      |         |         |         |         |             | T-CAP     | 6/1/2017  | 10:22 | 3      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | P      |     |  |
|     |         |         |         | 00      |         |         |         |             |           |           |       |        |       |       |      |           |       |       |        |     |  |
| 168 | 76      | 77      | 87      | 88      |         |         |         |             | T-CAP     | 6/1/2017  | 10:08 | 3      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | P      |     | 4 WAY                                  |
| 169 | 76      | 88      | 89      |         |         |         |         |             | T-CAP     | 6/1/2017  | 10:03 | 3      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | P      |     |  |
| 170 | 75      | 76      | 89      |         |         |         |         |             | T-CAP     | 6/1/2017  | 9:59  | 3      | 2     | AG    | 211  | 6/1/2017  | WE    | BD    | Р      |     |  |
| 171 | 75      | 89      | 90      |         |         |         |         |             | T-CAP     | 6/1/2017  | 9:54  | 3      | 2     | AG    | 211  | 6/1/2017  | WE    | BD    | P      |     |  |
| 172 | 73      | 75      | 90      | 91      |         |         |         |             | T-CAP     | 6/1/2017  | 9:29  | 3      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | Р      | _   | 4 WAY                                  |
| 173 | 91      | 93      |         |         |         |         | 42      |             | PATCH     | -1.1      |       |        | _     |       |      | - 1: 1:   |       |       |        | 21B | COVERED BY R429                        |
| 174 | 73      | 91      | 93      |         |         |         |         |             | T-CAP     | 6/1/2017  | 9:23  | 3      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | Р      |     |  |
| 175 | 72      | 73      | 93      |         |         |         |         |             | T-CAP     | 6/1/2017  | 9:17  | 3      | 2     | AG    | 211  | 6/1/2017  | WE    | BD    | Р      |     |  |
| 176 | 72      | 93      | 94      |         |         |         |         |             | T-CAP     | 6/1/2017  | 9:10  | 3      | 2     | AG    | 211  | 6/1/2017  | WE    | BD    | Р      |     |  |
| 177 | 70      | 72      | 94      |         |         |         |         |             | T-CAP     | 6/1/2017  | 8:57  | 3      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | Р      |     |  |
| 178 | 70      | 94      |         |         |         |         | 11      |             | PATCH     | 6/1/2017  | 8:53  | 4      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | Р      |     |  |
| 179 | 38      | 69      | 70      | 94      |         |         |         |             | T-CAP     | 6/1/2017  | 8:40  | 7      | 2     | AG    | 211  | 6/1/2017  | WE    | BD    | Р      |     |  |
| 180 | 38      | 94      | 95      |         |         |         |         |             | T-CAP     | 6/1/2017  | 8:33  | 2      | 2     | AG    | 211  | 6/1/2017  | WE    | BD    | Р      |     |  |
| 181 | 36      | 38      | 95      |         |         |         |         |             | T-CAP     | 6/1/2017  | 8:28  | 3      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | Р      |     |  |
| 182 | 36      | 95      | 96      |         |         |         |         |             | T-CAP     | 6/1/2017  | 8:24  | 5      | 2     | AG    | 211  | 6/1/2017  | RX    | BD    | Р      | 22  |  |
| 183 | 95      | 96      |         |         |         |         | 160     |             | PATCH     | 6/1/2017  | 7:51  | 3      | 2     | AG    | 211  | 6/1/2017  | WE    | BD    | Р      |     |  |
| 184 | 96      |         |         |         |         |         |         |             | PIPE BOOT | 6/6/2017  | 14:52 | 6      | 5     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     | 4' S: 97 // 102' W PS                  |
| 185 | 34      | 36      | 96      |         |         |         |         |             | T-CAP     | 6/6/2017  | 15:22 | 5      | 2     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      | 8   |  |
| 186 | 34      | 96      | 97      |         |         |         |         |             | T-CAP     | 6/6/2017  | 15:26 | 6      | 3     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     |  |
| 187 | 33      | 34      | 97      |         |         |         |         |             | T-CAP     | 6/6/2017  | 15:41 | 4      | 2     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     |  |
| 188 | 30      | 97      | 99      |         |         |         |         |             | T-CAP     | 6/6/2017  | 15:45 | 4      | 1     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     |  |
| 189 | 30      | 33      | 99      |         |         |         |         |             | T-CAP     | 6/6/2017  | 15:51 | 2      | 2     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     |  |
| 190 | 30      | 99      | 100     |         |         |         |         |             | T-CAP     | 6/7/2017  | 11:00 | 2      | 2     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     |  |
| 191 | 29      | 30      | 100     |         |         |         |         |             | T-CAP     | 6/7/2017  | 10:48 | 2      | 2     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     |  |
| 192 | 29      | 100     | 101     |         |         |         |         |             | T-CAP     | 6/7/2017  | 10:54 | 3      | 3     | AG    | 211  | 6/10/2017 | WE    | BD    | Р      |     |  |
| 193 | 100     | 101     |         |         |         |         |         |             | PATCH     | 6/7/2017  | 11:36 | 4      | 2     | AG    | 211  | 6/28/2017 | PP    | AW    | Р      | 23A |  |
| 194 | 29      | 31      | 32      | 101     | 102     |         |         |             | CAP       | 6/2/2017  | 10:36 | 10     | 3     | MAY   | 60   | 6/20/2017 | WE    | BD    | Р      |     |  |
| 195 | 27      | 31      | 102     | 103     |         |         |         |             | CAP       | 6/2/2017  | 10:47 | 4      | 3     | MAY   | 60   | 6/28/2017 | PP    | AW    | Р      |     |  |
| 196 | 24      | 25      | 27      | 103     | 106     |         |         |             | CAP       | 6/2/2017  | 10:17 | 5      | 4     | MAY   | 60   | 6/10/2017 | WE    | BD    | Р      |     |  |
| 197 | 23      | 24      | 106     | 107     |         |         |         |             | CAP       | 6/2/2017  | 9:55  | 2      | 2     | MAY   | 60   | 6/10/2017 | WE    | BD    | Р      |     |  |
| 198 | 106     | 107     | 108     | 109     |         |         |         |             | CAP       | 6/2/2017  | 9:35  | 3      | 2     | MAY   | 60   | 6/10/2017 | WE    | BD    | Р      |     |  |
| 199 | 105     | 106     | 108     |         |         |         |         |             | T-CAP     | 6/2/2017  | 9:40  | 1      | 1     | MAY   | 60   | 6/10/2017 | WE    | BD    | Р      |     |  |
| 200 | 103     | 105     | 106     |         |         |         |         |             | T-CAP     | 6/2/2017  | 9:49  | 2      | 1     | MAY   | 60   | 6/24/2017 | WE    | BD    | P      |     |  |
| 200 | 102     | 100     | 100     |         |         |         |         |             | I-CAP     | 0/2/201/  | 9.49  |        | 1     | IVIAT | 60   | 0/24/201/ | VV E  | טפ    | ۳      |     |  |



|            |          |          |         |         | N         | Marked   |             |             |                    |                      |                | Repair | red   |          |          |                      | Teste    | ed       |           |       | Notes                         |
|------------|----------|----------|---------|---------|-----------|----------|-------------|-------------|--------------------|----------------------|----------------|--------|-------|----------|----------|----------------------|----------|----------|-----------|-------|-------------------------------|
| Num        | Panel 1  | Panel 2  | Panel 3 | Panel 4 | Panel 5   | Panel 6  | Station     | Station End | Туре               | Date                 | Time           | Length | Width | Tech     | Mach     | Date                 | Tech     | QA ID    | Pass /    | DS#   | Comments                      |
| 201        | 102      | 103      | 104     | 105     | l unici s | , unc. o | J. Lat.ioii | June 1      | CAP                | 6/2/2017             | 8:05           | 8      | 2     | MAY      | 60       | 6/10/2017            | WE       | BD       | Fail<br>P | 20 :: | Comments                      |
| 202        | 102      | 103      | 104     | 103     |           |          |             |             | PATCH              | 6/7/2017             | 10:43          | 2      | 9     | AG       | 211      | 6/10/2017            | WE       | BD       | P         |       | 7' W 103-105                  |
| 202        | 101      | 103      | 104     |         |           |          |             |             | T-CAP              | 6/2/2017             | 8:14           | 3      | 2     | MAY      | 60       | 6/10/2017            | WE       | BD       | P         |       | / W 103-103                   |
| 203        | 101      | 102      | 104     |         |           |          |             |             | PATCH              | 6/2/2017             | 8:52           | 5      | 6     | MAY      | 60       | 6/10/2017            | WE       | BD       | P         |       | 7' N 105// 17' E 106// TMP 27 |
| 205        | 105      | 108      |         |         |           |          |             |             | PATCH              | 6/2/2017             | 9:19           | 4      | 2     | MAY      | 60       | 6/10/2017            | WE       | BD       | P         | 24    | / N 103// 17 L 100// NWF 27   |
| 206        | 109      | 108      |         |         |           |          |             |             | PATCH              | 6/2/2017             | 9:10           | 5      | 4     | MAY      | 60       | 6/24/2017            | WE       | BD       | P         | 24    | 4 E 142 // E2 E 107 // TMD 10 |
| 207        | 97       | 98       | PS      |         |           |          |             |             | T-CAP              | 6/1/2017             | 17:00          | 2      | 2     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       | 4' E 143// 52' E 107// TMP 18 |
| 208        | 96       | 97       | гэ      |         |           |          | 13          |             | PATCH              | 6/1/2017             | 16:11          | 4      | 3     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 209        | 96       | 97       | PS      |         |           |          | 13          |             | T-CAP              | 6/1/2017             | 16:44          | 8      | 2     | AG       | 211      | 6/2/2017             | СС       | BD       | P         |       |                               |
| 210        | 96       | PS       | гэ      |         |           |          | 7           |             | PATCH              | 6/1/2017             | 16:44          | 6      | 3     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 210        | 95       | 96       | PS      |         |           |          | ,           |             | T-CAP              | 6/1/2017             | 15:34          | 2      | 1     | AG       | 211      | 6/2/2017             | cc       | BD       | P         |       |                               |
| 211        | 95       | 96       | rs      |         |           |          | 9           |             | PATCH              | 6/1/2017             | 15:59          | 3      | 2     | AG       | 211      | 6/2/2017             | СС       | BD       | P         |       |                               |
| 212        | 95       | PS       |         |         |           |          | 14          |             | PATCH              | 6/1/2017             | 15:34          | 2      | 2     | AG       | 211      | 6/2/2017             | СС       | BD       | P         |       |                               |
| 213        | 92       | 95       | PS      |         |           |          | 14          |             | T-CAP              | 6/1/2017             | 15:21          | 2      | 2     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 215        | 92       | 94       | гэ      |         |           |          | 3           |             | PATCH              | 6/1/2017             | 14:38          | 4      | 2     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 216        | 92       | PS PS    |         |         |           |          | 10          |             | PATCH              | 6/1/2017             | 14:38          | 2      | 1     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 217        | 92       | PS PS    |         |         |           |          | 5           |             | PIPE BOOT          | 6/1/2017             | 14:32          | 7      | 6     | AG       | 211      | 6/2/2017             | cc       | BD       | P         |       |                               |
| 217        | 91       | 93       | PS      |         |           |          | 3           |             | T-CAP              | 6/1/2017             | 14:31          | 2      | 2     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 219        | 91       | PS       | гэ      |         |           |          | 10          |             | PATCH              | 6/1/2017             | 14:30          | 3      | 1     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 220        | 90       | 91       | PS      |         |           |          | 10          |             | T-CAP              | 6/1/2017             | 10:32          | 2      | 2     | MAY      | 60       | 6/2/2017             | cc       | BD       | P         |       |                               |
| 221        | 89       | 90       | PS      |         |           |          |             |             | T-CAP              | 6/1/2017             | 14:00          | 2      | 1     | AG       | 211      | 6/2/2017             | cc       | BD       | P         |       |                               |
| 222        | 89       | PS       | rs      |         |           |          | 6           |             | PATCH              | 6/1/2017             | 13:46          | 4      | 3     | AG       | 211      | 6/2/2017             | СС       | BD       | P         |       |                               |
| 223        | 88       | 89       | PS      |         |           |          | 0           |             | T-CAP              | 6/1/2017             | 13:40          | 2      | 2     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 224        | 87       | 88       | PS      |         |           |          |             |             | T-CAP              | 6/1/2017             |                | 2      | 1     |          |          | 6/2/2017             | СС       | BD       | P         |       |                               |
| 225        | 87       | 88       | P3      |         |           |          | 77          |             | PATCH              |                      | 10:07<br>17:06 | 3      | 2     | AG<br>AG | 211      |                      | CC       | BD       | P         |       |                               |
|            |          |          |         |         |           |          | 58          |             |                    | 5/31/2017            |                |        |       |          |          | 6/2/2017             |          |          | P         |       |                               |
| 226        | 87       | 88       |         |         |           |          |             |             | PATCH              | 5/31/2017            | 17:03          | 3      | 3     | AG       | 211      | 6/2/2017             | CC       | BD       |           |       |                               |
| 227        | 86       | 87       | DC.     |         |           |          | 67          |             | PATCH              | 5/31/2017            | 15:54          | 4      | 2     | AG       | 211      | 6/2/2017             | CC       | BD       | P         |       |                               |
| 228<br>229 | 86<br>86 | 87<br>PS | PS      |         |           |          | 11          |             | PIPE BOOT  PATCH   | 6/1/2017<br>6/1/2017 | 9:58           | 6      | 3     | MAY      | 60<br>60 | 6/2/2017<br>6/2/2017 | cc       | BD<br>BD | P<br>P    |       |                               |
| 230        | 86       |          |         |         |           |          |             |             | PATCH<br>PIPE BOOT | 6/1/2017             | 9:30           | 5      | 3     | MAY      |          |                      | CC       |          | P         |       |                               |
| 230        | 85       | PS<br>86 | PS      |         |           |          | 5           |             | T-CAP              | 6/1/2017             | 9:17           | 1      |       | MAY      | 60<br>60 | 6/2/2017<br>6/2/2017 |          | BD<br>BD | P         |       |                               |
| 231        | 85<br>85 | 86       | 12      |         |           |          | 56          |             |                    | 5/31/2017            | 9:05           | 3      | 2     |          |          | 6/2/2017             | CC<br>WE |          | P         |       |                               |
|            |          |          |         |         |           |          |             |             | PATCH              |                      | 15:49          |        |       | AG       | 211      |                      |          | BD       |           |       |                               |
| 233        | 85       | 86       | DC      |         |           |          | 41          |             | PATCH              | 5/31/2017            | 15:43          | 4      | 2     | AG       | 211      | 6/1/2017             | WE       | BD       | P<br>P    |       |                               |
| 234        | 84       | 85       | PS      |         |           |          |             |             | T-CAP              | 6/1/2017             | 8:56           | 1      | 1     | MAY      | 60       | 6/2/2017             | CC       | BD       |           |       |                               |
| 235        | 83       | 84       | PS      |         |           |          | 42          |             | T-CAP              | 6/1/2017             | 8:13           | 1      | 1     | MAY      | 60       | 6/2/2017             | CC       | BD       | P         |       |                               |
| 236        | 83       | PS       |         |         |           |          | 13          |             | PATCH              | 6/1/2017             | 8:12           | 3      | 2     | MAY      | 60       | 6/2/2017             | CC       | BD       | P<br>P    |       |                               |
| 237        | 82       | 83       | DC.     |         |           |          | 28          |             | PATCH              | 5/31/2017            | 16:00          | 3      | 2     | AG       | 211      | 6/2/2017             | CC       | BD       |           |       |                               |
| 238        | 82       | 83       | PS      |         |           |          |             |             | T-CAP              | 6/1/2017             | 8:08           | 2      | 2     | MAY      | 60       | 6/2/2017             | CC       | BD       | P         |       |                               |
| 239        | 82       | PS       |         |         |           |          | 17          |             | PATCH              | 6/1/2017             | 8:06           | 4      | 4     | MAY      | 60       | 6/2/2017             | CC       | BD       | P         |       |                               |
| 240        | 82       | PS       |         |         |           |          | 10          |             | PATCH              | 6/1/2017             | 8:00           | 2      | 1     | MAY      | 60       | 6/2/2017             | CC       | BD       | Р         |       |                               |



|     |         |         |         |         | N          | /larked   |         |             |         |           |       | Repair    | red       |      |      |           | Teste    | ed          |        |     | Notes    |
|-----|---------|---------|---------|---------|------------|-----------|---------|-------------|---------|-----------|-------|-----------|-----------|------|------|-----------|----------|-------------|--------|-----|----------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5    | Panel 6   | Station | Station End | Туре    | Date      | Time  | Length    | Width     | Tech | Mach | Date      | Tech     | QA ID       | Pass / | DS# | Comments |
| 241 | 82      | PS      |         |         |            |           | 3       |             | PATCH   | 5/31/2017 | 16:46 | 4         | 1         | AG   | 211  | 6/2/2017  | СС       | BD          | Fail   |     | 1        |
| 241 | 81      | 82      | PS      |         |            |           | ,       |             | T-CAP   | 5/31/2017 | 16:36 | 3         | 2         | AG   | 211  | 6/2/2017  | cc       | BD          | P      |     |          |
| 243 | 110     | PS      | 137     |         |            |           | 0       |             | PATCH   | 6/6/2017  | 13:55 | 2         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | P      |     |          |
| 244 | 110     | .5      | 157     |         |            |           | Ü       |             | 7711611 | 0/0/201/  | 10.55 | -         | -         | 7.0  |      | 0/10/201/ | ***      | 7.00        |        |     |          |
| 245 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 246 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 247 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 248 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 249 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 250 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 251 |         |         |         | S       | EE PANEL L | AYOUT DIA | GRAM    |             |         |           | SEE   | PANEL SEA | MING LOGS |      |      | SEE NON   | -DESTRUC | TIVE TEST I | LOGS   |     |          |
| 252 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 253 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 254 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 255 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 256 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 257 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 258 |         |         |         |         |            |           |         |             |         |           |       |           |           |      |      |           |          |             |        |     |          |
| 259 | 136     | 210     | 211     |         |            |           |         |             | PATCH   | 6/13/2017 |       | 2         | 2         | AG   | 112  | 6/18/2017 | WE       | AW          | Р      |     |          |
| 260 | 136     | 139     | 140     |         |            |           |         |             | PATCH   | 6/6/2017  | 10:55 | 2         | 1         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 261 | 136     | 140     | 141     |         |            |           |         |             | PATCH   | 6/6/2017  | 11:00 | 2         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 262 | 136     | 211     | 212     |         |            |           |         |             | PATCH   | 6/13/2017 | 16:45 | 2         | 2         | AG   | 112  | 6/16/2017 | WE       | AW          | Р      |     |          |
| 263 | 136     | 212     | 213     |         |            |           |         |             | PATCH   | 6/13/2017 | 16:57 | 3         | 2         | AG   | 112  | 6/16/2017 | WE       | AW          | Р      |     |          |
| 264 | 136     | 213     | 214     |         |            |           |         |             | PATCH   | 6/13/2017 | 17:04 | 2         | 2         | AG   | 112  | 6/16/2017 | WE       | AW          | P      |     |          |
| 265 | 136     | 141     | 142     |         |            |           |         |             | PATCH   | 6/6/2017  | 11:04 | 1         | 1         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 266 | 136     | 142     |         |         |            |           | 6       |             | PATCH   | 6/13/2017 | 17:07 | 2         | 2         | AG   | 112  | 6/28/2017 | PP       | AW          | Р      |     |          |
| 267 | 141     |         |         |         |            |           | 24' N   | 4' W        | PATCH   | 6/6/2017  | 11:32 | 4         | 4         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 268 | 138     | 139     |         |         |            |           | 38      |             | PATCH   | 6/6/2017  | 10:56 | 1         | 1         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 269 | 138     | 139     |         |         |            |           | 40      | 45          | PATCH   | 6/14/2017 | 7:27  | 5         | 2         | AG   | 112  | 6/16/2017 | WE       | AW          | Р      |     |          |
| 270 | 110     | 137     |         |         |            |           | 78      |             | PATCH   | 6/6/2017  | 9:55  | 2         | 1         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 271 | 116     | 117     | 118     |         |            |           |         |             | PATCH   | 6/6/2017  | 9:42  | 2         | 1         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 272 | 272     | 117     | 118     | 119     |            |           |         |             | PATCH   | 6/6/2017  | 9:32  | 2         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 273 | 120     | 121     |         |         |            |           | 3       |             | PATCH   | 6/6/2017  | 9:38  | 3         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 274 | 124     | 125     |         |         |            |           | 16      |             | PATCH   | 6/6/2017  | 9:00  | 4         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 275 | 130     | 131     |         |         |            |           | 34      | 41          | Bead    | 6/6/2017  | 8:44  | 7         | 8         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 276 | 132     | 139     | 134     |         |            |           | 34      | 41          | PATCH   | 6/6/2017  | 8:48  | 3         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |
| 277 | 135     | EX      |         |         |            |           | CORNER  |             | PATCH   | 6/6/2017  | 8:50  | 4         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | P      |     |          |
| 278 | 134     | 135     | EX      |         |            |           |         |             | PATCH   | 6/6/2017  | 8:54  | 2         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | P      |     |          |
| 279 | 133     | 134     | EX      |         |            |           |         |             | PATCH   | 6/6/2017  | 8:57  | 5         | 2         | AG   | 211  | 6/10/2017 | WE       | AW          | Р      |     |          |



|     |         |         |         |           |         | // Aarked |         |              |       |           |       | Repai  | red   |      |      |           | Teste | d     |        |      | Notes      |
|-----|---------|---------|---------|-----------|---------|-----------|---------|--------------|-------|-----------|-------|--------|-------|------|------|-----------|-------|-------|--------|------|------------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4   | Panel 5 | Panel 6   | Station | Station End  | Туре  | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass / | DS#  | Comments   |
|     |         |         | Tanci 3 | T dilei 4 | Tanet 3 | 1 dilei 0 |         | Station Life | 11    |           |       |        |       |      |      |           |       |       | Fail   | D3 # | Comments   |
| 280 | 133     | 134     |         |           |         |           | 17      |              | PATCH | 6/6/2017  | 9:05  | 3      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | P      |      |            |
| 281 | 132     | 133     |         |           |         |           | 18      |              | PATCH | 6/6/2017  | 9:13  | 2      | 1     | AG   | 211  | 6/10/2017 | WE    | AW    | P      |      |            |
| 282 | 132     | 133     | PS      |           |         |           |         |              | PATCH | 6/6/2017  | 9:18  | 1      | 1     | AG   | 211  | 6/10/2017 | WE    | AW    | P      |      |            |
| 283 | 131     | 132     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 16:49 | 6      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | P      | 40   |            |
| 284 | 130     | 131     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 16:40 | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | P      |      |            |
| 285 | 129     | 130     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 16:30 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | P      |      |            |
| 286 | 127     | 129     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 16:20 | 2      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | P      |      |            |
| 287 | 128     | 127     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 16:12 | 2      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 288 | 126     | 128     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 16:02 | 2      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 289 | 126     | 127     | 128     |           |         |           |         |              | PATCH | 6/3/2017  | 15:45 | 7      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      | 27   |            |
| 290 | 125     | 126     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 15:38 | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 291 | 124     | 125     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 15:15 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 292 | 123     | 124     | PS      |           |         |           | 0       | 9            | PATCH | 6/3/2017  | 15:03 | 10     | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      | 0-9 ON 125 |
| 293 | 122     | 123     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 14:34 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 294 | 121     | 122     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 14:02 | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 295 | 121     | 122     |         |           |         |           | 22      |              | PATCH | 6/6/2017  | 9:23  | 3      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      | 26   |            |
| 296 | 120     | 121     |         |           |         |           | 61      |              | PATCH | 6/3/2017  | 13:52 | 3      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 297 | 120     | 121     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 13:45 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 298 | 119     | 120     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 13:35 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 299 | 117     | 119     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 11:44 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 300 | 116     | 117     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 11:35 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 301 | 115     | 116     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 11:22 | 2      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 302 | 114     | 115     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 11:10 | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 303 | 113     | 114     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 10:36 | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 304 | 112     | 113     | PS      |           |         |           |         |              | PATCH | 6/3/2017  | 10:28 | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 305 | 137     | 209     | PS      |           |         |           | 0       | 13           | T-CAP | 6/6/2017  | 13:41 | 13     | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      |      |            |
| 306 | 110     | 111     |         |           |         |           | 27      |              | PATCH | 6/6/2017  | 10:01 | 2      | 1     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      |      |            |
| 307 | 110     | 111     | PS      |           |         |           | 0       |              | PATCH | 6/3/2017  | 9:59  | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 308 | 110     | 111     |         |           |         |           | 72      |              | PATCH | 6/3/2017  | 10:01 | 2      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 309 | 111     | PS      |         |           |         |           | 6       |              | PATCH | 6/3/2017  | 10:19 | 1      | 1     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 310 | 111     | 112     | PS      |           |         |           | 66      |              | PATCH | 6/3/2017  | 10:25 | 2      | 2     | AG   | 83   | 6/10/2017 | WE    | AW    | Р      |      |            |
| 311 | 110     | 111     |         |           |         |           | 60      |              | PATCH | 6/6/2017  | 10:26 | 3      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      |      |            |
| 312 | 110     | 137     |         |           |         |           | 24      |              | PATCH | 6/6/2017  | 10:25 | 2      | 1     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      |      |            |
| 313 | 110     | 137     |         |           |         |           | 38      |              | PATCH | 6/6/2017  | 10:25 | 2      | 1     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      |      |            |
| 314 | 137     | 209     |         |           |         |           | CORNER  |              | PATCH | 6/13/2017 | 16:23 | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р      |      |            |
| 315 | 136     | 137     | 209     |           |         |           |         |              | PATCH | 6/13/2017 | 16:30 | 3      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р      |      |            |
| 316 | 136     | 209     | 210     |           |         |           |         |              | PATCH | 6/13/2017 | 16:36 | 3      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р      |      |            |
| 317 | 136     | 137     | 138     |           |         |           |         |              | PATCH | 6/6/2017  | 10:30 | 3      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      |      |            |
| 318 | 138     | 139     |         |           |         |           | 15      | 20           | PATCH | 6/6/2017  | 10:45 | 5      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      | 41   |            |
| 319 | 136     | 138     | 139     |           |         |           |         |              | PATCH | 6/6/2017  | 10:40 | 1      | 1     | AG   | 211  | 6/10/2017 | WE    | AW    | Р      |      |            |



|            |         |         |         |         | N          | // Aarked |         |              |                |           |       | Repai  | red   |      |      |           | Teste    | d     |        |     | Notes      |
|------------|---------|---------|---------|---------|------------|-----------|---------|--------------|----------------|-----------|-------|--------|-------|------|------|-----------|----------|-------|--------|-----|------------|
| Num        | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5    | Panel 6   | Station | Station End  | Туре           | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech     | QA ID | Pass / | DS# | Comments   |
| 220        | 22      |         | 107     |         | T direct 5 | T dine: 0 |         | Station Line | PATCH          |           |       | 5      |       |      |      |           |          |       | Fail   |     | I comments |
| 320        | 22      | 23      | 107     | 143     |            |           | 14      |              | PATCH          | 6/7/2017  | 11:44 |        | 3     | AG   | 211  | 6/10/2017 | WE       | AW    | P      | 20  |            |
| 321        |         | 143     | 142     | 144     |            |           | 14      |              |                | 6/23/2017 | 9:48  | 5      | 2     | AG   | 211  | 6/23/2017 | WE       | AW    | P      | 30  |            |
| 322<br>323 | 21      | 22      | 143     | 144     |            |           |         |              | PATCH<br>PATCH | 6/7/2017  | 13:19 | 5      | 2     | AG   | 112  | 6/10/2017 | WE<br>WE | AW    | P      |     |            |
|            |         |         | 144     | 146     |            |           | 05      | 400          |                | 6/7/2017  | 13:29 |        |       | AG   | 112  | 6/10/2017 |          | AW    |        | 20  |            |
| 324        | 144     | 146     |         |         |            |           | 95      | 100          | PATCH          | 6/10/2017 | 13:14 | 5      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | P      | 28  |            |
| 325        | 143     | 144     | 440     |         |            |           | 113     | 115          | PATCH          | 6/10/2017 | 13:10 | 2      | 1     | AG   | 112  | 6/16/2017 | BS       | AW    | P      |     |            |
| 326        | 107     | 109     | 143     |         |            |           |         |              | PATCH          | 6/10/2017 | 13:06 | 2      | 1     | AG   | 112  | 6/16/2017 | BS       | AW    | P      |     |            |
| 327        | 107     | 109     |         |         |            |           | 7       | 10           | PATCH          | 6/2/2017  | 9:30  | 3      | 2     | AG   | 211  | 6/10/2017 | WE       | AW    | P      | 25  |            |
| 328        | 107     | 109     |         |         |            |           | 10      | 12           | PATCH          | 6/10/2017 | 12:58 | 2      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | P      |     |            |
| 329        | 109     | 143     |         |         |            |           | 52      | 53           | PATCH          | 6/10/2017 | 13:21 | 2      | 4     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 330        | 109     | 143     |         |         |            |           | 99      | 104          | PIPE BOOT      | 6/10/2017 | 13:23 | 5      | 3     | AG   | 112  | 6/28/2017 | PP       | AW    | Р      |     |            |
| 331        | 144     | 145     | 146     |         |            |           |         |              | PATCH          | 6/7/2017  | 16:47 | 3      | 2     | AG   | 112  | 6/28/2017 | PP       | AW    | Р      |     |            |
| 332        | 105     | 108     |         |         |            |           | 122     | 126          | PATCH          | 6/2/2017  | 15:03 | 6      | 4     | AG   | 83   | 6/28/2017 | PP       | AW    | Р      |     |            |
| 333        | 109     |         |         |         |            |           | 7' N    | 124' E       | PATCH          | 6/2/2017  | 15:24 | 1      | 1     | AG   | 83   | 6/16/2017 | BS       | AW    | Р      |     |            |
| 334        | 143     |         |         |         |            |           | 8' N    | 168' E       | PATCH          | 6/7/2017  | 17:02 | 2      | 1     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 335        | 143     | PS      |         |         |            |           |         |              | PIPE BOOT      | 6/7/2017  | 13:32 | 7      | 8     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 336        | 17      | 20      | 146     | 148     |            |           |         |              | PATCH          | 6/7/2017  | 13:57 | 3      | 2     | AG   | 112  | 6/10/2017 | WE       | AW    | Р      |     |            |
| 337        | 16      | 17      | 146     | 148     |            |           |         |              | PATCH          | 6/7/2017  | 14:02 | 2      | 2     | AG   | 112  | 6/10/2017 | WE       | AW    | Р      |     |            |
| 338        | 15      | 16      | 149     | 150     |            |           |         |              | PIPE BOOT      | 6/7/2017  | 14:24 | 7      | 6     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 339        | 150     | 338     |         |         |            |           |         |              | PIPE BOOT      | 6/7/2017  | 14:24 | 4      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 340        | 149     | 150     | PE2     |         |            |           |         |              | PATCH          | 6/6/2017  | 17:40 | 3      | 2     | AG   | 211  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 341        | 148     | 149     | PE2     |         |            |           |         |              | PATCH          | 6/6/2017  | 17:01 | 4      | 2     | AG   | 211  | 6/10/2017 | WE       | AW    | Р      |     |            |
| 342        | 148     | PE1     | PE2     |         |            |           |         |              | PATCH          | 6/6/2017  | 17:05 | 1      | 1     | AG   | 211  | 6/16/2017 | PP       | AW    | Р      |     |            |
| 343        | 147     | 148     | PE1     |         |            |           |         |              | PATCH          | 6/6/2017  | 17:25 | 1      | 1     | AG   | 211  | 6/16/2017 | PP       | AW    | Р      |     |            |
| 344        | 146     | 147     | 148     |         |            |           |         |              | PATCH          | 6/6/2017  | 17:20 | 3      | 2     | AG   | 211  | 6/16/2017 | PP       | AW    | Р      |     |            |
| 345        | 147     | 151     | PE1     |         |            |           |         |              | PATCH          | 6/6/2017  | 17:30 | 4      | 3     | AG   | 211  | 6/16/2017 | PP       | AW    | Р      |     |            |
| 346        | 150     | 151     | PE1     | PE2     |            |           |         |              | PATCH          | 6/6/2017  | 17:34 | 5      | 2     | AG   | 211  | 6/16/2017 | PP       | AW    | Р      |     |            |
| 347        | 14      | 15      | 150     | 151     |            |           |         |              | PATCH          | 6/7/2017  | 14:40 | 3      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 348        | 14      | 15      | R347    |         |            |           |         |              | PATCH          | 6/7/2017  | 14:42 | 3      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      | 4   |            |
| 349        | 141     | 151     | 152     |         |            |           |         |              | PATCH          | 6/7/2017  | 15:36 | 3      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 350        | 147     | 152     |         |         |            |           | 14      |              | PATCH          | 6/7/2017  | 15:39 | 2      | 1     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 351        | 146     | 147     | 152     |         |            |           |         |              | PATCH          | 6/7/2017  | 16:22 | 4      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 352        | 152     | 153     |         |         |            |           | 22      | 27           | PIPE BOOT      | 6/7/2017  | 16:38 | 6      | 4     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 353        | 146     | 152     | 153     |         |            |           |         |              | PATCH          | 6/7/2017  | 16:48 | 2      | 1     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 354        | 145     | 146     | 153     |         |            |           |         |              | PATCH          | 6/7/2017  | 16:52 | 2      | 1     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 355        | 145     | 153     | 155     |         |            |           |         |              | PATCH          | 6/7/2017  | 16:55 | 2      | 1     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 356        | 155     | 156     |         |         |            |           | 38      | 42           | PATCH          | 6/10/2017 | 13:48 | 4      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 357        | 155     | 156     |         |         |            |           | 65      | 68           | PATCH          | 6/10/2017 | 13:40 | 3      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      |     |            |
| 358        | 152     | 153     |         |         |            |           | 56      | 62           | PATCH          | 6/10/2017 | 13:54 | 6      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      | 29  |            |
| 359        | 155     | 156     |         |         |            |           | 147     |              | PATCH          |           | 14:04 | 6      | 2     | AG   | 112  | 6/16/2017 | BS       | AW    | Р      | 31  |            |



|     |         |         |            |         | N       | Marked  |         |             |           |                      |       | Repair | red   |          |            |                        | Teste | d     |           |     | Notes    |
|-----|---------|---------|------------|---------|---------|---------|---------|-------------|-----------|----------------------|-------|--------|-------|----------|------------|------------------------|-------|-------|-----------|-----|----------|
| Num | Panel 1 | Panel 2 | Panel 3    | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Type      | Date                 | Time  | Length | Width | Tech     | Mach       | Date                   | Tech  | QA ID | Pass /    | DS# | Comments |
| 360 | 153     | 154     | 155        |         |         |         |         |             | PATCH     | <u> </u>             | 15:24 |        |       |          |            |                        | BS    |       | Fail<br>P |     |          |
| 361 | 153     | 154     | 155        |         |         |         |         |             | PATCH     | 6/7/2017             | 15:24 | 2      | 3     | AG<br>AG | 112<br>112 | 6/16/2017              | BS    | AW    | P         |     |          |
| 362 | 13      |         |            | 152     |         |         |         |             | PATCH     | 6/7/2017<br>6/7/2017 | 14:50 | 9      | 3     |          | 112        | 6/16/2017<br>6/16/2017 | BS    | AW    | P         | 3   |          |
| 363 | 11      | 14      | 151<br>152 | 154     |         |         |         |             | PATCH     | 6/7/2017             | 15:03 | 4      | 2     | AG<br>AG | 112        | 6/16/2017              | BS    | AW    | P         | 3   |          |
| 364 | 10      | 11      | 154        | 155     |         |         |         |             | PATCH     | 6/7/2017             | 15:21 | 5      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
| 365 | 9       | 10      | 155        | 155     |         |         |         |             | PATCH     | 6/10/2017            | 16:45 | 2      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
| 366 | 9       | 155     | 156        |         |         |         |         |             | PATCH     | 6/10/2017            | 16:41 | 3      | 3     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
|     |         |         |            |         |         |         |         |             |           |                      |       |        |       |          |            |                        |       |       |           |     |          |
| 367 | 8       | 9       | 156        |         |         |         |         |             | PATCH     | 6/10/2017            | 16:37 | 7      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
| 368 | 8       | 156     | 158        | 150     |         |         |         |             | PATCH     | 6/10/2017            | 16:41 | 3      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
| 369 | 7       | 8       | 158        | 159     |         |         |         |             | PATCH     | 6/10/2017            | 16:21 | 1      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
| 370 | 7       | 158     | 159        |         |         |         |         |             | PATCH     | 6/10/2017            | 16:17 | 1      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
| 371 | 6       | 7       | 159        | 161     |         |         |         |             | PATCH     | 6/10/2017            | 16:14 | 9      | 3     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 372 | 6       | 159     | 161        |         |         |         |         |             | PATCH     | 6/10/2017            | 16:02 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | P         |     |          |
| 373 | 159     | 161     | 160        |         |         |         |         |             | PATCH     | 6/10/2017            | 16:04 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 374 | 158     | 159     |            |         |         |         | 99      |             | PATCH     | 6/10/2017            | 14:14 | 6      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         | 32  |          |
| 375 | 157     | 158     | 159        |         |         |         |         |             | PATCH     | 6/10/2017            | 14:22 | 3      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 376 | 156     | 157     | 158        |         |         |         |         |             | PATCH     | 6/10/2017            | 14:18 | 2      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 377 | 162     | 163     | 170        |         |         |         |         |             | PATCH     | 6/10/2017            | 14:30 | 6      | 3     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 378 | 162     | 163     |            |         |         |         | 55      | 57          | PIPE BOOT | 6/27/2017            | 11:25 | 6      | 8     | WL       | 15         | 6/27/2017              | PP    | AW    | Р         |     |          |
| 379 | 160     | 162     |            |         |         |         | 163     | 169         | PIPE BOOT | 6/16/2017            | 10:43 | 6      | 8     | WL       | 211        | 6/19/2017              | BS    | AW    | Р         |     |          |
| 380 | 163     | 164     | 165        |         |         |         |         |             | PATCH     | 6/10/2017            | 14:52 | 4      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 381 | 160     | 161     | 162        |         |         |         |         |             | PATCH     | 6/10/2017            | 16:07 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 382 | 5       | 6       | 161        | 162     |         |         |         |             | PATCH     | 6/10/2017            | 15:58 | 8      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 383 | 5       |         |            |         |         |         | 53 E    | 11 N        | PATCH     | 6/10/2017            | 16:54 | 1      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 384 | 4       | 5       | 162        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:50 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 385 | 4       | 162     | 163        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:48 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 386 | 3       | 4       | 163        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:43 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 387 | 3       | 165     | 165        |         |         |         |         |             | PATCH     | 6/12/2017            | 10:41 | 8      | 4     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 388 | 2       | 3       | 165        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:38 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 389 | 2       | 165     | 166        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:34 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 390 | 1       | 2       | 166        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:31 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 391 | 1       | 16      | 167        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:24 | 4      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 392 | 1       | 19      | 167        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:14 | 2      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 393 | 19      | 167     | 169        |         |         |         |         |             | PATCH     | 6/10/2017            | 15:11 | 4      | 8     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 394 | 18      | 19      |            |         |         |         | 5       | 12          | PATCH     | 6/12/2017            | 9:42  | 7      | 5     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 395 | 165     |         |            |         |         |         | 12 W    | 11 N        | PATCH     | 6/10/2017            | 15:05 | 1      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 396 | 165     |         |            |         |         |         | 5 W     | 11 N        | PATCH     | 6/10/2017            | 14:54 | 2      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 397 | 164     | 165     | 166        |         |         |         |         |             | PATCH     | 6/10/2017            | 14:56 | 2      | 1     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |
| 398 | 167     | 168     |            |         |         |         | 4       |             | PATCH     | 6/12/2017            | 10:48 | 5      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         | 33  |          |
| 399 | 167     | 168     | 170        |         |         |         |         |             | PATCH     | 6/12/2017            | 10:51 | 3      | 2     | AG       | 112        | 6/16/2017              | BS    | AW    | Р         |     |          |



|     |         |         |         |         | N       | /larked |         |             |           |           |       | Repair | red   |      |      |           | Teste | d     |           |     | Notes        |
|-----|---------|---------|---------|---------|---------|---------|---------|-------------|-----------|-----------|-------|--------|-------|------|------|-----------|-------|-------|-----------|-----|--------------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Type      | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /    | DS# | Comments     |
| 400 | 166     | 167     | 170     |         |         |         |         |             | PATCH     | 6/10/2017 | 14:45 | 3      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Fail<br>P |     | <u> </u>     |
| 401 | 164     | 166     | 170     |         |         |         |         |             | PATCH     | 6/10/2017 | 14:40 | 2      | 1     | AG   | 112  | 6/16/2017 | BS    | AW    | P         |     |              |
| 402 | 163     | 164     | 170     |         |         |         |         |             | PATCH     | 6/10/2017 | 14:34 | 2      | 1     | AG   | 112  | 6/16/2017 | BS    | AW    | P         |     |              |
| 403 | 171     | 179     | 181     |         |         |         |         |             | PATCH     | 6/12/2017 | 13:30 | 3      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | P         |     |              |
| 404 | 171     | 179     | -       |         |         |         | 6       |             | PATCH     | 6/12/2017 | 13:26 | 5      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         |     |              |
| 405 | 171     | 173     | 179     |         |         |         |         |             | PATCH     | 6/12/2017 | 13:16 | 3      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | P         |     |              |
| 406 | 173     | 179     | -       |         |         |         | 15      |             | PATCH     | 6/12/2017 | 11:46 | 5      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         | 35  |              |
| 407 | 173     | 174     | 179     |         |         |         |         |             | PATCH     | 6/12/2017 | 11:53 | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         |     |              |
| 408 | 170     | 171     | -       |         |         |         | 121     |             | PATCH     | 6/12/2017 | 11:39 | 6      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | P         | 34  |              |
| 409 | 171     | 172     | 173     |         |         |         | 121     |             | PATCH     | 6/12/2017 | 10:57 | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         | -   |              |
| 410 | 172     | 173     | 174     |         |         |         |         |             | PATCH     | 6/12/2017 | 11:02 | 2      | 1     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         |     |              |
| 411 | 169     | 170     | 178     |         |         |         |         |             | PATCH     | 6/12/2017 | 8:52  | 6      | 6     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         |     |              |
| 412 | 169     | 178     |         |         |         |         | 5       |             | PATCH     | 6/12/2017 | 8:44  | 2      | 1     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         |     |              |
| 413 | 168     | 169     | 170     |         |         |         |         |             | PATCH     | 6/12/2017 | 10:45 | 2      | 1     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         |     |              |
| 414 | 175     | 176     | 179     |         |         |         |         |             | PATCH     | 6/12/2017 | 11:26 | 3      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 415 | 174     | 175     | 179     |         |         |         |         |             | PATCH     | 6/12/2017 | 11:31 | 2      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 416 | 176     | 179     | 180     |         |         |         |         |             | PATCH     | 6/12/2017 | 11:16 | 5      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 417 | 176     | 178     | 180     |         |         |         |         |             | PATCH     | 6/12/2017 | 11:11 | 4      | 4     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 418 | 179     | 180     |         |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 10:58 | 10     | 5     | WL   | 15   | 6/27/2017 | PP    | AW    | Р         |     |              |
| 419 | 179     | 180     | 181     |         |         |         |         |             | PATCH     | 6/12/2017 | 11:21 | 3      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 420 | 181     | 183     | PE3     |         |         |         |         |             | PATCH     | 6/12/2017 | 16:18 | 5      | 3     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 421 | 183     | 186     | PE3     |         |         |         |         |             | PATCH     | 6/12/2017 | 15:37 | 4      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 422 | 182     | 185     | 186     | PE3     |         |         |         |             | PATCH     | 6/12/2017 | 15:11 | 9      | 6     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 423 | 181     | 182     | PE3     |         |         |         |         |             | PATCH     | 6/12/2017 | 15:49 | 4      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 424 | 189     | 182     | 184     | 185     |         |         |         |             | PIPE BOOT | 6/27/2017 | 9:47  | 16     | 10    | AG   | 112  | 6/27/2017 | PP    | AW    | Р         |     | CAPS 182/184 |
| 425 | 179     | 181     |         |         |         |         |         |             | PATCH     | 6/12/2017 | 13:22 | 6      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         | 38  |              |
| 426 | 184     | 185     | PS      | R247    | R248    |         |         |             | PATCH     | 6/20/2017 | 14:32 | 3      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |     |              |
| 427 | 171     | 184     | R258    | R248    | R249    | PS      |         |             | PATCH     | 6/20/2017 | 14:06 | 6      | 3     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |     |              |
| 428 | 185     | 190     | R247    |         |         |         |         |             | PATCH     | 6/20/2017 | 14:44 | 2      | 1     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |     |              |
| 429 | 190     | 191     | R247    |         |         |         |         |             | PATCH     | 6/20/2017 | 14:48 | 2      | 1     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |     |              |
| 430 | 191     | R246    | R247    | PS      |         |         |         |             | PATCH     | 6/20/2017 | 14:52 | 3      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |     |              |
| 431 | R246    | PS      |         |         |         |         |         |             | PATCH     | 6/20/2017 | 15:00 | 3      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |     |              |
| 432 | 191     | 193     | R245    | R246    | PS      |         |         |             | PATCH     | 6/20/2017 | 15:08 | 3      | 3     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |     |              |
| 433 | 185     | 189     | 190     |         |         |         |         |             | PATCH     | 6/20/2017 | 16:58 | 5      | 2     | BS   | 15   | 6/27/2017 | PP    | AW    | Р         |     |              |
| 434 | 190     | 191     |         |         |         |         | 42      |             | PATCH     | 6/12/2017 | 16:34 | 6      | 2     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         | 39  |              |
| 435 | 155     | 187     | 189     |         |         |         |         |             | PATCH     | 6/12/2017 | 13:42 | 5      | 3     | AG   | 112  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 436 | 201     | 202     |         |         |         |         | 0       | 9           | CAP       | 6/20/2017 | 14:20 | 9      | 2     | WL   | 211  | 6/20/2017 | PP    | AW    | Р         |     |              |
| 437 | 202     | 204     | 205     |         |         |         |         |             | PATCH     | 6/20/2017 | 14:22 | 5      | 4     | WL   | 211  | 6/20/2017 | PP    | AW    | Р         |     |              |
| 438 | 204     | 205     | 206     |         |         |         |         |             | PATCH     | 6/16/2017 | 14:30 | 3      | 3     | WL   | 211  | 6/19/2017 | PP    | AW    | Р         |     |              |
| 439 | 198     | 200     |         |         |         |         | 126     |             | PATCH     | 6/20/2017 | 15:53 | 6      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         | 54  |              |



|     |         |         |         |         | N       | /larked |           |             |           |           |       | Repair | red       |      |      |           | Teste | ed .        |           |                                    | Notes    |
|-----|---------|---------|---------|---------|---------|---------|-----------|-------------|-----------|-----------|-------|--------|-----------|------|------|-----------|-------|-------------|-----------|------------------------------------|----------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station   | Station End | Туре      | Date      | Time  | Length | Width     | Tech | Mach | Date      | Tech  | QA ID       | Pass /    | DS#                                | Comments |
| 440 | 203     | PS      |         |         |         |         | 10        | 15          | PATCH     | 6/20/2017 | 16:25 | 5      | 2         | WL   | 211  | 6/24/2017 | WE    | AW          | Fail<br>P | 55B                                |          |
| 441 | 207     | 204     |         |         |         |         | 2         | 4           | PATCH     | 6/20/2017 | 16:53 | 2      | 1         | WL   | 211  | 6/24/2017 | WE    | AW          | P         | 336                                |          |
| 442 | 207     | 208     |         |         |         |         | 105       | 4           | PATCH     | 6/20/2017 | 15:08 | 6      | 2         | WL   | 211  | 6/24/2017 | WE    | AW          | P         | 56                                 |          |
| 443 | 249     | PS PS   |         |         |         |         | 2         | 7           | PATCH     | 6/27/2017 | 8:09  | 20     | 2         | AG   | 112  | 6/27/2017 | PP    | AW          | P         | 67, 67A, 67B                       |          |
| 444 | 248     | PS      |         |         |         |         | 6         | 11          | PATCH     | 6/27/2017 | 8:04  | 5      | 2         | AG   | 112  | 6/27/2017 | PP    | AW          | P         | 68                                 |          |
| 445 | 252     | 245     |         |         |         |         | 25        | 27          | PIPE BOOT | 6/24/2017 | 16:42 | 9      | 3         | AG   | 112  | 6/27/2017 | WE    | AW          | P         | 00                                 |          |
| 446 | 190     | 191     | 192     |         |         |         | 23        | 21          | PATCH     | 6/12/2017 | 13:42 | 5      | 3         | AG   | 112  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 440 | 185     | 186     | 187     |         |         |         |           |             | PATCH     | 6/12/2017 | 13:46 | 2      | 2         | AG   | 112  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 448 | 185     | 186     | PE3     |         |         |         |           |             | PIPE BOOT | 6/27/2017 | 13:00 | 10     | 5         | WL   | 15   | 6/27/2017 | PP    | AW          | P         |                                    |          |
| 449 | 187     | 188     | 189     |         |         |         |           |             | PATCH     |           | 13:55 | 5      | 3         | AG   | 112  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 450 | 192     | 193     | 103     |         |         |         | 18        |             | PATCH     | 6/16/2017 | 14:50 | 6      | 2         | WL   | 211  | 6/19/2017 | PP    | AW          | P         | 37                                 |          |
| 451 | 192     | 193     |         |         |         |         | 20        |             | PATCH     | 6/12/2017 | 14:58 | 2      | 2         | AG   | 112  | 6/19/2017 | PP    | AW          | P         | 37                                 |          |
| 451 | 192     | 193     | 193     |         |         |         | 20        |             | PATCH     | 6/12/2017 | 14:07 | 2      | 1         | AG   | 112  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 452 | 192     | 191     | R245    |         |         |         |           |             | PATCH     | 6/12/2017 | 15:14 | 2      | 1         | BS   | 15   | 6/20/2017 | BS    | AW          | P         |                                    |          |
| 454 | 194     | R244    | R245    | PS      |         |         |           |             | PATCH     | 6/20/2017 | 15:27 | 2      | 2         | BS   | 15   | 6/20/2017 | BS    | AW          | P         |                                    |          |
| 455 | 194     | 196     | R244    | F3      |         |         |           |             | PATCH     | 6/20/2017 | 15:30 | 2      | 2         | BS   | 15   | 6/20/2017 | BS    | AW          | P         |                                    |          |
| 456 | R244    | PS      | 11244   |         |         |         |           |             | PATCH     | 6/20/2017 | 15:36 | 5      | 3         | BS   | 15   | 6/20/2017 | BS    | AW          | P         |                                    |          |
| 457 | 196     | 197     | R244    |         |         |         |           |             | PATCH     | 6/20/2017 | 15:40 | 2      | 1         | BS   | 15   | 6/20/2017 | BS    | AW          | P         |                                    |          |
| 458 | 194     | 195     | 196     |         |         |         |           |             | PATCH     |           | 17:10 | 4      | 3         | AG   | 112  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 459 | 195     | 196     | 197     |         |         |         |           |             | PATCH     | 6/12/2017 | 17:13 | 3      | 2         | AG   | 112  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 460 | 198     | 199     | 200     |         |         |         |           |             | PATCH     | 6/16/2017 | 11:50 | 7      | 5         | WL   | 211  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 461 | 199     | 200     | 201     |         |         |         |           |             | PATCH     | 6/16/2017 | 13:25 | 3      | 2         | WL   | 211  | 6/19/2017 | PP    | AW          | P P       |                                    |          |
| 462 | 197     | 198     | 201     |         |         |         | 67        |             | PATCH     | 6/16/2017 | 13:32 | 6      | 2         | WL   | 211  | 6/19/2017 | PP    | AW          | P         | 42                                 |          |
| 463 | 198     | 200     |         |         |         |         | 42        |             | PATCH     | 6/16/2017 | 15:45 | 6      | 2         | WL   | 211  | 6/19/2017 | PP    | AW          | P         | 44                                 |          |
| 464 | 198     | 200     |         |         |         |         | 51        | 59          | PIPE BOOT | 6/27/2017 | 7:48  | 8      | 3         | WL   | 15   | 6/27/2017 | PP    | AW          | P         | 44                                 |          |
| 465 | 197     | 198     | R244    | PS      |         |         | 31        | 33          | PATCH     | 6/20/2017 | 15:46 | 4      | 3         | BS   | 15   | 6/20/2017 | BS    | AW          | P         |                                    |          |
| 466 | 198     | 200     | PS PS   | F3      |         |         |           |             | PATCH     | 6/20/2017 | 15:57 | 2      | 2         | BS   | 15   | 6/20/2017 | BS    | AW          | P         |                                    |          |
| 467 | 200     | 201     | PS      |         |         |         |           |             | PATCH     | 6/20/2017 | 16:01 | 2      | 2         | BS   | 15   | 6/24/2017 | WE    | AW          | P         |                                    |          |
| 468 | 201     | PS PS   | F3      |         |         |         |           |             | PATCH     | 6/20/2017 | 16:14 | 5      | 3         | BS   | 15   | 6/24/2017 | WE    | AW          | P         |                                    |          |
| 469 | 201     | 203     | PS      |         |         |         |           |             | PATCH     | 6/20/2017 | 16:26 | 4      | 2         | BS   | 15   | 6/24/2017 | WE    | AW          | P         |                                    |          |
| 470 | 203     | 204     | PS      |         |         |         |           |             | PATCH     | 6/20/2017 | 16:17 | 14     | 2         | WL   | 211  | 6/24/2017 | WE    | AW          | P         | 55                                 |          |
| 471 | 203     | 206     | PS      |         |         |         |           |             | PATCH     | 6/20/2017 | 15:29 | 3      | 2         | WL   | 211  | 6/24/2017 | WE    | AW          | P         | ,,,                                |          |
| 471 | 203     | 204     | 13      |         |         |         | 7         |             | PATCH     | 6/20/2017 | 16:38 | 6      | 2         | WL   | 211  | 6/24/2017 | WE    | AW          | P         | 43                                 |          |
| 472 | 203     | 203     | 204     |         |         |         | ,         |             | PATCH     | 6/20/2017 | 16:43 | 2      | 2         | WL   | 211  | 6/20/2017 | PP    | AW          | P         | 43                                 |          |
| 473 | 202     | 202     | 204     |         |         |         |           |             | PIPE BOOT | 6/26/2017 | 14:42 | 8      | 8         | WL   | 15   | 6/27/2017 | PP    | AW          | P         |                                    |          |
| 474 | 201     | 202     | 203     |         |         |         | 24        |             | PATCH     | 6/26/2017 | 14:42 | 2      | 1         | WL   | 211  | 6/19/2017 | PP    | AW          | P         |                                    |          |
| 475 | 207     | 208     | PS      |         |         |         | <b>24</b> |             | PATCH     | 6/20/2017 | 15:12 | 5      | 2         | WL   | 211  | 6/19/2017 | WE    | AW          | P         |                                    |          |
| 476 | 200     | 207     | PS      |         |         |         |           |             | PATCH     | 6/20/2017 | 14:51 | 2      | 1         | WL   | 211  | 6/24/2017 | WE    | AW          | P         |                                    |          |
| 477 | 100     | 98      | 99      |         |         |         |           |             | CAP       | 0/20/2017 |       |        | MING LOGS |      | 211  |           |       | TIVE TEST L |           | 20A2, 20A3,<br>20A4, 20A5,<br>20A6 |          |



|     |         |         |         |         | ľ       | Marked  |         |             |              |           |       | Repair    | red       |      |      |           | Teste     | d           |        |                                       | Notes    |
|-----|---------|---------|---------|---------|---------|---------|---------|-------------|--------------|-----------|-------|-----------|-----------|------|------|-----------|-----------|-------------|--------|---------------------------------------|----------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Type         | Date      | Time  | Length    | Width     | Tech | Mach | Date      | Tech      | QA ID       | Pass / | DS#                                   | Comments |
| 479 | 91      | 93      |         |         |         |         | 0       | 43          | CAP          |           |       |           |           |      |      |           |           | 4           | Fail   | 21B, 21B2,<br>21B3, 21B4              |          |
| 480 | 86      | 87      |         |         |         |         | 0       | 70          | CAP          |           | SEE   | PANEL SEA | MING LOGS |      |      | SEE NON   | -DESTRUCT | TIVE TEST L | ogs    | 20, 20B, 20B2,<br>20B3, 20B4,<br>20B5 |          |
| 481 | 85      | 86      |         |         |         |         | 0       | 16          | CAP          |           |       |           |           |      |      |           |           |             |        |                                       |          |
| 482 | 85      | 86      |         |         |         |         | 21      | 65          | CAP          |           |       |           |           |      |      |           |           |             |        | 2086, 2087                            |          |
| 483 | 209     | 217     | PS      |         |         |         | 0       | 4           | PATCH, T-cap | 6/13/2017 | 11:23 | 4         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | Р      |                                       |          |
| 484 | 209     | 210     | 217     |         |         |         |         |             | T-CAP        | 6/19/2017 | 10:13 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 485 | 210     | 211     | 217     |         |         |         |         |             | T-CAP        | 6/19/2017 | 10:18 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 486 | 211     | 212     | 217     |         |         |         |         |             | T-CAP        | 6/19/2017 | 10:24 | 3         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 487 | 211     | 212     |         |         |         |         | 13      |             | PATCH        | 6/19/2017 | 10:29 | 5         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      | 48                                    |          |
| 488 | 212     | 213     |         |         |         |         | 5       | 7           | PATCH        | 6/19/2017 | 11:44 | 3         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 489 | 212     | 213     | 215     |         |         |         |         |             | T-CAP        | 6/19/2017 | 11:38 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 490 | 213     | 214     | 215     | 216     |         |         |         |             | T-CAP, PATCH | 6/19/2017 | 11:36 | 11        | 5         | AG   | 112  | 6/20/2017 | BS        | AW          | Р      |                                       |          |
| 491 | 216     | 217     |         |         |         |         | 10      |             | PATCH        | 6/19/2017 | 10:45 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 492 | 215     | 216     | 217     |         |         |         |         |             | T-CAP        | 6/19/2017 | 10:34 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 493 | 212     | 215     | 217     |         |         |         |         |             | T-CAP        | 6/19/2017 | 10:32 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 494 | 218     | 220     |         |         |         |         | 73      | 81          | PATCH        | 6/19/2017 | 10:05 | 9         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 495 | 217     | 218     |         |         |         |         | 16      |             | PATCH        | 6/19/2017 | 10:12 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 496 | 217     | 218     | 219     |         |         |         |         |             | T-CAP        | 6/19/2017 | 10:10 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 497 | 218     | 219     | 220     |         |         |         |         |             | T-CAP        | 6/19/2017 | 10:07 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 498 | 219     | 220     | PS      |         |         |         |         |             | T-CAP        | 6/13/2017 | 15:21 | 2         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | Р      |                                       |          |
| 499 | 217     | 219     | PS      |         |         |         |         |             | T-CAP        | 6/13/2017 | 15:18 | 2         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | Р      |                                       |          |
| 500 | 220     | 221     | PS      |         |         |         |         |             | T-CAP        | 6/13/2017 | 15:38 | 2         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | Р      |                                       |          |
| 501 | 221     | 223     | PS      |         |         |         |         |             | T-CAP        | 6/13/2017 | 15:48 | 2         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | Р      |                                       |          |
| 502 | 221     | 223     |         |         |         |         | 21      | 26          | PATCH        | 6/16/2017 | 15:49 | 6         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 503 | 221     | 223     |         |         |         |         | 45      | 52          | PATCH        | 6/16/2017 | 15:45 | 8         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 504 | 220     | 221     | 222     |         |         |         |         |             | T-CAP        | 6/16/2017 | 15:54 | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 505 | 220     | 222     |         |         |         |         | 0       | 5           | PIPE BOOT    | 6/19/2017 | 8:47  | 5         | 2         | AG   | 112  | 6/20/2017 | PP        | AW          | Р      |                                       |          |
| 506 | 220     | 222     |         |         |         |         | 5       | 10          | PIPE BOOT    | 6/19/2017 | 9:01  | 5         | 4         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 507 | 220     | 222     |         |         |         |         | 13      | 20          | PATCH        | 6/19/2017 | 9:07  | 7         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      | 57                                    |          |
| 508 | 221     | 222     |         |         |         |         | 7       | 14          | PIPE BOOT    | 6/19/2017 | 8:18  | 7         | 6         | AG   | 112  | 6/19/2017 | PP        | AW          | Р      |                                       |          |
| 509 | 221     | 222     | 223     |         |         |         |         |             | T-CAP        | 6/16/2017 | 15:57 | 2         | 2         | AG   | 112  | 6/24/2017 | WE        | AW          | Р      |                                       |          |
| 510 | 223     | 224     |         |         |         |         | 47      |             | PATCH        | 6/16/2017 | 15:38 | 5         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | P      | 50                                    |          |
| 511 | 224     | 225     |         |         |         |         | 13      |             | PATCH        | 6/19/2017 | 8:28  | 2         | 2         | AG   | 112  | 6/19/2017 | PP        | AW          | P      |                                       |          |
| 512 | 223     | 224     | PS      |         |         |         | -       |             | T-CAP        | 6/14/2017 | 9:09  | 2         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | P      |                                       |          |
| 513 | 224     | 225     | PS      |         |         |         |         |             | T-CAP        | 6/14/2017 | 9:07  | 2         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | P      |                                       |          |
| 514 | 225     | 226     | PS      |         |         |         |         |             | T-CAP        | 6/14/2017 | 10:25 | 4         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | P      |                                       |          |
| 515 | 226     | 227     | PS      |         |         |         |         |             | T-CAP        | 6/14/2017 | 10:38 | 3         | 2         | AG   | 112  | 6/16/2017 | BS        | BV          | P      |                                       |          |
| 516 | 227     | PS PS   | 13      |         |         |         | 4       |             | PATCH        | 6/14/2017 | 10:44 | 3         | 3         | AG   | 112  | 6/16/2017 | BS        | BV          | P      |                                       |          |
| 310 | LLI     | 13      |         |         |         |         | -       |             | TAIGI        | 0/17/201/ | 10.44 | J         | 3         | 70   | 112  | 0/10/201/ | JJ.       | υv          | F      |                                       |          |



|     |         |         |          |          |         | // Aarked |         |             |                  |           |       | Repair | red   |      |      |           | Teste | d     |        |              | Notes    |
|-----|---------|---------|----------|----------|---------|-----------|---------|-------------|------------------|-----------|-------|--------|-------|------|------|-----------|-------|-------|--------|--------------|----------|
| Num | Panel 1 | Panel 2 | Panel 3  | Panel 4  | Panel 5 | Panel 6   | Station | Station End | Туре             | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass / | DS#          | Comments |
|     |         |         | railei 3 | railei 4 | railers | railero   |         | Station End |                  |           |       |        |       |      |      |           |       |       | Fail   | D3 #         | Comments |
| 517 | 226     | 227     |          |          |         |           | 64      |             | PIPE BOOT        |           | 15:32 | 8      | 4     | AG   | 112  | 6/19/2017 | PP    | AW    | P      |              |          |
| 518 | 226     | 227     |          |          |         |           | 72      |             | PIPE BOOT        | 6/21/2017 | 10:13 | 6      | 4     | AG   | 211  | 6/24/2017 | WE    | AW    | P      |              |          |
| 519 | 227     | 228     |          |          |         |           | 83      | 88          | PATCH            |           | 11:17 | 5      | 2     | AG   | 211  | 6/28/2017 | PP    | AW    | P      |              |          |
| 520 | 228     | 229     |          |          |         |           | 29      |             | PATCH            | 6/16/2017 | 15:04 | 5      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | P      | 51           |          |
| 521 | 227     | 228     | PS       |          |         |           |         |             | T-CAP            | 6/14/2017 | 10:53 | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | P      |              |          |
| 522 | 228     | 229     | PS       |          |         |           |         |             | T-CAP            | 6/14/2017 | 11:14 | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | P      |              |          |
| 523 | 229     | 230     | PS       |          |         |           |         |             | T-CAP            | 6/14/2017 | 11:25 | 3      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | P      |              |          |
| 524 | 230     | 231     | PS       |          |         |           |         |             | T-CAP            | 6/16/2017 | 8:37  | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | P      |              |          |
| 525 | 230     |         |          |          |         |           |         |             | PIPE BOOT        | 6/16/2017 | 11:25 | 12     | 10    | AG   | 112  | 6/16/2017 | BS    | BV    | P      |              |          |
| 526 | 231     | 232     |          |          |         |           | 31      |             | PIPE BOOT        | 6/16/2017 | 14:14 | 12     | 6     | AG   | 112  | 6/19/2017 | PP    | AW    | Р      |              |          |
| 527 | 231     | 232     |          |          |         |           | 36      |             | PIPE BOOT        | 6/21/2017 | 13:20 | 13     | 6     | AG   | 211  | 6/24/2017 | PP    | AW    | P      |              |          |
| 528 | 231     | 232     |          |          |         |           | 45      |             | PIPE BOOT        | 6/21/2017 | 13:04 | 8      | 3     | AG   | 211  | 6/24/2017 | PP    | AW    | P      |              |          |
| 529 | 232     |         |          |          |         |           | 23 E    | 5 N         | PIPE BOOT        | 6/16/2017 | 10:13 | 7      | 3     | AG   | 112  | 6/16/2017 | BS    | BV    | P      |              |          |
| 530 | 232     | 233     | 234      |          |         |           |         |             | T-CAP            | 6/16/2017 | 10:16 | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | Р      |              |          |
| 531 | 231     | 232     | 233      |          |         |           |         |             | T-CAP            | 6/16/2017 | 10:18 | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | P      |              |          |
| 532 | 231     | 233     | PS       |          |         |           |         |             | T-CAP            | 6/16/2017 | 8:49  | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | Р      |              |          |
| 533 | 233     | 234     | PS       |          |         |           |         |             | T-CAP            | 6/16/2017 | 8:52  | 4      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | Р      |              |          |
| 534 | 234     | 235     | 101      |          |         |           |         |             | T-CAP            | 6/16/2017 | 9:07  | 2      | 2     | AG   | 112  | 6/16/2017 | BS    | BV    | Р      |              |          |
| 535 | 234     | 235     |          |          |         |           | 55      |             | PIPE BOOT        | 6/16/2017 | 10:00 | 7      | 4     | AG   | 112  | 6/19/2017 | PP    | AW    | P      |              |          |
| 536 | 235     |         |          |          |         |           | 74 E    | 9 N         | PIPE BOOT        | 6/24/2017 | 9:25  | 4      | 4     | AG   | 112  | 6/24/2017 | PP    | AW    | Р      |              |          |
| 537 | 234     | 235     | 236      |          |         |           |         |             | PIPE BOOT, T-CAP | 6/21/2017 | 17:25 | 7      | 6     | AG   | 211  | 6/24/2017 | WE    | AW    | Р      |              |          |
| 538 | 8       | 9       | 10       | 11       | WT      |           |         |             | CAP              | 6/16/2017 | 8:30  | 54     | 2     | WL   | 211  | 6/19/2017 | BS    | BV    | Р      | 17,A,A2,B,B2 |          |
| 539 | 43      |         |          |          |         |           | 9 W     | 7 S         | PATCH            | 5/26/2017 | 13:35 | 5      | 2     | AG   | 112  | 5/26/2017 | WE    | AW    | Р      |              |          |
| 540 | 39      | 40      |          |          |         |           | 46      |             | PATCH            | 5/25/2017 | 13:00 | 2      | 2     | AG   | 112  | 6/28/2017 | PP    | AW    | Р      |              |          |
| 541 | 80      | 82      |          |          |         |           | 9       |             | PATCH            | 6/19/2017 | 13:30 | 5      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | Р      | 49           |          |
| 542 | 83      | 84      |          |          |         |           | 28      | 37          | PATCH            | 6/19/2017 | 13:18 | 9      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | Р      | 19B2         |          |
| 543 | 83      | 84      |          |          |         |           | 37      | 40          | PATCH            | 6/6/2017  | 14:30 | 3      | 2     | AG   | 211  | 6/19/2017 | PP    | AW    | Р      | 19B          |          |
| 544 | 83      | 84      |          |          |         |           | 40      | 44          | PATCH            | 6/2/2017  | 17:13 | 4      | 2     | AG   | 83   | 6/19/2017 | PP    | AW    | P      | 19B          |          |
| 545 | 83      | 84      |          |          |         |           | 44      | 48          | PATCH            | 6/20/2017 | 10:38 | 4      | 2     | WL   | 211  | 6/20/2017 | PP    | AW    | Р      | 19           |          |
| 546 | 85      | 86      | R482     | R231     |         |           |         |             | PATCH            | 6/19/2017 | 13:54 | 6      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | P      |              |          |
| 547 | 85      | 86      | R482     |          |         |           | 66      | 68          | PATCH            | 6/19/2017 | 13:38 | 6      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | P      |              |          |
| 548 | 86      | 87      | R480     |          |         |           |         |             | PATCH            | 6/19/2017 | 14:05 | 6      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | Р      | 20A          |          |
| 549 | 84      | 85      |          |          |         |           | 18      | 27          | PATCH            | 6/19/2017 | 13:20 | 9      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | Р      |              |          |
| 550 | 84      | 85      |          |          |         |           | 15      | 18          | PATCH            | 6/6/2017  | 14:25 | 3      | 2     | AG   | 211  | 6/19/2017 | PP    | AW    | P      |              |          |
| 551 | 84      | 85      |          |          |         |           | 4       | 11          | PATCH            | 6/19/2017 | 13:25 | 7      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | P      |              |          |
| 552 | 85      | R482    |          |          |         |           |         |             | PATCH            | 6/19/2017 | 14:16 | 2      | 2     | WL   | 211  | 6/20/2017 | PP    | AW    | Р      |              |          |
| 553 | 86      | R482    |          |          |         |           |         |             | PATCH            | 6/19/2017 | 14:12 | 2      | 2     | WL   | 211  | 6/20/2017 | PP    | AW    | Р      |              |          |
| 554 | 85      | 86      | R481     |          |         |           | 14      | 17          | PATCH            | 6/19/2017 | 15:00 | 5      | 3     | WL   | 211  | 6/20/2017 | PP    | AW    | Р      |              |          |
| 555 | 85      | 86      | R481     |          |         |           | 2       | 4           | PATCH            | 6/19/2017 | 14:55 | 5      | 3     | WL   | 211  | 6/20/2017 | PP    | AW    | Р      |              |          |
| 556 | 78      | 85      | 86       |          |         |           |         |             | PATCH            | 6/1/2017  | 10:30 | 4      | 2     | AG   | 211  | 6/20/2017 | PP    | AW    | Р      |              |          |



|     |         |         |         |         | N        | /larked  |         |             |           |           |       | Repair | ed    |      |      |           | Teste | d     |           |               | Notes    |
|-----|---------|---------|---------|---------|----------|----------|---------|-------------|-----------|-----------|-------|--------|-------|------|------|-----------|-------|-------|-----------|---------------|----------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5  | Panel 6  | Station | Station End | Туре      | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /    | DS#           | Comments |
| 557 | 77      | 86      | R480    | Tune.   | . unc. s | - uner o | 56      | 58          | PATCH     | 6/19/2017 | 15:20 | 2      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | Fail<br>P | 55            |          |
| 558 | 77      | 87      | R480    |         |          |          | 50      | 30          | PATCH     | 6/19/2017 | 15:27 | 2      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | P         |               |          |
| 559 | 84      | 85      | 11100   |         |          |          | 11      | 15          | PATCH     | 6/2/2017  | 17:04 | 4      | 2     | AG   | 83   | 6/20/2017 | PP    | AW    | P         | 19B           |          |
| 560 | 87      | PS      |         |         |          |          | 10      | 15          | PATCH     | 6/19/2017 | 14:18 | 5      | 2     | WL   | 211  | 6/28/2017 | PP    | AW    | P         | 47B           |          |
| 561 | 88      | PS      |         |         |          |          | 10      | 10          | PATCH     | 6/14/2017 | 11:35 | 16     | 2     | AG   | 112  | 6/28/2017 | PP    | AW    | P         | 47            |          |
| 562 | 92      | 94      |         |         |          |          | 6       | 12          | PATCH     | 6/20/2017 | 8:07  | 6      | 2     | WL   | 211  | 6/28/2017 | PP    | AW    | P         | 47            |          |
| 563 | 92      | 94      |         |         |          |          | 12      | 16          | PATCH     | 6/2/2017  | 16:54 | 4      | 2     | AG   | 83   | 6/28/2017 | PP    | AW    | P         |               |          |
| 564 | 92      | 94      |         |         |          |          | 16      | 19          | PATCH     | 6/6/2017  | 14:43 | 3      | 2     | AG   | 211  | 6/28/2017 | PP    | AW    | P         |               |          |
|     |         |         |         |         |          |          |         | 27          |           |           |       |        |       |      |      |           |       |       |           | 24 244 2442   |          |
| 565 | 92      | 94      | 02      |         |          |          | 19      | 21          | PATCH     | 6/20/2017 | 7:50  | 8      | 2     | WL   | 211  | 6/28/2017 | PP    | AW    | P         | 21, 21A, 21A2 |          |
| 566 | 91      | 92      | 93      |         |          |          |         |             | PATCH     | 6/1/2017  | 8:07  | 2      | 2     | AG   | 211  | 6/19/2017 | PP    | AW    | P         |               |          |
| 567 | 92      | 93      | 94      |         |          |          |         |             | PATCH     | 6/1/2017  | 7:58  | 3      | 2     | AG   | 211  | 6/19/2017 | PP    | AW    | P         |               |          |
| 568 | 91      | 93      | R479    |         |          |          | 6       | 8           | PATCH     | 6/19/2017 | 16:10 | 3      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | P         |               |          |
| 569 | 91      | R479    |         |         |          |          | 25      | 30          | PATCH     | 6/19/2017 | 15:42 | 5      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | P         | 58            |          |
| 570 | 73      | 91      | 93      |         |          |          |         |             | PATCH     | 6/19/2017 | 15:55 | 6      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | Р         |               |          |
| 571 | 100     | 101     |         |         |          |          | 2       | 6           | PATCH     | 6/19/2017 | 17:07 | 4      | 2     | WL   | 211  | 6/20/2017 | PP    | AW    | Р         |               |          |
| 572 | 100     | 101     |         |         |          |          | 11      | 14          | PATCH     | 6/7/2017  | 11:30 | 3      | 2     | AG   | 211  | 6/20/2017 | PP    | AW    | Р         |               |          |
| 573 | 100     | 101     |         |         |          |          | 14      | 22          | PATCH     | 6/19/2017 | 16:58 | 8      | 2     | WL   | 211  | 6/20/2017 | PP    | AW    | Р         |               |          |
| 574 | 95      |         |         |         |          |          | 31 W    | 1 S         | PIPE BOOT | 6/2/2017  | 16:39 | 7      | 4     | AG   | 83   | 6/10/2017 | WE    | AW    | Р         |               |          |
| 575 | 97      | PS      |         |         |          |          | 9       | 14          | PATCH     | 6/23/2017 | 15:50 | 16     | 3     | AG   | 211  | 6/24/2017 | WE    | AW    | Р         | 52,52B        |          |
| 576 | 97      | 98      |         |         |          |          | 5       | 8           | PATCH     | 6/1/2017  | 16:54 | 3      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р         |               |          |
| 577 | 98      | PS      |         |         |          |          | 3       | 9           | PATCH     | 6/16/2017 | 14:31 | 6      | 2     | AG   | 112  | 6/16/2017 | BS    | AW    | Р         |               |          |
| 578 | 98      | 100     | PS      |         |          |          |         |             | PIPE BOOT | 6/2/2017  | 10:30 | 7      | 7     | AG   | 211  | 6/10/2017 | WE    | AW    | Р         |               |          |
| 579 | 98      | 100     | R478    |         |          |          |         |             | PATCH     | 6/20/2017 | 8:27  | 7      | 3     | WL   | 211  | 6/24/2017 | PP    | AW    | Р         | 20A7          |          |
| 580 | 98      | 99      | R478    |         |          |          |         |             | PATCH     | 6/20/2017 | 8:37  | 2      | 2     | WL   | 211  | 6/24/2017 | PP    | AW    | Р         |               |          |
| 581 | 97      | 98      | 99      |         |          |          |         |             | PATCH     | 6/1/2017  | 17:30 | 3      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р         |               |          |
| 582 | 97      | 99      |         |         |          |          | 21      | 24          | PATCH     | 6/20/2017 | 10:25 | 10     | 3     | WL   | 211  | 6/24/2017 | WE    | AW    | Р         |               |          |
| 583 | 99      | 100     | R478    |         |          |          |         |             | PATCH     | 6/20/2017 | 11:05 | 6      | 2     | WL   | 211  | 6/24/2017 | PP    | AW    | Р         | 20A5          |          |
| 584 | 97      | 99      |         |         |          |          | 120     | 124         | PATCH     | 6/19/2017 | 16:21 | 4      | 2     | WL   | 211  | 6/19/2017 | PP    | AW    | Р         | 23B           |          |
| 585 | 27      | 103     |         |         |          |          | 9       | 14          | PATCH     | 6/20/2017 | 11:33 | 5      | 2     | WL   | 211  | 6/20/2017 | BS    | AW    | Р         | 46            |          |
| 586 | 101     | 102     |         |         |          |          | 32      | 28          | PIPE BBOT | 6/7/2017  | 10:24 | 6      | 5     | AG   | 211  | 6/10/2017 | WE    | AW    | Р         |               |          |
| 587 | 30      | 99      | 100     | R478    |          |          |         |             | PATCH     | 6/19/2017 | 16:46 | 7      | 3     | WL   | 211  | 6/19/2017 | PP    | AW    | Р         |               |          |
| 588 | 101     | 102     |         |         |          |          | 14      | 22          | PIPE BOOT | 6/7/2017  | 10:21 | 8      | 6     | AG   | 211  | 6/10/2017 | WE    | AW    | Р         |               |          |
| 589 | 104     | 105     |         |         |          |          | 92      | 97          | PIPE BOOT | 6/10/2017 | 10:56 | 5      | 5     | AG   | 112  | 6/24/2017 | PP    | AW    | Р         |               |          |
| 590 | 101     | 104     |         |         |          |          | 113     | 115         | PATCH     | 6/2/2017  | 11:10 | 2      | 2     | AG   | 211  | 6/10/2017 | WE    | AW    | Р         |               |          |
| 591 | 100     | 101     | PS      |         |          |          |         |             | PATCH     | 6/2/2017  | 10:55 | 1      | 1     | AG   | 211  | 6/16/2017 | BS    | AW    | Р         |               |          |
| 592 | 100     | PS      |         |         |          |          | 8       | 15          | PIPE BOOT | 6/2/2017  | 10:45 | 7      | 3     | AG   | 211  | 6/10/2017 | WE    | AW    | Р         |               |          |
| 593 | 109     | 143     | PS      |         |          |          |         |             | PATCH     | 6/19/2017 | 16:15 | 3      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |               |          |
| 594 | 143     | 144     | PS      |         |          |          | 0       | 4           | PATCH     | 6/19/2017 | 16:20 | 4      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |               |          |
| 595 | 143     | 144     | PS      |         |          |          |         |             | PATCH     | 6/19/2017 | 14:40 | 2      | 2     | BS   | 15   | 6/24/2017 | WE    | AW    | Р         |               |          |
| 596 | 144     | PS      |         |         |          |          | 3       | 5           | PATCH     | 6/19/2017 | 13:05 | 2      | 1     | BS   | 15   | 6/20/2017 | BS    | AW    | Р         |               |          |



|     |              |         |         |         | N       | /larked |         |             |           |           |       | Repair | red   |      |      |           | Teste | d     |                |              | Notes             |
|-----|--------------|---------|---------|---------|---------|---------|---------|-------------|-----------|-----------|-------|--------|-------|------|------|-----------|-------|-------|----------------|--------------|-------------------|
| Num | Panel 1      | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Туре      | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /<br>Fail | DS#          | Comments          |
| 597 | 144          | PS      |         |         |         |         | 9       | 15          | PATCH     | 6/19/2017 | 13:10 | 6      | 5     | BS   | 15   | 6/20/2017 | BS    | AW    | P              |              |                   |
| 598 | 144          | 145     | R255    | PS      |         |         | -       |             | PATCH     | 6/19/2017 | 13:15 | 7      | 10    | BS   | 15   | 6/20/2017 | BS    | AW    | P              |              |                   |
| 599 | 145          | 155     | R255    | R254    | PS      |         |         |             | PATCH     | 6/19/2017 | 13:20 | 4      | 5     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 600 | 155          | 156     | R254    |         |         |         |         |             | PATCH     | 6/19/2017 | 13:25 | 2      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 601 | 249          | 250     | PS      |         |         |         |         |             | PATCH     | 6/19/2017 | 13:44 | 16     | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 602 | 238          | 239     | 240     |         |         |         |         |             | T-CAP     | 6/24/2017 | 11:02 | 2      | 2     | AG   | 112  | 6/24/2017 | WE    | AW    | Р              |              |                   |
| 603 | 154          | R253    | R252    | PS      |         |         |         |             | PATCH     | 6/19/2017 | 13:31 | 5      | 3     | BS   | 15   | 6/20/2017 | BS    | W     | Р              |              |                   |
| 604 | R603         | R252    | PS      |         |         |         |         |             | PATCH     | 6/20/2017 | 13:53 | 7      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 605 | 154          | R251    | R252    | PS      |         |         |         |             | PATCH     | 6/20/2017 | 13:40 | 3      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 606 | R251         | PS      |         |         |         |         | 8       | 10          | PATCH     | 6/20/2017 | 13:57 | 3      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 607 | R251         | 159     | R256    |         |         |         |         |             | PATCH     | 6/20/2017 | 13:49 | 3      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 608 | R250         | R251    | R256    | 170     | PS      |         |         |             | PATCH     | 6/20/2017 | 14:00 | 3      | 3     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 609 | 170          | R219    | R250    | PS      |         |         |         |             | PATCH     | 6/20/2017 | 14:03 | 11     | 3     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 610 | 170          | 171     | R249    |         |         |         |         |             | PATCH     | 6/20/2017 | 14:07 | 2      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 611 | 171          | R249    | PS      |         |         |         |         |             | PATCH     | 6/20/2017 | 14:10 | 4      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 612 | 181          | 184     | R258    |         |         |         |         |             | PATCH     | 6/20/2017 | 14:12 | 3      | 3     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 613 | 171          | 181     | R258    |         |         |         |         |             | PATCH     | 6/20/2017 | 14:18 | 1      | 1     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 614 | CENTER PF R2 | 258     |         |         |         |         |         |             | PATCH     | 6/20/2017 | 14:22 | 3      | 3     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              |              |                   |
| 615 | R247         | PS      |         |         |         |         |         |             | PATCH     | 6/20/2017 | 14:38 | 6      | 2     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              | 45           |                   |
| 616 | 243          | R617    |         |         |         |         | 6       | 9           | PATCH     | 6/2/2017  | 10:47 | 3      | 2     | AG   | 211  | 6/27/2017 | PP    | AW    | Р              |              |                   |
| 617 | 243          | 246     | AT      |         |         |         |         |             | PATCH     | 6/21/2017 | 14:47 | 11     | 6     | SP   | 45   | 6/21/2017 | KS    | AW    | Р              |              |                   |
| 618 | 27           | 28      | 31      |         |         |         |         |             | PATCH     | 5/26/2017 | 10:50 | 3      | 2     | MAY  | 60   | 5/26/2017 | WE    | AW    | Р              |              |                   |
| 619 | 29           | 30      | 100     |         |         |         |         |             | T-CAP     | 6/7/2017  | 10:48 | 2      | 2     | AG   | 211  | 6/10/2017 | WE    | BD    | Р              |              | DUPLICATE OF R191 |
| 620 | 44           | 47      | WT      |         |         |         | 0       | 2           | PATCH     | 5/30/2017 | 15:01 | 3      | 2     | AG   | 211  | 5/30/2017 | WE    | AW    | Р              |              | DUPLICATE OF R122 |
| 621 | 100          | 101     |         |         |         |         |         |             | PATCH     | 6/7/2017  | 11:36 | 4      | 3     | AG   | 211  | 6/20/2017 | WE    | AW    | Р              | 23           |                   |
| 622 | 100          | 101     |         |         |         |         |         |             | PATCH     | 6/23/2017 | 9:17  | 12     | 3     | AG   | 211  | 6/23/2017 | PP    | AW    | Р              |              |                   |
| 623 | 97           | 99      |         |         |         |         |         |             | PATCH     | 6/23/2017 | 9:20  | 7      | 3     | AG   | 211  | 6/23/2017 | PP    | AW    | Р              |              |                   |
| 624 | 220          | 221     |         |         |         |         | 64      |             | PATCH     | 6/20/2017 | 9:11  | 7      | 2     | AG   | 112  | 6/20/2017 | PP    | AW    | Р              | 57B          |                   |
| 625 | 83           | 84      |         |         |         |         | 27      | 50          | PATCH     | 6/23/2017 | 9:25  | 23     | 3     | AG   | 211  | 6/28/2017 | PP    | AW    | Р              | 19B, 19B2    |                   |
| 626 | 78           | 84      | 85      |         |         |         | 0       | 27          | PATCH     | 6/23/2017 | 14:20 | 28     | 3     | AG   | 211  | 6/28/2017 | PP    | AW    | Р              | 19,19A, 19A2 |                   |
| 627 | 131          | PS      |         |         |         |         | 9       | 14          | PATCH     | 6/19/2017 | 17:08 | 5      | 2     | AG   | 112  | 6/28/2017 | PP    | AW    | Р              | 40           |                   |
| 628 | 231          | 232     |         |         |         |         | 36      |             | PIPE BOOT | 6/21/2017 | 13:20 | 13     | 6     | AG   | 211  | 6/24/2017 | PP    | AW    | Р              |              | DUPLICATE OF R527 |
| 629 | 231          | 232     |         |         |         |         | 45      |             | PIPE BOOT | 6/21/2017 | 13:04 | 8      | 3     | AG   | 211  | 6/24/2017 | PP    | AW    | Р              |              | DUPLICATE OF R528 |
| 630 | 103          | 104     | 235     | 244     |         |         |         |             | T-CAP     | 6/23/2017 | 16:01 | 4      | 2     | AG   | 211  | 6/24/2017 | WE    | AW    | Р              |              |                   |
| 631 | 235          | 244     |         |         |         |         | 11      |             | PATCH     | 6/23/2017 | 15:58 | 2      | 1     | AG   | 211  | 6/24/2017 | WE    | AW    | Р              |              |                   |
| 632 | 235          | 237     | 244     |         |         |         |         |             | T-CAP     | 6/24/2017 | 9:46  | 3      | 2     | AG   | 112  | 6/24/2017 | WE    | AW    | Р              |              |                   |
| 633 | 235          | 237     |         |         |         |         | 50      |             | PATCH     | 6/24/2017 | 9:40  | 5      | 2     | AG   | 112  | 6/24/2017 | WE    | AW    | P              | 60           |                   |
| 634 | 237          | 244     |         |         |         |         | 10      |             | PATCH     | 6/24/2017 | 9:49  | 6      | 2     | AG   | 112  | 6/24/2017 | WE    | AW    | P              | 65           |                   |
| 635 | 235          | 236     | 237     |         |         |         |         |             | T-CAP     | 6/24/2017 | 9:31  | 2      | 1     | AG   | 112  | 6/24/2017 | PP    | AW    | Р              |              |                   |



| No.   Parel    otes              |
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| March   19   | Comments          |
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| 656   242   250   251   28   |                   |
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| 658 249 250 PS   |                   |
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| 664 243 246 247 8 8617 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8   |                   |
| 665 243 246 R617   |                   |
| 667 248 249 PS   |                   |
| 668 247 248 PS RS  |                   |
| 669 247 PS PATCH 6/24/2017 14:50 5 5 AG 112 6/24/2017 WE AW P 670 246 247 PS T-CAP 6/24/2017 11:35 2 2 WL 15 6/24/2017 WE AW P   |                   |
| 670     246     247     PS     31     37     PATCH     6/24/2017     14:45     8     6     AG     112     6/24/2017     WE     AW     P       671     246     247     PS     T-CAP     6/24/2017     11:35     2     2     WL     15     6/24/2017     WE     AW     P   |                   |
| 671 246 247 PS T-CAP 6/24/2017 11:35 2 2 WL 15 6/24/2017 WE AW P   |                   |
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| 673 252 245 25 27 PIPE BOOT 6/24/2017 16:42 9 3 AG 112 6/27/2017 WE AW P   | DUPLICATE OF R445 |
| 674 245 252 28 32 PIPE BOOT 6/26/2017 9:07 6 4 AG 112 6/27/2017 PP AW P  |                   |
| 675 245 252 PS T-CAP 6/24/2017 10:40 3 2 WL 15 6/24/2017 PP AW P   |                   |



|     |         |         |         |         | n       | Marked  |         |             |           |           |       | Repair | red   |          |          |           | Teste | d     |           |     | Notes    |
|-----|---------|---------|---------|---------|---------|---------|---------|-------------|-----------|-----------|-------|--------|-------|----------|----------|-----------|-------|-------|-----------|-----|----------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Type      | Date      | Time  | Length | Width | Tech     | Mach     | Date      | Tech  | QA ID | Pass /    | DS# | Comments |
| 676 | 245     | PS      |         |         | '       |         | 0       | 5           | PATCH     | 6/24/2017 | 10:45 | 5      | 3     | WL       | 15       | 6/24/2017 | WE    | AW    | Fail<br>P |     |          |
| 677 | 253     | 254     |         |         |         |         | 6       | 8           | PATCH     | 6/24/2017 | 9:30  | 3      | 1     | WL       | 15       | 6/24/2017 | WE    | AW    | P         |     |          |
| 678 | 252     | 253     | R679    |         |         |         | 0       |             | PATCH     | 6/24/2017 | 10:00 | 2      |       |          |          | 6/24/2017 | PP    |       | P         |     |          |
| 679 | 252     | 253     | PS PS   |         |         |         |         |             | T-CAP     | 6/24/2017 | 9:47  | 6      | 3     | WL<br>WL | 15<br>15 | 6/24/2017 | PP    | AW    | P         |     |          |
| 680 | 252     | 253     | 254     |         |         |         |         |             | T-CAP     | 6/24/2017 | 10:15 | 4      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | P         |     |          |
| 681 | 252     | 254     | 255     |         |         |         |         |             | T-CAP     |           |       | 6      |       |          |          |           |       |       | P         |     |          |
|     |         |         |         |         |         |         |         |             |           | 6/24/2017 | 9:21  |        | 2     | WL       | 15       | 6/24/2017 | WE    | AW    |           |     |          |
| 682 | 255     | 256     | PS      |         |         |         |         |             | T-CAP     | 6/24/2017 | 8:45  | 3      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | P         |     |          |
| 683 | 255     | 256     |         |         |         |         | 13      |             | PATCH     | 6/24/2017 | 8:52  | 5      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | P         | 62  |          |
| 684 | 256     | 257     | PS      |         |         |         |         |             | T-CAP     | 6/24/2017 | 8:18  | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 685 | 257     | 258     | PS      |         |         |         |         |             | T-CAP     | 6/24/2017 | 8:10  | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 686 | 257     | 258     |         |         |         |         | 14      |             | PATCH     | 6/24/2017 | 14:15 | 3      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 687 | 258     | 259     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 17:41 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 688 | 259     | 260     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 17:30 | 2      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 689 | 260     | 261     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 17:05 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 690 | 261     | 262     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 16:51 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 691 | 262     | 263     |         |         |         |         | 2       | 4           | PATCH     | 6/23/2017 | 16:15 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 692 | 263     | 264     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 15:45 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 693 | 264     | 265     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 15:30 | 1      | 1     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 694 | 265     | 266     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 15:16 | 2      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 695 | 265     | 266     |         |         |         |         | 19      | 21          | PATCH     | 6/23/2017 | 15:25 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 696 | 266     | 267     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 14:42 | 3      | 1     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 697 | 267     | 268     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 14:28 | 2      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 698 | 268     | 269     | PS      |         |         |         |         |             | T-CAP     | 6/23/2017 | 14:20 | 2      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 699 | 269     | 274     | 282     |         |         |         |         |             | T-CAP     | 6/26/2017 | 10:48 | 3      | 2     | WL       | 15       | 6/26/2017 | PP    | AW    | Р         |     |          |
| 700 | 274     | 282     |         |         |         |         | 5       | 7           | PATCH     | 6/24/2017 | 14:40 | 2      | 1     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 701 | 281     | 282     | PS      |         |         |         |         |             | T-CAP     | 6/24/2017 | 14:38 | 3      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 702 | 208     | 281     | PS      |         |         |         |         |             | T-CAP     | 6/24/2017 | 14:28 | 3      | 3     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 703 | 274     | 281     |         |         |         |         | 14      |             | PATCH     | 6/24/2017 | 14:52 | 6      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         | 64  |          |
| 704 | 274     | 281     | 282     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:00 | 3      | 3     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 705 | 274     | 280     | 281     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:07 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 706 | 273     | 280     | 281     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:14 | 3      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 707 | 271     | 273     | 281     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:22 | 3      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 708 | 272     | 273     | 280     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:48 | 2      | 2     | WL       | 15       | 6/24/2017 | PP    | AW    | Р         |     |          |
| 709 | 274     | 275     | 280     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:32 | 2      | 2     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 710 | 272     | 279     | 280     |         |         |         |         |             | T-CAP     | 6/24/2017 | 16:00 | 3      | 3     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 711 | 275     | 277     | 279     | 280     |         |         |         |             | T-CAP     | 6/24/2017 | 16:01 | 4      | 3     | WL       | 15       | 6/24/2017 | WE    | AW    | Р         |     |          |
| 712 | 276     | 277     | 278     | 279     |         |         |         |             | T-CAP     | 6/26/2017 | 14:35 | 3      | 2     | WL       | 15       | 6/26/2017 | WE    | AW    | Р         |     |          |
| 713 | 278     | 279     |         |         |         |         |         |             | PATCH     | 6/26/2017 | 9:48  | 4      | 2     | WL       | 15       | 6/26/2017 | WE    | AW    | Р         |     |          |
| 714 | 276     |         |         |         |         |         | 2'E 5'S |             | PIPE BOOT | 6/26/2017 | 8:34  | 4      | 3     | WL       | 15       | 6/26/2017 | WE    | AW    | Р         |     |          |
| 715 | 275     | 276     | 277     |         |         |         |         |             | T-CAP     | 6/26/2017 | 15:55 | 2      | 2     | WL       | 15       | 6/26/2017 | WE    | AW    | Р         |     |          |
| 715 | 275     | 276     | 277     |         |         |         |         |             | T-CAP     | 6/26/2017 | 15:55 | 2      | 2     | WL       | 15       | 6/26/2017 | WE    | AW    | Р         |     |          |



|     |         |         |         |         | N       | /larked |         |             |           |           |       | Repair | red   |      |      |           | Teste | d     |           |      | Notes    |
|-----|---------|---------|---------|---------|---------|---------|---------|-------------|-----------|-----------|-------|--------|-------|------|------|-----------|-------|-------|-----------|------|----------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4 | Panel 5 | Panel 6 | Station | Station End | Туре      | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /    | DS#  | Comments |
| 716 | 274     | 275     |         |         |         |         | 38      | 47          | PATCH     | 6/26/2017 | 10:40 | 9      | 5     | WL   | 15   | 6/26/2017 | WE    | AW    | Fail<br>P |      | <u> </u> |
| 717 | 270     | 272     |         |         |         |         | 28      | 31          | PATCH     | 6/26/2017 | 16:16 | 3      | 2     | WL   | 15   | 6/26/2017 | WE    | AW    | P         |      |          |
| 718 | 270     | 283     |         |         |         |         |         |             | PATCH     | 6/24/2017 | 16:51 | 4      | 2     | WL   | 15   | 6/26/2017 | WE    | AW    | P         |      |          |
| 719 | 270     | 272     | 273     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:40 | 3      | 3     | WL   | 15   | 6/24/2017 | PP    | AW    | P         |      |          |
| 720 | 270     | 271     | 273     |         |         |         |         |             | T-CAP     | 6/24/2017 | 15:32 | 2      | 2     | WL   | 15   | 6/26/2017 | WE    | AW    | P         |      |          |
| 721 | 271     | 273     |         |         |         |         | 21      |             | PATCH     | 6/24/2017 | 15:27 | 6      | 2     | WL   | 15   | 6/24/2017 | WE    | AW    | Р         | 63   |          |
| 722 | 283     | 284     | 285     |         |         |         |         |             | T-CAP     | 6/24/2017 | 16:21 | 2      | 2     | WL   | 15   | 6/24/2017 | WE    | AW    | P         | - 03 |          |
| 723 | 283     | 285     |         |         |         |         | 18      |             | PATCH     | 6/24/2017 | 16:41 | 6      | 2     | WL   | 15   | 6/26/2017 | WE    | AW    | P         | 66   |          |
| 724 | 283     | 285     |         |         |         |         | 27      | 29          | PATCH     | 6/24/2017 | 16:48 | 3      | 2     | WL   | 15   | 6/26/2017 | WE    | AW    | P         | - 00 |          |
| 725 | 170     | 160     | R256    | R257    |         |         |         |             | PIPE BOOT | 6/27/2017 | 7:58  | 8      | 6     | AG   | 112  | 6/27/2017 | PP    | AW    | P         |      |          |
| 726 | 160     | 162     | 170     | R257    |         |         |         |             | PATCH     | 6/19/2017 | 14:00 | 6      | 3     | BS   | 15   | 6/20/2017 | PP    | AW    | P         |      |          |
| 727 | 160     | R256    | R257    |         |         |         |         |             | PATCH     | 6/19/2017 | 14:02 | 2      | 1     | BS   | 15   | 6/20/2017 | PP    | AW    | P         |      |          |
| 728 | 159     | 160     | R256    |         |         |         |         |             | PIPE BOOT | 6/26/2017 | 10:30 | 6      | 7     | AG   | 112  | 6/27/2017 | PP    | AW    | P         |      |          |
| 729 | 129     | 130     |         |         |         |         | 15      | 20          | PIPE BOOT | 6/22/2017 | 11:03 | 18     | 9     | AG   | 211  | 6/23/2017 | WE    | AW    | P         |      |          |
| 730 | 142     | AT      |         |         |         |         |         |             | PATCH     | 6/26/2017 | 16:15 | 25     | 4     | WL   | 15   | 6/28/2017 | PP    | AW    | Р         |      |          |
| 731 | 136     | 142     | 214     | AT      |         |         |         |             | PATCH     | 6/26/2017 | 16:00 | 27     | 4     | WL   | 15   | 6/28/2017 | PP    | AW    | P         |      |          |
| 732 | 245     | 246     |         |         |         |         | 66      | 70          | PATCH     | 6/27/2017 | 13:41 | 4      | 2     | AG   | 112  | 6/27/2017 | PP    | AW    | P         |      |          |
| 733 | 245     | 252     |         |         |         |         |         |             | PATCH     | 6/27/2017 | 13:23 | 3      | 2     | AG   | 112  | 6/27/2017 | PP    | AW    | P         |      |          |
| 734 | 252     | 254     | AT      |         |         |         |         |             | PATCH     | 6/27/2017 | 13:14 | 1      | 1     | AG   | 112  | 6/27/2017 | PP    | AW    | P         |      |          |
| 735 | 254     | 255     | AT      |         |         |         |         |             | PATCH     | 6/27/2017 | 15:00 | 8      | 3     | AG   | 112  | 6/27/2017 | PP    | AW    | Р         |      |          |
| 736 | 255     | 256     | AT      |         |         |         |         |             | PATCH     | 6/27/2017 | 15:15 | 11     | 8     | AG   | 112  | 6/27/2017 | PP    | AW    | Р         |      |          |
| 737 | 256     | 257     | 258     | AT      |         |         |         |             | PIPE BOOT | 6/30/2017 | 7:30  | 17     | 14    | WL   | 112  | 6/30/2017 | PP    | AW    | Р         |      |          |
| 738 | 258     | 259     | AT      |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 13:57 | 11     | 10    | AG   | 112  | 6/28/2017 | PP    | AW    | Р         |      |          |
| 739 | 259     | 260     | AT      |         |         |         |         |             | PATCH     | 6/27/2017 | 13:58 | 19     | 6     | AG   | 112  | 6/27/2017 | PP    | AW    | Р         |      |          |
| 740 | 260     | 261     | AT      |         |         |         |         |             | PATCH     | 6/27/2017 | 13:45 | 22     | 3     | AG   | 112  | 6/27/2017 | PP    | AW    | Р         |      |          |
| 741 | 240     | AT      |         |         |         |         |         |             | PATCH     | 6/29/2017 | 14:40 | 4      | 2     | WL   | 15   | 6/29/2017 | PP    | AW    | Р         |      |          |
| 742 | 249     | PS      |         |         |         |         | 6       | 16          | PATCH     | 6/27/2017 | 16:04 | 10     | 2     | AG   | 112  | 6/27/2017 | PP    | AW    | Р         | 67A  |          |
| 743 | 249     | 250     | PS      |         |         |         | 4       | 16          | PATCH     | 6/27/2017 | 16:21 | 15     | 2     | AG   | 112  | 6/27/2017 | PP    | AW    | Р         | 67B  |          |
| 744 | 135     | WT      |         |         |         |         | 7       | 13          | PATCH     | 6/28/2017 | 10:45 | 6      | 2     | WL   | 15   | 6/29/2017 | PP    | AW    | Р         | 69   |          |
| 745 | 208     |         |         |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 8:03  | 3      | 3     | WL   | 15   | 6/27/2017 | PP    | AW    | Р         |      | SDR15    |
| 746 | 200     | 201     |         |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 8:51  | 3      | 3     | WL   | 15   | 6/27/2017 | PP    | AW    | Р         |      | SDR14    |
| 747 | 189     |         |         |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 9:17  | 3      | 3     | WL   | 15   | 6/27/2017 | PP    | AW    | Р         |      | SDR13    |
| 748 | 182     | 185     |         |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 9:43  | 3      | 3     | WL   | 15   | 6/27/2017 | PP    | AW    | Р         |      | SDR12    |
| 749 | 189     |         |         |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 10:28 | 3      | 3     | WL   | 15   | 6/27/2017 | PP    | AW    | Р         |      | SDR11    |
| 750 | 162     |         |         |         |         |         | SEE PAN | IEL LAYOUT  | PIPE BOOT | 6/27/2017 | 11:11 | 3      | 3     | WL   | 15   | 6/27/2017 | PP    | AW    | Р         |      | SDR10    |
| 751 | 165     |         |         |         |         |         |         | GRAM        | PIPE BOOT | 6/27/2017 | 14:05 | 3      | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р         |      | SDR9     |
| 752 | 155     |         |         |         |         |         |         |             | PIPE BOOT | 6/27/2017 | 14:41 | 3      | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р         |      | SDR8     |
| 753 | 108     |         |         |         |         |         |         |             | PIPE BOOT | 6/28/2017 | 8:07  | 3      | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р         |      | SDR7     |
| 754 | 96      |         |         |         |         |         |         |             | PIPE BOOT | 6/28/2017 | 8:25  | 3      | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р         |      | SDR6     |
| 755 | 89      |         |         |         |         |         |         |             | PIPE BOOT | 6/28/2017 | 8:43  | 3      | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р         |      | SDR5     |



|     |         |         |         |             | N         | /larked |          |                     |           |           |       | Repair | red   |      |      |           | Teste | d     |                |     | Notes    |
|-----|---------|---------|---------|-------------|-----------|---------|----------|---------------------|-----------|-----------|-------|--------|-------|------|------|-----------|-------|-------|----------------|-----|----------|
| Num | Panel 1 | Panel 2 | Panel 3 | Panel 4     | Panel 5   | Panel 6 | Station  | Station End         | Туре      | Date      | Time  | Length | Width | Tech | Mach | Date      | Tech  | QA ID | Pass /<br>Fail | DS# | Comments |
| 756 | 63      | 64      |         |             |           |         |          |                     | PIPE BOOT | 6/28/2017 | 9:08  | 3      | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р              |     | SDR3     |
| 757 | 78      | 84      | 85      |             |           |         |          |                     | PIPE BOOT | 6/29/2017 | 8:30  | 3      | 3     | WL   | 15   | 6/29/2017 | PP    | AW    | Р              |     | SDR4     |
| 758 | 47      | 48      |         |             |           |         |          | IEL LAYOUT<br>IGRAM | PIPE BOOT | 6/28/2017 | 10:35 | 3      | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р              |     | SDR2     |
| 759 | 48      | WT      |         |             |           |         |          |                     | PIPE BOOT | 6/29/2017 | 8:00  | 3      | 2     | WL   | 15   | 6/29/2017 | PP    | AW    | Р              |     | SDR1     |
| 760 | 18      | WT      | AT      |             |           |         |          |                     | PATCH     | 6/28/2017 | 16:45 | 6      | 3     | BS   | 43   | 6/29/2017 | PP    | AW    | Р              |     |          |
| 761 | 167     |         |         |             |           |         | 28'E 8'N |                     | PATCH     | 7/1/2017  | 7:45  | 3      | 2     | WL   | 112  | 7/1/2017  | PP    | AW    | Р              |     |          |
| 762 | 57      |         |         |             |           |         |          |                     | PIPE BOOT | 5/26/2017 | 10:40 | 4      | 4     | AG   | 112  | 5/26/2017 | WE    | AW    | Р              |     |          |
| 763 | 159     | 160     |         |             |           |         | 213      |                     | PATCH     | 6/20/2017 | 15:00 | 5      | 4     | BS   | 15   | 6/20/2017 | BS    | AW    | Р              | 53  |          |
| 764 | 23      | 24      |         |             |           |         | 97       |                     | PATCH     | 5/22/2017 | 11:00 | 4      | 2     | MAY  | 211  | 5/30/2017 | WE    | AW    | Р              | 6   |          |
| 765 |         |         | 5       | SEE PANEL I | AYOUT DIA | GRAM    |          |                     | PIPE BOOT | 6/2/2017  | 11:15 | 6      | 5     | MAY  | 60   | 6/10/2017 | WE    | AW    | Р              |     |          |
| 766 | 135     | WT      |         |             |           |         |          |                     | PATCH     | 6/28/2017 | 10:45 | 17     | 3     | WL   | 15   | 6/28/2017 | PP    | AW    | Р              |     |          |



#### **APPENDIX D**

#### LANDFILL GAS AND LIQUIDS MANAGEMENT INFRASTRUCTURE

#### **Sub-Appendices**

D.1 Pipe InformationD.2 Pressure Test Forms

#### Sub-Appendix D.1

**Pipe Information** 

Table 1: Typical Cell Classification by Current Thermoplastic Piping Material Designation Code

| PHYSICAL                              | ASTM           |           | PE2            | 2708                             | PE             | <b>3608</b>              | PE <sub>4</sub> | 1710                     |
|---------------------------------------|----------------|-----------|----------------|----------------------------------|----------------|--------------------------|-----------------|--------------------------|
| PROPERTY                              | Test<br>Method | Units     | Cell<br>Number | Typical<br>Value                 | Cell<br>Number | Typical<br>Value         | Cell<br>Number  | Typical<br>Value         |
| DENSITY                               | D 1505         | GR/CC     | 2              | >0.925-<br>0.940                 | 3              | >0.940-<br>0.947         | 4               | >0.947-<br>0.955         |
| MELT INDEX                            | D 1238         | gr/10 min | 3              | < 0.4-0.15                       | 4              | < 0.15                   | 4               | < 0.15                   |
| FLEXURAL<br>MODULUS                   | D 790          | PSI       | 3              | 40,000<br>-<80,000               | 5              | 110,000 -<br><180,000    | 5               | 110,000 -<br><180,000    |
| TENSILE<br>STRENGTH                   | D 638          | PSI       | 3              | 2600 -<br><3000                  | 4              | 3000 -<br><3500          | 4               | 3000 -<br>< 3500         |
| RESISTANCE TO<br>SLOW CRACK<br>GROWTH | F 1473         | HOURS     | 7              | 500 min                          | 6              | 100 min                  | 7               | 500 min                  |
| Hydrostatic<br>Design Basis,<br>HDB   | D 2387         | PSI       | 3              | 1250                             | 4              | 1600                     | 4               | 1600                     |
| UV STABILIZER                         | D 1603         | %         | E              | COLORED<br>WITH UV<br>STABILIZER | C              | 2% MIN CAR-<br>BON BLACK | C               | 2% MIN CAR-<br>BON BLACK |

#### Notes:

It should be noted that other PE thermoplastics piping material designation codes do exist and may be encountered in the market place occasionally. However, the three primary PE thermoplastic piping material designations codes of Table 1 represent the principle PE piping products in the market today. For more information regarding these other thermoplastic piping material designation codes, please contact your ISCO sales professional.

Table 2 below provides a simplification of Table 1 and illustrates the relative ease with which PE piping products may be specified. Using this approach allows the designer or specifier to accurately designate the appropriate PE piping product through the use a single thermoplastic piping material designation code and a relatively simple text string that establishes the physical property requirements for seven key performance properties.

Table 2: Representative Minimum Cell Classification by Thermoplastic Piping Material Designation Code

| THERMOPLASTIC PIPING MATERIAL DESIGNATION CODE | MINIMUM CELL CLASSIFICATION PER ASTM D3350 |
|--|--|
| PE2708   | 233373E                                    |
| PE3608   | 345464C                                    |
| PE4710   | 445474C                                    |

The selected thermoplastic piping material designation code and minimum cell classification is then combined with the appropriate production and installation standards to effectively specify a tough, durable PE piping system. ISCO Industries can provide model specifications for a wide range of PE pipe applications. These model specifications are available at www.isco-pipe.com or by contacting your ISCO sales professional.



**HDPE** Pipe

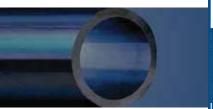
1-800-345-ISCO

www.isco-pipe.com



<sup>1)</sup> The density provided is base resin density (without the influence of carbon black). Typical PE4710 HDPE pipe has a density of 0.956 to 0.964 with carbon black.

<sup>2)</sup> To be designated a PE4710, the pipe resin must meet certain supplementary requirements established by the Hydrostatic Stress Board (HSB) of the Plastics Pipe Institute (PPI).



#### **HDPE** Pipe

- Items highlighted in Blue indicates standard stocking items that are more readily available.
- Pressures are based on using water at 23°C (73°F).
- Average inside diameter calculated using nominal OD and minimum wall plus 6% for use in estimating fluid flows. Actual ID will vary.
- Service factors should be utilized to compensate for the effect of liquids other than water, and for other temperatures.
- Other piping sizes or DR's may be available upon request.
- Standard Lengths: 40' for 2"-24"
  50' for 26" and larger Coils available for 3/4"-6"(8" by special order)

1-800-345-ISCO

www.isco-pipe.com

#### PE 4710 IPS HDPE Pipe Sizes

| Б                     |                 | Nominal<br>Size | 1"     | 1 1/4" | 1 1/2" | 2"     | 3"     | 4"     | 5"     | 6"     | 8"     | 10"     | 12"     | 14"     | 16"     | 18"     |
|-----------------------|-----------------|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|---------|---------|
|                       | essure<br>ating | Actual<br>O.D.  | 1.32"  | 1.660" | 1.90"  | 2.38"  | 3.500" | 4.50"  | 5.563" | 6.625" | 8.625" | 10.750" | 12.75"  | 14.00"  | 16.00"  | 18.00"  |
|                       |                 | Min. wall       | 0.188" | 0.237" | 0.271" | 0.339" | 0.500" | 0.643" | 0.795" | 0.946" | 1.232" | 1.536"  | 1.821"  | 2.000"  | 2.286"  | 2.571"  |
| , <sub>D</sub>        | )R 7            | Average<br>I.D. | 0.917" | 1.157" | 1.325" | 1.656" | 2.440" | 3.137" | 3.878" | 4.619" | 6.013" | 7.494"  | 8.889"  | 9.760"  | 11.154" | 12.549" |
|                       | 33psi)          | Weight<br>lb/lf | 0.291  | 0.463  | 0.607  | 0.950  | 2.060  | 3.402  | 5.200  | 7.374  | 12.498 | 19.416  | 27.312  | 32.930  | 43.010  | 54.435  |
|                       |                 | Min. wall       | 0.180" | 0.227" | 0.260" | 0.325" | 0.479" | 0.616" | 0.762" | 0.908" | 1.182" | 1.473"  | 1.747"  | 1.918"  | 2.192"  | 2.466"  |
| DI                    | R 7.3           | Average<br>I.D. | 0.933" | 1.178" | 1.348" | 1.685" | 2.484" | 3.193" | 3.947" | 4.701" | 6.120" | 7.628"  | 9.047"  | 9.934"  | 11.353" | 12.773" |
|                       | 12psi)          | Weight<br>lb/lf | 0.281  | 0.450  | 0.590  | 0.920  | 1.990  | 3.290  | 5.022  | 7.130  | 12.070 | 18.750  | 26.380  | 31.810  | 41.550  | 52.580  |
|                       |                 | Min. wall       | 0.146" | 0.184" | 0.211" | 0.264" | 0.389" | 0.500" | 0.618" | 0.736" | 0.958" | 1.194"  | 1.417"  | 1.556"  | 1.778"  | 2.000"  |
| D                     | R 9             | Average<br>I.D. | 1.005" | 1.269" | 1.452" | 1.816" | 2.676" | 3.440" | 4.253" | 5.064" | 6.593" | 8.218"  | 9.747"  | 10.702" | 12.231" | 13.760" |
| ( 25                  | 50psi)          | Weight<br>lb/lf | 0.235  | 0.374  | 0.490  | 0.770  | 1.664  | 2.751  | 4.204  | 5.963  | 10.110 | 15.700  | 22.085  | 26.630  | 34.780  | 44.020  |
|                       |                 | Min. wall       | 0.120" | 0.151" | 0.173" | 0.216" | 0.318" | 0.409" | 0.506" | 0.602" | 0.784" | 0.977"  | 1.159"  | 1.273"  | 1.455"  | 1.636"  |
| DI                    | R 11            | Average<br>I.D. | 1.062" | 1.340" | 1.534" | 1.917" | 2.825" | 3.633" | 4.491" | 5.348" | 6.963" | 8.678"  | 10.293" | 11.302" | 12.916" | 14.531" |
| ( 20                  | 00psi )         | Weight<br>lb/lf | 0.200  | 0.314  | 0.411  | 0.642  | 1.395  | 2.310  | 3.523  | 5.000  | 8.470  | 13.160  | 18.510  | 22.320  | 29.150  | 36.890  |
|                       |                 | Min. wall       |        |        |        | 0.176" | 0.259" | 0.333" | 0.412" | 0.491" | 0.639" | 0.796"  | 0.944"  | 1.037"  | 1.185"  | 1.333"  |
| DR 13.5<br>( 160psi ) | Average<br>I.D. |                 |        |        | 2.002" | 2.950" | 3.793" | 4.689" | 5.585" | 7.271" | 9.062" | 10.748" | 11.801" | 13.487" | 15.173" |         |
|                       | Weight<br>lb/lf |                 |        |        | 0.534  | 1.160  | 1.920  | 2.928  | 4.152  | 7.040  | 10.932 | 15.380  | 18.540  | 24.220  | 30.651  |         |
|                       |                 | Min. wall       |        |        |        | 0.153" | 0.226" | 0.290" | 0.359" | 0.427" | 0.556" | 0.694"  | 0.823"  | 0.903"  | 1.032"  | 1.161"  |
|                       | R 15.5          | Average<br>I.D. |        |        |        | 2.050" | 3.021" | 3.885" | 4.802" | 5.719" | 7.445" | 9.280"  | 11.006" | 12.085" | 13.812" | 15.538" |
| (13                   | 38psi )         | Weight<br>lb/lf |        |        |        | 0.470  | 1.020  | 1.687  | 2.580  | 3.656  | 6.197  | 9.626   | 13.530  | 16.310  | 21.300  | 26.950  |
|                       |                 | Min. wall       |        |        |        | 0.140" | 0.206" | 0.265" | 0.327" | 0.390" | 0.507" | 0.632"  | 0.750"  | 0.824"  | 0.941"  | 1.059"  |
|                       | R 17            | Average<br>I.D. |        |        |        | 2.079" | 3.064" | 3.939" | 4.869" | 5.799" | 7.549" | 9.409"  | 11.160" | 12.254" | 14.005" | 15.755" |
| ( 12                  | 25psi )         | Weight<br>lb/lf |        |        |        | 0.431  | 0.940  | 1.550  | 2.360  | 3.360  | 5.690  | 8.834   | 12.430  | 14.983  | 19.570  | 24.770  |
|                       |                 | Min. wall       |        |        |        |        |        | 0.214" | 0.265" | 0.315" | 0.411" | 0.512"  | 0.607"  | 0.667"  | 0.762"  | 0.857"  |
| DI                    | R 21            | Average<br>I.D. |        |        |        |        |        | 4.046" | 5.001" | 5.956" | 7.754" | 9.665"  | 11.463" | 12.587" | 14.385" | 16.183" |
| (10                   | ( 100psi )      | Weight<br>lb/lf |        |        |        |        |        | 1.270  | 1.940  | 2.750  | 4.662  | 7.242   | 10.190  | 12.282  | 16.042  | 20.304  |
|                       |                 | Min. wall       |        |        |        |        |        | 0.173" | 0.214" | 0.255" | 0.332" | 0.413"  | 0.490"  | 0.538"  | 0.615"  | 0.692"  |
| DI                    | R 26            | Average<br>I.D. |        |        |        |        |        | 4.133" | 5.109" | 6.085" | 7.922" | 9.873"  | 11.710" | 12.858" | 14.695" | 16.532" |
| ( 80                  | ( 80 psi )      | Weight<br>lb/lf |        |        |        |        |        | 1.035  | 1.582  | 2.250  | 3.800  | 5.910   | 8.312   | 10.022  | 13.090  | 16.570  |
|                       |                 | Min. wall       |        |        |        |        |        | 0.138" | 0.171" | 0.204" | 0.265" | 0.331"  | 0.392"  | 0.431"  | 0.492"  | 0.554"  |
|                       | 32.5            | Average<br>I.D. |        |        |        |        |        | 4.206" | 5.200" | 6.193" | 8.062" | 10.049" | 11.918" | 13.087" | 14.956" | 16.826" |
| ( 63                  | 3 psi )         | Weight<br>lb/lf |        |        |        |        |        | 0.835  | 1.280  | 1.811  | 3.070  | 4.770   | 6.710   | 8.090   | 10.561  | 13.370  |

#### PE 4710 IPS HDPE Pipe Sizes

| 20"     | 22"     | 24"     | 26"     | 28"     | 30"     | 32"     | 34"     | 36"     | 42"     | 48"     | 54"     | 63"     | Nominal<br>Size<br>Actual | Pressure   |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------------------------|------------|
| 20.00"  | 22.00"  | 24.00"  | 26.00"  | 28.00"  | 30.00"  | 32.00"  | 34.00"  | 36.00"  | 42.00"  | 48.00"  | 54.00"  | 62.99"  | O.D.                      | Rating     |
| 2.857"  | 3.143"  | 3.429"  |         |         |         |         |         |         |         |         |         |         | Min. wall                 |            |
| 13.943" | 15.337" | 16.731" |         |         |         |         |         |         |         |         |         |         | Average<br>I.D.           | DR 7       |
| 67.203  | 80.591  | 95.916  |         |         |         |         |         |         |         |         |         |         | Weight<br>lb/lf           | ( 333psi ) |
| 2.740"  | 3.014"  | 3.288"  | 3.562"  |         |         |         |         |         |         |         |         |         | Min. wall                 |            |
| 14.192" | 15.611" | 17.030" | 18.449" |         |         |         |         |         |         |         |         |         | Average<br>I.D.           | DR 7.3     |
| 64.910  | 78.550  | 93.480  | 110.769 |         |         |         |         |         |         |         |         |         | Weight<br>lb/lf           | ( 317psi ) |
| 2.222"  | 2.444"  | 2.667"  | 2.889"  | 3.111"  | 3.333"  | 3.556"  |         |         |         |         |         |         | Min. wall                 |            |
| 15.289" | 16.818" | 18.347" | 19.876" | 21.404" | 22.933" | 24.462" |         |         |         |         |         |         | Average<br>I.D.           | DR 9       |
| 54.342  | 65.754  | 78.250  | 92.535  | 107.312 | 123.183 | 140.183 |         |         |         |         |         |         | Weight<br>lb/lf           | ( 250psi ) |
| 1.818"  | 2.000"  | 2.182"  | 2.364"  | 2.545"  | 2.727"  | 2.909"  | 3.091"  | 3.273"  |         |         |         |         | Min. wall                 |            |
| 16.145" | 17.760" | 19.375" | 20.989" | 22.604" | 24.218" | 25.833" | 27.447" | 29.062" |         |         |         |         | Average<br>I.D.           | DR 11      |
| 45.541  | 55.105  | 65.580  | 77.440  | 89.785  | 103.076 | 117.285 | 132.411 | 148.454 |         |         |         |         | Weight<br>lb/lf           | ( 200psi ) |
| 1.481"  | 1.630"  | 1.778"  | 1.926"  | 2.074"  | 2.222"  | 2.370"  | 2.519"  | 2.667"  | 3.111"  |         |         |         | Min. wall                 |            |
| 16.859" | 18.545" | 20.231" | 21.917" | 23.603" | 25.289" | 26.975" | 28.661" | 30.347" | 35.404" |         |         |         | Average<br>I.D.           | DR 13.5    |
| 37.840  | 45.790  | 54.490  | 64.261  | 74.522  | 85.543  | 97.324  | 109.905 | 123.208 | 167.675 |         |         |         | Weight<br>lb/lf           | ( 160psi ) |
| 1.290"  | 1.419"  | 1.548"  | 1.677"  | 1.806"  | 1.935"  | 2.065"  | 2.194"  | 2.323"  | 2.710"  | 3.097"  | 3.484"  |         | Min. wall                 |            |
| 17.265" | 18.991" | 20.717" | 22.444" | 24.170" | 25.897" | 27.623" | 29.350" | 31.076" | 36.255" | 41.435" | 46.614" |         | Average<br>I.D.           | DR 15.5    |
| 33.280  | 39.712  | 47.920  | 56.532  | 65.563  | 75.264  | 85.672  | 96.714  | 108.424 | 147.568 | 192.774 | 243.921 |         | Weight<br>lb/lf           | ( 138psi ) |
| 1.176"  | 1.294"  | 1.412"  | 1.529"  | 1.647"  | 1.765"  | 1.882"  | 2.000"  | 2.118"  | 2.471"  | 2.824"  | 3.176"  |         | Min. wall                 |            |
| 17.506" | 19.256" | 21.007" | 22.758" | 24.508" | 26.259" | 28.009" | 29.760" | 31.511" | 36.762" | 42.014" | 47.266" |         | Average<br>I.D.           | DR 17      |
| 30.580  | 37.000  | 44.031  | 51.856  | 60.154  | 69.068  | 78.557  | 88.700  | 99.457  | 135.372 | 176.813 | 223.713 |         | Weight<br>lb/lf           | ( 125psi ) |
| 0.952"  | 1.048"  | 1.143"  | 1.238"  | 1.333"  | 1.429"  | 1.524"  | 1.619"  | 1.714"  | 2.000"  | 2.286"  | 2.571"  | 3.000"  | Min. wall                 |            |
| 17.981" | 19.779" | 21.577" | 23.375" | 25.173" | 26.971" | 28.770" | 30.568" | 32.366" | 37.760" | 43.154" | 48.549" | 56.631" | Average<br>I.D.           | DR 21      |
| 25.070  | 30.330  | 36.100  | 42.486  | 49.266  | 56.585  | 64.370  | 72.657  | 81.446  | 110.874 | 144.833 | 183.253 | 249.570 | Weight<br>lb/lf           | ( 100psi ) |
| 0.769"  | 0.846"  | 0.923"  | 1.000"  | 1.077"  | 1.154"  | 1.231"  | 1.308"  | 1.385"  | 1.615"  | 1.846"  | 2.077"  | 2.423"  | Min. wall                 |            |
| 18.369" | 20.206" | 22.043" | 23.880" | 25.717" | 27.554" | 29.391" | 31.228" | 33.065" | 38.575" | 44.086" | 49.597" | 57.854" | Average<br>I.D.           | DR 26      |
| 20.453  | 24.750  | 29.452  | 34.570  | 40.187  | 46.135  | 52.494  | 59.264  | 66.444  | 90.393  | 118.082 | 149.464 | 203.630 | Weight<br>lb/lf           | ( 80 psi ) |
| 0.615"  | 0.677"  | 0.738"  | 0.800"  | 0.862"  | 0.923"  | 0.985"  | 1.046"  | 1.108"  | 1.292"  | 1.477"  | 1.662"  | 1.938"  | Min. wall                 | ٦          |
| 18.695" | 20.565" | 22.434" | 24.304" | 26.174" | 28.043" | 29.913" | 31.782" | 33.652" | 39.260" | 44.869" | 50.478" | 58.881" | Average<br>I.D.           | DR 32.5    |
| 16.501  | 19.970  | 23.762  | 27.940  | 32.421  | 37.196  | 42.340  | 47.773  | 53.581  | 72.893  | 95.233  | 120.556 | 164.280 | Weight<br>lb/lf           | ( 63 psi ) |



#### **HDPE** Pipe

- Items highlighted in Blue indicates standard stocking items that are more readily available.
- Pressures are based on using water at 23°C (73°F).
- Average inside diameter calculated using nominal OD and minimum wall plus 6% for use in estimating fluid flows. Actual ID will vary.
- Service factors should be utilized to compensate for the effect of liquids other than water, and for other temperatures.
- Other piping sizes or DR's may be available upon request.
- Standard Lengths: 40' for 2"-24" 50' for 26" and larger Coils available for 3/4"-6"(8" by special order)

1-800-345-ISCO

www.isco-pipe.com



19

#### Sub-Appendix D.2

#### **Pressure Test Forms**

**Feezor Engineering, Inc.** 3377 Hollenberg Dr. Bridgeton, MO 63044



#### **PIPELINE FIELD TESTING REPORT**

Client: Bridgeton Landfill LLC Date: 8/15/2017

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Page: 1

Engineers/Owner Rep: Bill Abernathy

**Contractors Rep: Jason Carter** 

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

GEW-201, 40, 40R, 203, 202, 55, 55R, 204, 53, 53R, 207, 41R, 41R2, 43R, 43R2, 205, 206, 44, 51, 211, 214,

49, 212, 54, 54R

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Gas Headers/Laterals** 

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

#### **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | Start Time  |
|------------------------------|-------------------------------|-------------|
| 10                           | 65                            | 9:30        |
| 10                           | 65                            | 9:40        |
| 10                           | 67                            | 9:50        |
| 10                           | 67                            | 10:00       |
| 10                           | 69                            | 10:10       |
| 10                           | 69                            | 10:20       |
| 10                           | 70                            | 10:53       |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time |
| 10                           | 70                            | 10:53       |

| Comments: Pass / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |

**Date Test Performed.:** 8/15/2017

Engineers/Owners Rep.:

**Feezor Engineering, Inc.** 3377 Hollenberg Dr. Bridgeton, MO 63044



#### **PIPELINE FIELD TESTING REPORT**

Date: 8/15/2017

Job No.: BT-125

Page: 2

Client: Bridgeton Landfill LLC

**Project: Phase 1 North Quarry EVOH Cover System** 

Engineers/Owner Rep: Bill Abernathy
Contractors Rep: Jason Carter

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

GEW-42R, 200

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Gas Headers/Laterals** 

**Type of Test**: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

#### **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | <u>Start Time</u> |
|------------------------------|-------------------------------|-------------------|
| 10                           | 81                            | 17:04             |
| 10                           | 81                            | 17:14             |
| 10                           | 81                            | 17:24             |
| 10                           | 81                            | 17:34             |
| 10                           | 81                            | 17:44             |
| 10                           | 81                            | 17:54             |
| 10                           | 81                            | 18:08             |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time       |
| 10                           | 81                            | 18:08             |

| Comments: | Pass / Fail | (Circle One) |  |  |
|-----------|-------------|--------------|--|--|
|           |             |              |  |  |

Date Test Performed.: 8/15/2017

**Engineers/Owners Rep.:** 

**Feezor Engineering, Inc.** 3377 Hollenberg Dr. Bridgeton, MO 63044



#### **PIPELINE FIELD TESTING REPORT**

Client: Bridgeton Landfill LLC

Date: 8/16/2017

**Project: Phase 1 North Quarry EVOH Cover System** 

Job No.: BT-125

**Engineers/Owner Rep: Bill Abernathy** 

Page: 3

**Contractors Rep: Jason Carter** 

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

GEW-2, 3, 4, 46R

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Gas Headers/Laterals** 

**Type of Test**: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

#### **Test Results**

| Start Pressure (PSI)         | Temperature (F)        | Start Time  |
|------------------------------|------------------------|-------------|
| 10                           | 79                     | 11:36       |
| 10                           | 79                     | 11:46       |
| 10                           | 79                     | 11:56       |
| 10                           | 80                     | 12:06       |
| 10                           | 80                     | 12:16       |
| 10                           | 80                     | 12:26       |
| 10                           | 81                     | 13:08       |
| <b>Ending Pressure (PSI)</b> | Ending Temperature (F) | Ending Time |
| 10                           | 80                     | 13:08       |

| Comments: Pass / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |

Date Test Performed.: 8/16/2017

**Engineers/Owners Rep.:** 

mil Jahret



## **PIPELINE FIELD TESTING REPORT**

Client: Bridgeton Landfill LLC

Date: 8/17/2017

**Project: Phase 1 North Quarry EVOH Cover System** 

Job No.: BT-125

Engineers/Owner Rep: Bill Abernathy

Page: 4

Contractors Rep: Jason Carter

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

GEW-45, 47R

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Gas Headers/Laterals** 

**Type of Test**: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)        | Start Time  |
|------------------------------|------------------------|-------------|
| 10                           | 77                     | 9:43        |
| 10                           | 77                     | 9:53        |
| 10                           | 79                     | 10:03       |
| 10                           | 79                     | 10:13       |
| 10                           | 79                     | 10:23       |
| 10                           | 79                     | 10:33       |
| 10                           | 81                     | 13:58       |
| <b>Ending Pressure (PSI)</b> | Ending Temperature (F) | Ending Time |
| 10                           | 81                     | 13:58       |

| Comments: | Pass / Fail | (Circle One) |  |
|-----------|-------------|--------------|--|
|           |             |              |  |

Date Test Performed.: 8/17/2017

**Engineers/Owners Rep.:** 

miljahr



## PIPELINE FIELD TESTING REPORT

Client: Bridgeton Landfill LLC Date: 8/18/2017

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Page: 5

Engineers/Owner Rep: Jon Wilkinson

**Contractors Rep: Jason Carter** 

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at PZ-109-SS, running clockwise around north quarry, past CT-10, past GEW-2S, then splitting at tee located immediately downhill of GEW-2. One part of pipe extends from tee, past GEW-2, past GEW-3, and ends near GEW-4. Other part of pipe extends from tee and follows surface water ditch to PZ-104R-SS.

Description: (Material and Line Usage - HDPE -Header, HDPE Force-main)

HDPE SDR 11 - Forcemain - 3" carrier

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)        | Start Time  |
|------------------------------|------------------------|-------------|
| 100                          | 81                     | 10:30       |
| 100                          | 81                     | 10:40       |
| 100                          | 81                     | 10:50       |
| 100                          | 81                     | 11:00       |
| 100                          | 81                     | 11:10       |
| 100                          | 81                     | 11:20       |
| 100                          | 81                     | 12:00       |
| <b>Ending Pressure (PSI)</b> | Ending Temperature (F) | Ending Time |
| 100                          | 81                     | 12:00       |

| Comments: | Pas / Fail | (Circle One) |  |  |
|-----------|------------|--------------|--|--|
|           |            |              |  |  |
|           |            |              |  |  |

Date Test Performed.: 8/18/2017
Engineers/Owners Rep.:



## **PIPELINE FIELD TESTING REPORT**

Client: Bridgeton Landfill LLC Date: 8/18/2017

Page: 6

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson

**Contractors Rep: Jason Carter** 

Location: (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at PZ-102R-SS, running along anchor trench to end adjacent to flare station.

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

HDPE SDR 11 - Forcemain - 3" carrier

**Type of Test:** (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | Start Time  |
|------------------------------|-------------------------------|-------------|
| 100                          | 89                            | 15:00       |
| 100                          | 89                            | 15:10       |
| 100                          | 89                            | 15:20       |
| 100                          | 89                            | 15:30       |
| 100                          | 89                            | 15:40       |
| 100                          | 90                            | 15:50       |
| 100                          | 90                            | 16:05       |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time |
| 100                          | 90                            | 16:05       |

| Comments: Pass / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |
|                       |              |

Date Test Performed.: 8/18/2017
Engineers/Owners Rep.:



## **PIPELINE FIELD TESTING REPORT**

Client: Bridgeton Landfill LLC Date: 8/18/2017

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Bill Abernathy Page: 7

**Contractors Rep: Jason Carter** 

Location: (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at PZ-102R-SS, running along anchor trench to end adjacent to flare station.

**Description:** (Material and Line Usage - HDPE -Header, HDPE Force-main)

HDPE SDR 17 - Forcemain - 6" Containment

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

#### **Test Results**

| Start Pressure (PSI)  | Temperature (F)        | Start Time  |
|-----------------------|------------------------|-------------|
| 10                    | 89                     | 15:00       |
| 10                    | 89                     | 15:10       |
| 10                    | 89                     | 15:20       |
| 10                    | 89                     | 15:30       |
| 10                    | 89                     | 15:40       |
| 10                    | 90                     | 15:50       |
| 10                    | 90                     | 16:05       |
| Ending Pressure (PSI) | Ending Temperature (F) | Ending Time |
| 10                    | 90                     | 16:05       |

| Comments: Pass / Fail (Circle One) |           |  |
|------------------------------------|-----------|--|
|                                    |           |  |
| Date Test Performed.:              | 8/18/2017 |  |
| Date Test Performed.:              | 8/18/2017 |  |



## PIPELINE FIELD TESTING REPORT

Date: 8/19/2017

Job No.: BT-125

Page: 8

Client: Bridgeton Landfill LLC

Project: Phase 1 North Quarry EVOH Cover System

Engineers/Owner Rep: Jon Wilkinson
Contractors Rep: Jason Carter

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at GEW-47R to near LCS-6B, then splitting at tee near LCS-6B. One part of pipe extends from tee to GEW-4. Other part of pipe extends from tee to CT near PEW-53 and PEW-52.

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 9 - Airline** 

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | Start Time  |
|------------------------------|-------------------------------|-------------|
| 100                          | 71                            | 7:00        |
| 100                          | 71                            | 7:10        |
| 100                          | 73                            | 7:20        |
| 100                          | 73                            | 7:30        |
| 100                          | 73                            | 7:40        |
| 100                          | 75                            | 7:50        |
| 100                          | 75                            | 8:00        |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time |
| 100                          | 75                            | 8:00        |

| Comments: Pas: / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |

Date Test Performed.:

**Engineers/Owners Rep.:** 

8/19/2017



## PIPELINE FIELD TESTING REPORT

Client: Bridgeton Landfill LLC Date: 8/19/2017

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson Page: 9

**Contractors Rep: Jason Carter** 

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at PEW-52/PEW-53, then going uphill past GEW-49, past GEW-214, then to blind flange near TMP-44. From blind flange, continues past GEW-211, past GEW-207, past GEW-54/54R, to anchor trench downhill of of GEW-41/41R, then uphill to GEW-40R, past GEW-55/55R and ends at GEW-53/53R

**Description:** (Material and Line Usage - HDPE -Header, HDPE Force-main)

HDPE SDR 11 - Forcemain 3" carrier

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | <u>Start Time</u> |
|------------------------------|-------------------------------|-------------------|
| 100                          | 78                            | 9:00              |
| 100                          | 78                            | 9:10              |
| 100                          | 78                            | 9:20              |
| 100                          | 80                            | 9:30              |
| 100                          | 80                            | 9:40              |
| 100                          | 80                            | 9:50              |
| 100                          | 81                            | 10:00             |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time       |
| 100                          | 81                            | 10:00             |

| Comments: Pass / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |

Date Test Performed.: 8/19/2017
Engineers/Owners Rep.:



## PIPELINE FIELD TESTING REPORT

Client: Bridgeton Landfill LLC Date: 8/19/2017

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson Page: 10

**Contractors Rep: Jason Carter** 

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at PEW-52/PEW-53, then going uphill past GEW-49, past GEW-214, then to blind flange near TMP-44. From blind flange, continues past GEW-211, past GEW-207, past GEW-54/54R, to anchor trench downhill of of GEW-41/41R, then uphill to GEW-40R, past GEW-55/55R and ends at GEW-53/53R

**Description:** (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Forcemain 6" Containment** 

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)                  | <u>Start Time</u> |
|------------------------------|----------------------------------|-------------------|
| 10                           | 78                               | 9:00              |
| 10                           | 78                               | 9:10              |
| 10                           | 78                               | 9:20              |
| 10                           | 80                               | 9:30              |
| 10                           | 80                               | 9:40              |
| 10                           | 80                               | 9:50              |
| 10                           | 81                               | 10:00             |
| <b>Ending Pressure (PSI)</b> | Ending Temperature (F) Ending Ti |                   |
| 10                           | 81                               | 10:00             |

| Comments: | Pass / Fail | (Circle One) |  |  |
|-----------|-------------|--------------|--|--|
|           |             |              |  |  |

Date Test Performed.: 8/19/2017

**Engineers/Owners Rep.:** 



## PIPELINE FIELD TESTING REPORT

Client: Bridgeton Landfill LLC Date: 8/19/2017

Page: 11

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson
Contractors Rep: Jason Carter

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at TMP-47/48, runs past LCS-6B, splits into wye. One line from wye terminates at GEW-47R.

Other line from wye terminates at unlabeled CT near PEW-53 and PEW-52

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 11 - Forcemain 3" Carrier** 

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | <u>Temperature (F)</u> <u>Start Time</u> |             |
|------------------------------|--|-------------|
| 100                          | 82                                       | 10:45       |
| 100                          | 84                                       | 10:55       |
| 100                          | 84                                       | 11:05       |
| 100                          | 86                                       | 11:15       |
| 100                          | 86                                       | 11:25       |
| 100                          | 86                                       | 11:35       |
| 100                          | 88                                       | 12:15       |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b>            | Ending Time |
| 100                          | 88                                       | 12:15       |

| Comments: | Pas: / Fail | (Circle One) |  |  |
|-----------|-------------|--------------|--|--|
|           |             |              |  |  |
|           |             |              |  |  |

Date Test Performed.: 8/19/2017

**Engineers/Owners Rep.:** 

All



## PIPELINE FIELD TESTING REPORT

Client: Bridgeton Landfill LLC Date: 8/19/2017

Page: 12

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson
Contractors Rep: Jason Carter

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at TMP-47/48, runs past LCS-6B, splits into wye. One line from wye terminates at GEW-47R.

Other line from wye terminates at unlabeled CT near PEW-53 and PEW-52

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Forcemain 6" Containment** 

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | Start Time  |
|------------------------------|-------------------------------|-------------|
| 10                           | 82                            | 10:45       |
| 10                           | 84                            | 10:55       |
| 10                           | 84                            | 11:05       |
| 10                           | 86                            | 11:15       |
| 10                           | 86                            | 11:25       |
| 10                           | 86                            | 11:35       |
| 10                           | 88                            | 12:15       |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time |
| 10                           | 88                            | 12:15       |

| Comments: Pass / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |

Date Test Performed.: 8/19/2017

**Engineers/Owners Rep.:** 



#### PIPELINE FIELD TESTING REPORT

Client: Bridgeton Landfill LLC Date: 8/19/2017

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson Page: 13

**Contractors Rep: Jason Carter** 

Location: (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at GEW-4 and passes GEW-3, GEW-2, then proceeds downhill to perimeter access road. The line splits at a tee. The pipe from one leads to CT-11. The other splits into another tee a few feet away. One side from the second tee leads to GEW-46R. Other pipe from second tee leads clockwise around perimeter access road to road crossing 4, near CT-12.

**Description:** (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 9 - Airline** 

**Type of Test**: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

#### **Test Results**

| Start Pressure (PSI)         | <u>Temperature (F)</u> <u>Start Time</u> |             |
|------------------------------|--|-------------|
| 100                          | 86                                       | 11:15       |
| 100                          | 86                                       | 11:25       |
| 100                          | 86                                       | 11:35       |
| 100                          | 88                                       | 11:45       |
| 100                          | 88                                       | 11:55       |
| 100                          | 88                                       | 12:05       |
| 100                          | 88                                       | 12:15       |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b>            | Ending Time |
| 100                          | 88                                       | 12:15       |

| Comments: Pass / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |
|                       |              |

Date Test Performed.: 8/19/2017

**Engineers/Owners Rep.:** 

file



## PIPELINE FIELD TESTING REPORT

Client: Bridgeton Landfill LLC Date: 8/19/2017

Page: 14

Project: Phase 1 North Quarry EVOH Cover System Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson
Contractors Rep: Jason Carter

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at PZ-109-SS, running clockwise around north quarry, past CT-10, past GEW-2S, then splitting at tee located immediately downhill of GEW-2. One part of pipe extends from tee, past GEW-2, past GEW-3, and ends near GEW-4. Other part of pipe extends from tee and follows surface water ditch to PZ-104R-SS.

Description: (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Forcemain 6" Containment** 

Type of Test: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | <u>Temperature (F)</u>        | <u>Start Time</u> |
|------------------------------|-------------------------------|-------------------|
| 10                           | 81                            | 13:09             |
| 10                           | 85                            | 13:19             |
| 10                           | 89                            | 13:29             |
| 10                           | 89                            | 13:39             |
| 10                           | 89                            | 13:49             |
| 10                           | 89                            | 13:59             |
| 10                           | 89                            | 14:10             |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time       |
| 10                           | 89                            | 14:10             |

| Comments: Pas: / Fail | (Circle One) |
|-----------------------|--------------|
|                       |              |

Date Test Performed.: 8/19/2017

**Engineers/Owners Rep.:** 



## **PIPELINE FIELD TESTING REPORT**

Client: Bridgeton Landfill LLC

Date: 8/19/2017

**Project: Phase 1 North Quarry EVOH Cover System** 

Job No.: BT-125

Engineers/Owner Rep: Jon Wilkinson

Page: 15

**Contractors Rep: Jason Carter** 

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

Beginning at PEW-48 and leading uphill to GEW-42/42R

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 9 - Airline** 

**Type of Test**: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | <b>Start Time</b> |
|------------------------------|-------------------------------|-------------------|
| 100                          | 89                            | 14:20             |
| 100                          | 89                            | 14:30             |
| 100                          | 89                            | 14:40             |
| 100                          | 89                            | 14:50             |
| 100                          | 88                            | 15:00             |
| 100                          | 88                            | 15:10             |
| 100                          | 88                            | 15:25             |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time       |
| 100                          | 88                            | 15:25             |

| <b>Comments:</b> F | Pass / Fail | (Circle One) |  |  |
|--------------------|-------------|--------------|--|--|
|                    |             |              |  |  |
|                    |             |              |  |  |

Date Test Performed.: 8/19/2017

**Engineers/Owners Rep.:** 

ffl-



## **PIPELINE FIELD TESTING REPORT**

Date: 8/21/2017

Job No.: BT-125

Page: 16

**Client: Bridgeton Landfill LLC** 

**Project: Phase 1 North Quarry EVOH Cover System** 

Engineers/Owner Rep: Bill Abernathy

**Contractors Rep: Jason Carter** 

**Location:** (Bldg. to Bldg., Struct. to Struct., M.H. to M.H., Sta. to Sta., etc.)

GEW-42, 200

<u>Description:</u> (Material and Line Usage - HDPE -Header, HDPE Force-main)

**HDPE SDR 17 - Forcemain 6" Containment** 

**Type of Test**: (Air, Hydrostatic, Infiltration, Exfiltration, Other)

AIR

## **Test Results**

| Start Pressure (PSI)         | Temperature (F)               | Start Time  |
|------------------------------|-------------------------------|-------------|
| 10                           | 82                            | 7:00        |
| 10                           | 82                            | 7:10        |
| 10                           | 82                            | 7:20        |
| 10                           | 82                            | 7:30        |
| 10                           | 82                            | 7:40        |
| 10                           | 82                            | 7:50        |
| 10                           | 82                            | 8:48        |
| <b>Ending Pressure (PSI)</b> | <b>Ending Temperature (F)</b> | Ending Time |
| 10                           | 82                            | 8:48        |

| Comments: | Pas: / Fail | (Circle One) |
|-----------|-------------|--------------|
|           |             |              |

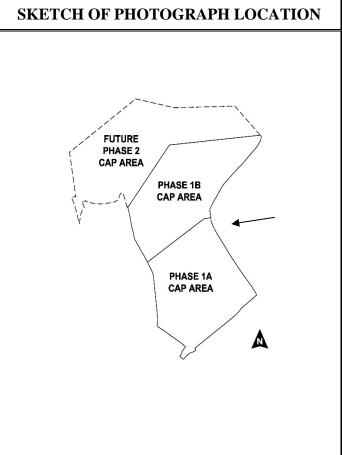
Date Test Performed.: 8/21/2017

Engineers/Owners Rep.:

## APPENDIX E CONSTRUCTION PHOTOGRAPHS

| PHOTOGRAPHIC RECORD FORM  |                                  |                        |               |
|---|----------------------------------|------------------------|---------------|
| Project Name: North   | Quarry EVOH Liner CQA            | Project Number: BT-125 |               |
| Photograph: 1   | Filename: IMG_20161201_140019177 | Date: 12/1/16          | Time: 2:00 PM |
| Comments: Initial stakeout and grading of fill before EVOH liner. |                                  |                        |               |
| Photographer's Signature:   |                                  | Typed: Andrew Roberts  |               |







#### PHOTOGRAPHIC RECORD FORM Project Name: North Quarry EVOH Liner CQA Project Number: BT-125 Filename: IMG\_20161203\_124511399 Photograph: 2 Date: 12/3/16 Time: 12:45 PM Comments: Fill and grading work. Photographer's Signature:

Typed: Andrew Roberts



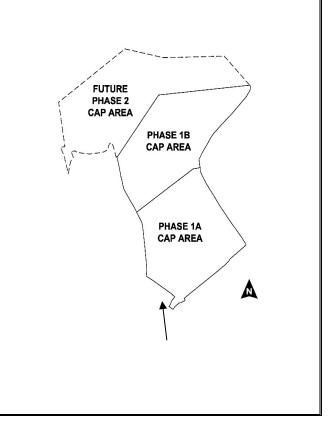
## SKETCH OF PHOTOGRAPH LOCATION FUTURE PHASE 2 CAP AREA PHASE 1B CAP AREA

PHASE 1A CAP AREA



## Project Name: North Quarry EVOH Liner CQA Project Number: BT-125 Photograph: 3 Filename: IMG\_20161203\_124513071 Date: 12/3/16 Time: 12:45 PM Comments: Fill and grading work. Photographer's Signature: Typed: Andrew Roberts

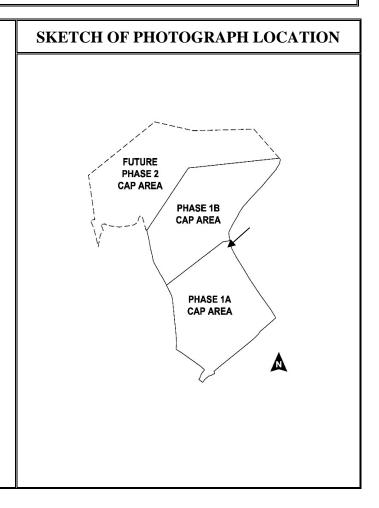






## Project Name: North Quarry EVOH Liner CQA Project Number: BT-125 Photograph: 4 Filename: 20170321\_153152 Date: 3/21/17 Photographer's Signature: Typed: Arron Weber

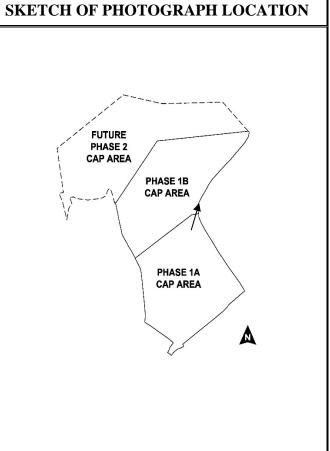






## Project Name: North Quarry EVOH Liner CQA Project Number: BT-125 Photograph: 5 Filename: 20170322\_085907 Date: 3/22/17 Photographer's Signature: Typed: Arron Weber

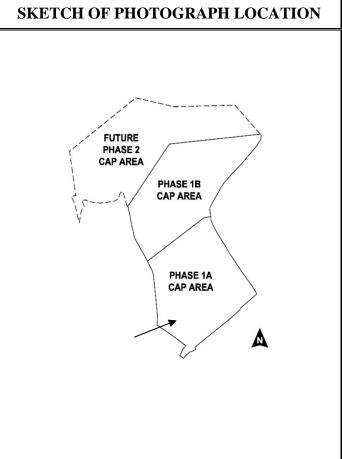






| PHOTOGRAPHIC RECORD FORM                                 |                           |                        |                |
|--|---------------------------|------------------------|----------------|
| Project Name: North                                      | Quarry EVOH Liner CQA     | Project Number: BT-125 |                |
| Photograph: 6  | Filename: 20170515_110856 | Date: 5/15/17          | Time: 11:08 AM |
| Comments: Placement and grading of necessary fill soils. |                           |                        |                |
| Photographer's Signature:                                |                           | Typed: Arron Weber     |                |







#### PHOTOGRAPHIC RECORD FORM Project Name: North Quarry EVOH Liner CQA Project Number: BT-125 Filename: 20170516\_151239 Photograph: 7 Date: 5/16/17 Time: 3:12 PM Comments: Installation of geocomposite layer under EVOH liner for roads. Photographer's Signature:

Typed: Arron Weber

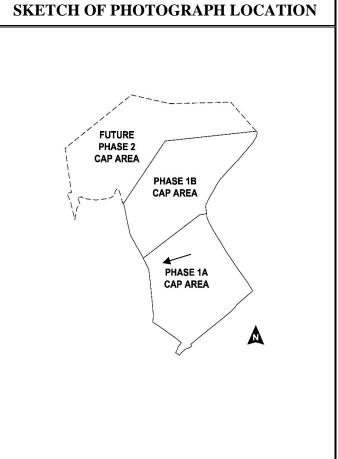


## SKETCH OF PHOTOGRAPH LOCATION **FUTURE** PHASE 2 CAP AREA PHASE 1B CAP AREA PHASE 1A CAP AREA



## Project Name: North Quarry EVOH Liner CQA Project Number: BT-125 Photograph: 8 Filename: 20170522\_132644 Date: 5/22/17 Photographer's Signature: Typed: Arron Weber







## PHOTOGRAPHIC RECORD FORM

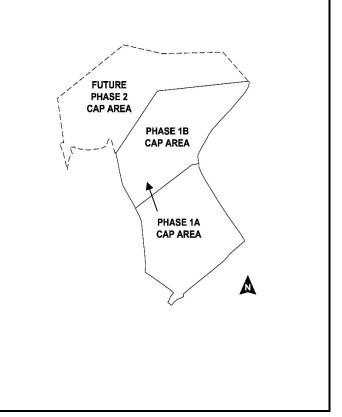
Project Name: North Quarry EVOH Liner CQA Project Number: BT-125

Photograph: 9 | Filename: 20170522\_132817 | Date: 5/22/17 | Time: 1:28 PM

Comments: Installation of geocomposite layer over EVOH liner for roads.

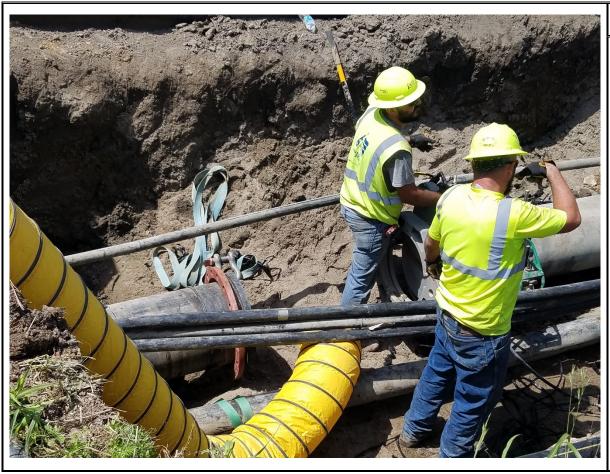
Photographer's Signature: Typed: Arron Weber

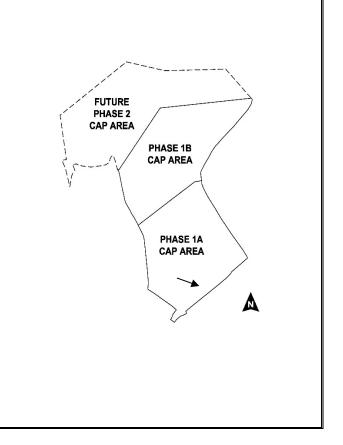






## Project Name: North Quarry EVOH Liner CQA Project Number: BT-125 Photograph: 10 Filename: 20170530\_144257 Date: 5/30/17 Photographer's Signature: Typed: Arron Weber

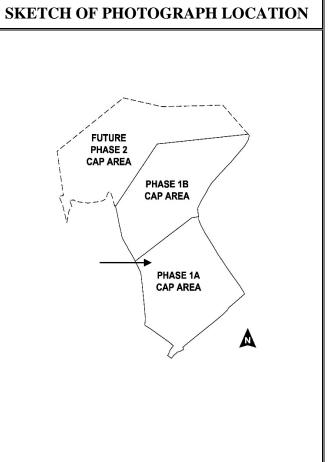






| PHOTOGRAPHIC RECORD FORM                                   |                       |                             |  |
|--|-----------------------|-----------------------------|--|
| Project Name: North  | Quarry EVOH Liner CQA | Project Number: BT-125      |  |
| Photograph: 11   | Filename: IMG_2209    | Date: 6/1/17 Time: 11:06 AM |  |
| Comments: Installation of cushion geotextile.              |                       |                             |  |
| Photographer's Signature: 359.0556 Typed: Bradley DalSanto |                       |                             |  |

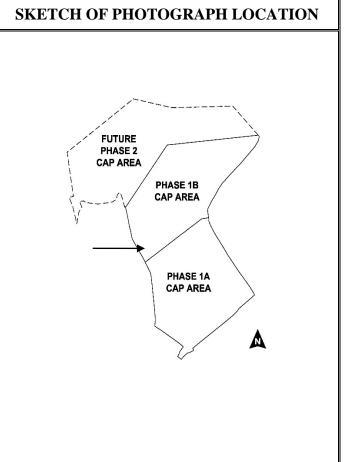






| PHOTOGRAPHIC RECORD FORM                                    |                       |                        |                |
|---|-----------------------|------------------------|----------------|
| Project Name: North   | Quarry EVOH Liner CQA | Project Number: BT-125 |                |
| Photograph: 12  | Filename: IMG_2210    | Date: 6/1/17           | Time: 11:35 AM |
| Comments: Installation of EVOH liner.                       |                       |                        |                |
| Photographer's Signature: 350.0556  Typed: Bradley DalSanto |                       |                        |                |

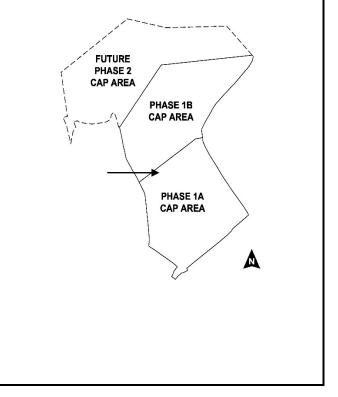






| PHOTOGRAPHIC RECORD FORM                                   |                         |                        |                |
|--|-------------------------|------------------------|----------------|
| Project Name: North  | n Quarry EVOH Liner CQA | Project Number: BT-12: | 5              |
| Photograph: 13   | Filename: IMG_2214      | Date: 6/2/17           | Time: 11:18 AM |
| Comments: Using field tensiometer on EVOH liner.           |                         |                        |                |
| Photographer's Signature: 350.0556 Typed: Bradley DalSanto |                         | to                     |                |

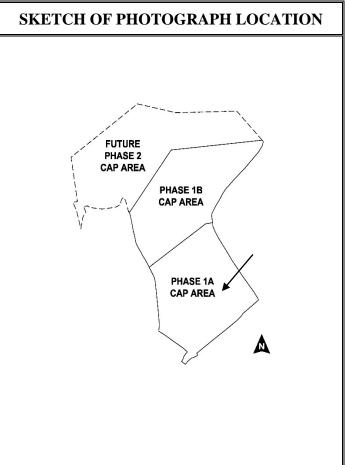






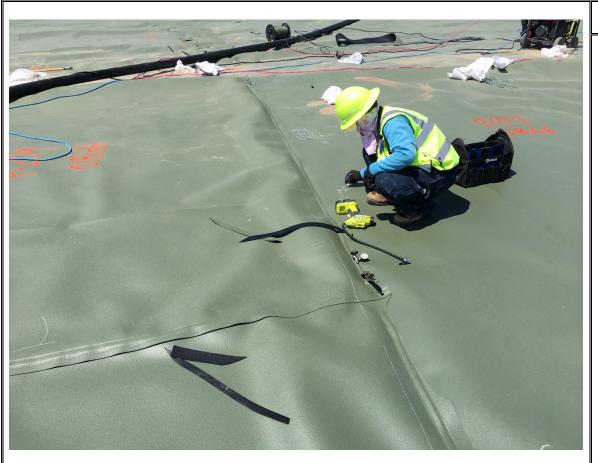
## Project Name: North Quarry EVOH liner CQA Project Number: BT-125 Photograph: 14 Filename: IMG\_2226 Comments: Installation of gas piping. Photographer's Signature: 350.056 Typed: Bradley DalSanto

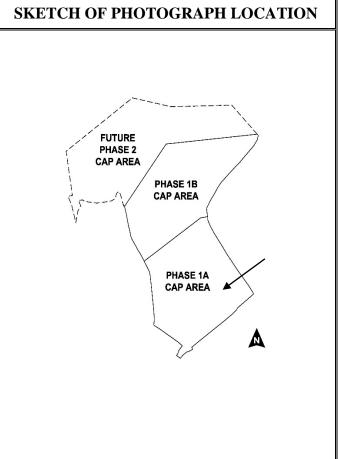






| PHOTOGRAPHIC RECORD FORM                                   |                         |                        |                |
|--|-------------------------|------------------------|----------------|
| Project Name: North  | n Quarry EVOH Liner CQA | Project Number: BT-125 |                |
| Photograph: 15   | Filename: IMG_2227      | Date: 6/13/17          | Time: 11:09 AM |
| Comments: Air testing EVOH fusion weld.                    |                         |                        |                |
| Photographer's Signature: 359.0556 Typed: Bradley DalSanto |                         |                        |                |







## **APPENDIX F**

#### **CONSTRUCTION CERTIFICATION DRAWINGS**

| Drawing 001 | Title Page                               |
|-------------|--|
| Drawing 002 | Summary of Site Works                    |
| Drawing 003 | Grading Plan View                        |
| Drawing 004 | EVOH Cover Undercap Plan View            |
| Drawing 005 | <b>EVOH Cover Panel Layout Plan View</b> |
| Drawing 006 | EVOH Cover Overcap Plan View             |
| Drawing 007 | Details 1                                |
| Drawing 008 | Details 2                                |
| Drawing 009 | Details 3                                |
| Drawing 010 | Details 4                                |
| Drawing 011 | Details 5                                |
| Drawing 012 | Details 6                                |
| Drawing 013 | Details 7                                |
| Drawing 014 | Details 8                                |
|             |  |

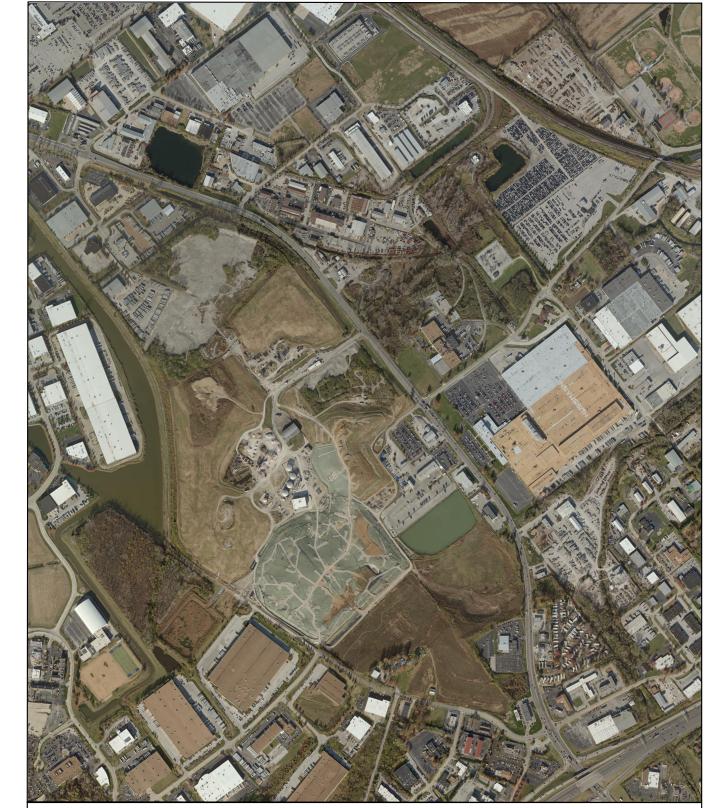
## AS-BUILT RECORD DRAWINGS FOR THE

# BRIDGETON LANDFILL NORTH QUARRY PHASE 1 EVOH COVER

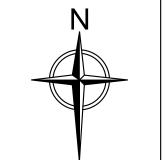
# OCTOBER 2017 PREPARED FOR:

## BRIDGETON LANDFILL, LLC

13570 ST. CHARLES ROCK ROAD BRIDGETON, MISSOURI 63044



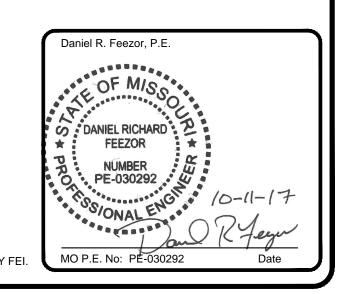
LOCATION MAP

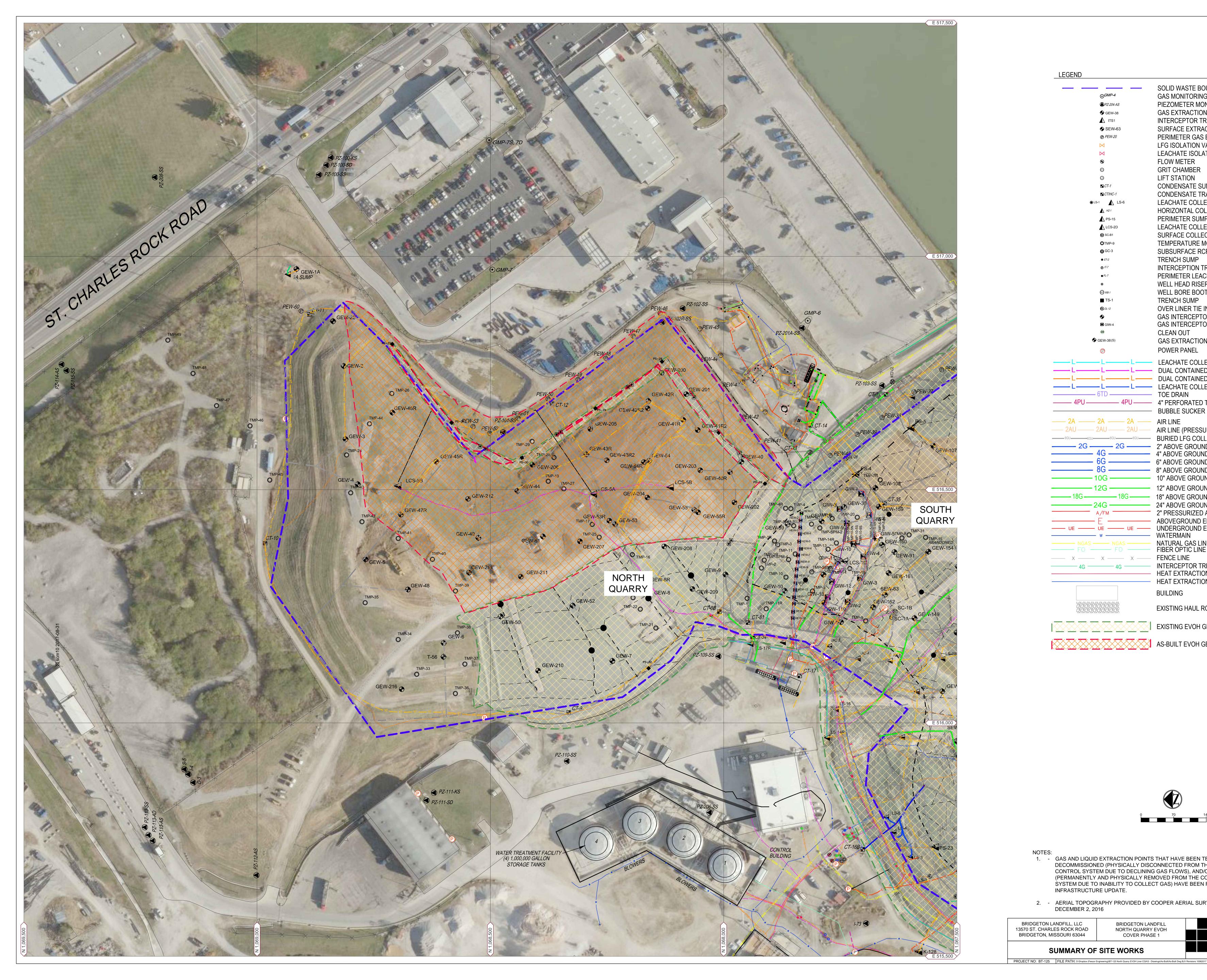


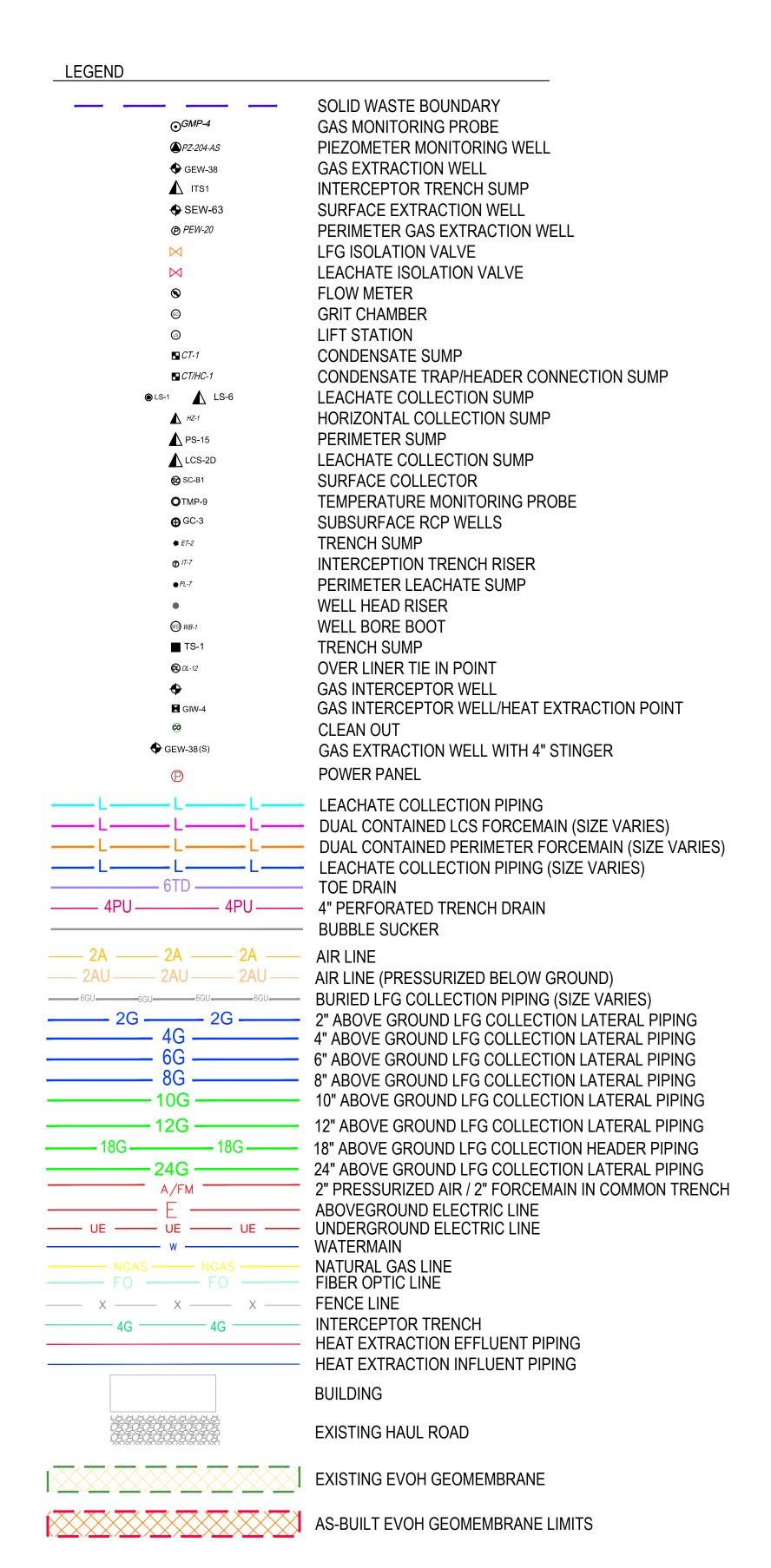


3377 HOLLENBERG DRIVE BRIDGETON, MO 63044

| INDEX OF DRAWINGS |                                   |
|-------------------|-----------------------------------|
| 001               | TITLE PAGE                        |
| 002               | SUMMARY OF SITE WORKS             |
| 003               | GRADING PLAN VIEW                 |
| 004               | EVOH COVER UNDERCAP PLAN VIEW     |
| 005               | EVOH COVER PANEL LAYOUT PLAN VIEW |
| 006               | EVOH COVER OVERCAP PLAN VIEW      |
| 007               | DETAILS #1                        |
| 008               | DETAILS #2                        |
| 009               | DETAILS #3                        |
| 010               | DETAILS #4                        |
| 011               | DETAILS #5                        |
| 012               | DETAILS #6                        |
| 013               | DETAILS #7                        |
| 014               | DETAILS #8                        |









1. - GAS AND LIQUID EXTRACTION POINTS THAT HAVE BEEN TEMPORARILY DECOMMISSIONED (PHYSICALLY DISCONNECTED FROM THE COLLECTION AND CONTROL SYSTEM DUE TO DECLINING GAS FLOWS), AND/OR ABANDONED, (PERMANENTLY AND PHYSICALLY REMOVED FROM THE COLLECTION AND CONTROL

INFRASTRUCTURE UPDATE.

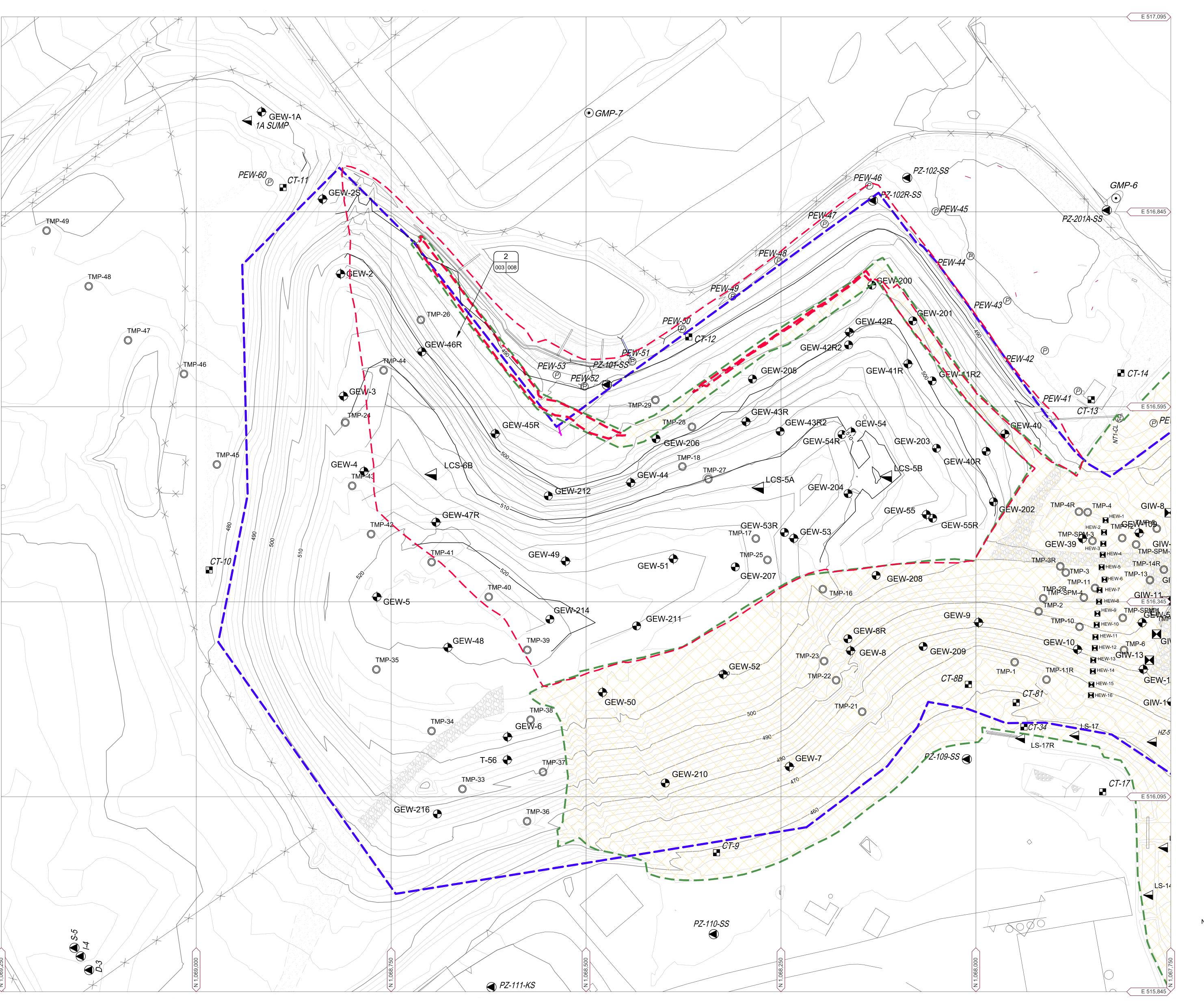
2. - AERIAL TOPOGRAPHY PROVIDED BY COOPER AERIAL SURVEYS, INC. AND IS DATED

DECEMBER 2, 2016 OCTOBER 2017 BRIDGETON LANDFILL, LLC **BRIDGETON LANDFILL** DESIGNED BY: IN 13570 ST. CHARLES ROCK ROAD NORTH QUARRY EVOH APPROVED BY: DRF BRIDGETON, MISSOURI 63044 **COVER PHASE 1 SUMMARY OF SITE WORKS** 

ENGINEERING, INC.

DRAWING NO.:

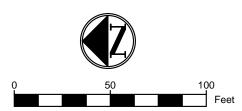
SYSTEM DUE TO INABILITY TO COLLECT GAS) HAVE BEEN REMOVED FROM THE SITE



SOLID WASTE BOUNDARY GAS MONITORING PROBE PIEZOMETER MONITORING WELL GAS EXTRACTION WELL **♦** GEW-38 INTERCEPTOR TRENCH SUMP ▲ ITS1 SURFACE EXTRACTION WELL **♦** SEW-63 PERIMETER GAS EXTRACTION WELL PEW-20 LFG ISOLATION VALVE LEACHATE ISOLATION VALVE **FLOW METER GRIT CHAMBER** LIFT STATION CONDENSATE SUMP CONDENSATE TRAP/HEADER CONNECTION SUMP **■** *CT/HC-1* LEACHATE COLLECTION SUMP HORIZONTAL COLLECTION SUMP PERIMETER SUMP A PS-15 LEACHATE COLLECTION SUMP LCS-2D SURFACE COLLECTOR **⊚** SC-B1 TEMPERATURE MONITORING PROBE **○**TMP-9 SUBSURFACE RCP WELLS TRENCH SUMP INTERCEPTION TRENCH RISER PERIMETER LEACHATE SUMP WELL HEAD RISER WELL BORE BOOT TRENCH SUMP OVER LINER TIE IN POINT GAS INTERCEPTOR WELL GAS INTERCEPTOR WELL/HEAT EXTRACTION POINT **CLEAN OUT** GAS EXTRACTION WELL WITH 4" STINGER **♦** GEW-38(S) POWER PANEL AERIAL TOPOGRAPHY (2' CONTOUR) AERIAL TOPOGRAPHY (10' CONTOUR) AS-BUILT GRADING (2' CONTOUR) - AS-BUILT GRADING (10' CONTOUR) EXISTING HAUL ROAD EXISTING EVOH GEOMEMBRANE

AS-BUILT EVOH GEOMEMBRANE LIMITS

LEGEND



1. - GAS AND LIQUID EXTRACTION POINTS THAT HAVE BEEN TEMPORARILY DECOMMISSIONED (PHYSICALLY DISCONNECTED FROM THE COLLECTION AND CONTROL SYSTEM DUE TO DECLINING GAS FLOWS), AND/OR ABANDONED, (PERMANENTLY AND PHYSICALLY REMOVED FROM THE COLLECTION AND CONTROL SYSTEM DUE TO INABILITY TO COLLECT GAS) HAVE BEEN REMOVED FROM THE SITE INFRASTRUCTURE UPDATE.

 AERIAL TOPOGRAPHY PROVIDED BY COOPER AERIAL SURVEYS, INC. AND IS DATED DECEMBER 2, 2016

BRIDGETON LANDFILL, LLC
13570 ST. CHARLES ROCK ROAD
BRIDGETON, MISSOURI 63044

COCTOBER 2017
DESIGNED BY: IN
APPROVED BY: DRF

COVER PHASE 1

DRAWING NO.:

FEEOR
Engineering for a Better World
ENGINEERING, INC.

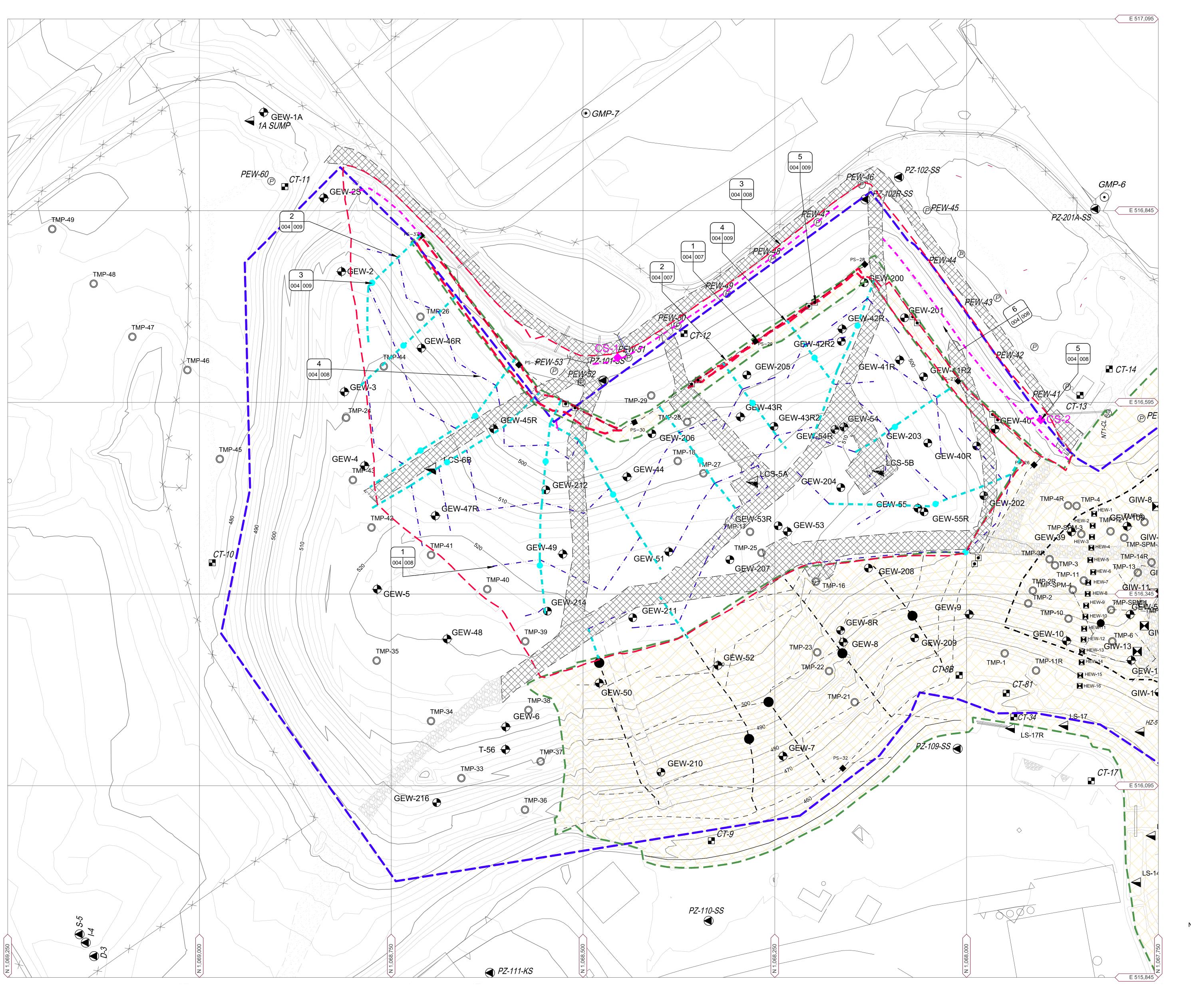
PROJECT NO: BT-125
FILE PATH: D\Dropbox (Feezor Engineering)\BT-125 North Quarry EVOH Liner CQA\S- Drawings\As-Built\As-Built Dwg BJV Revisions 10062017

DRAWING NO.:

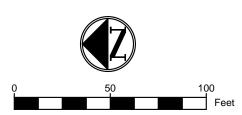
DRAWING NO.:

DRAWING NO.:

REVISION DATE



LEGEND SOLID WASTE BOUNDARY **EXISTING GAS EXTRACTION WELL** EXISTING PERIMETER GAS EXTRACTION WELL EXISTING CONDENSATE SUMP **■** CT-1 EXISTING CONDENSATE TRAP/HEADER CONNECTION SUMP **⊞** CT/HC-1 EXISTING LEACHATE COLLECTION SUMP LCS-2D EXISTING TEMPERATURE MONITORING PROBE **○**TMP-9 AERIAL TOPOGRAPHY (2' CONTOUR) AERIAL TOPOGRAPHY (10' CONTOUR) AS-BUILT GRADING (2' CONTOUR) AS-BUILT GRADING (10' CONTOUR) EXISTING PERIMETER COLLECTION DRAIN EXISTING PERIMETER COLLECTION DRAIN SUMP EXISTING DOWNSLOPE STRIP DRAIN COLLECTOR EXISTING DOWNSLOPE STRIP DRAIN COLLECTOR SUMP RISER EXISTING STRIP DRAIN PROPOSED DRAINAGE CHANNEL EXISTING EVOH GEOMEMBRANE AS-BUILT ROAD UNDERLAY GEOCOMPOSITE AS-BUILT EVOH GEOMEMBRANE LIMITS - AS-BUILT STRIP DRAIN TOE COLLECTOR AS-BUILT EVOH DOWNSLOPE STRIP DRAIN COLLECTOR AS-BUILT STRIP DRAIN DOWNSLOPE STRIP DRAIN COLLECTOR RISER STUB CONDENSATE SUMP PUMP STATION FOR TOE STRIP DRAIN



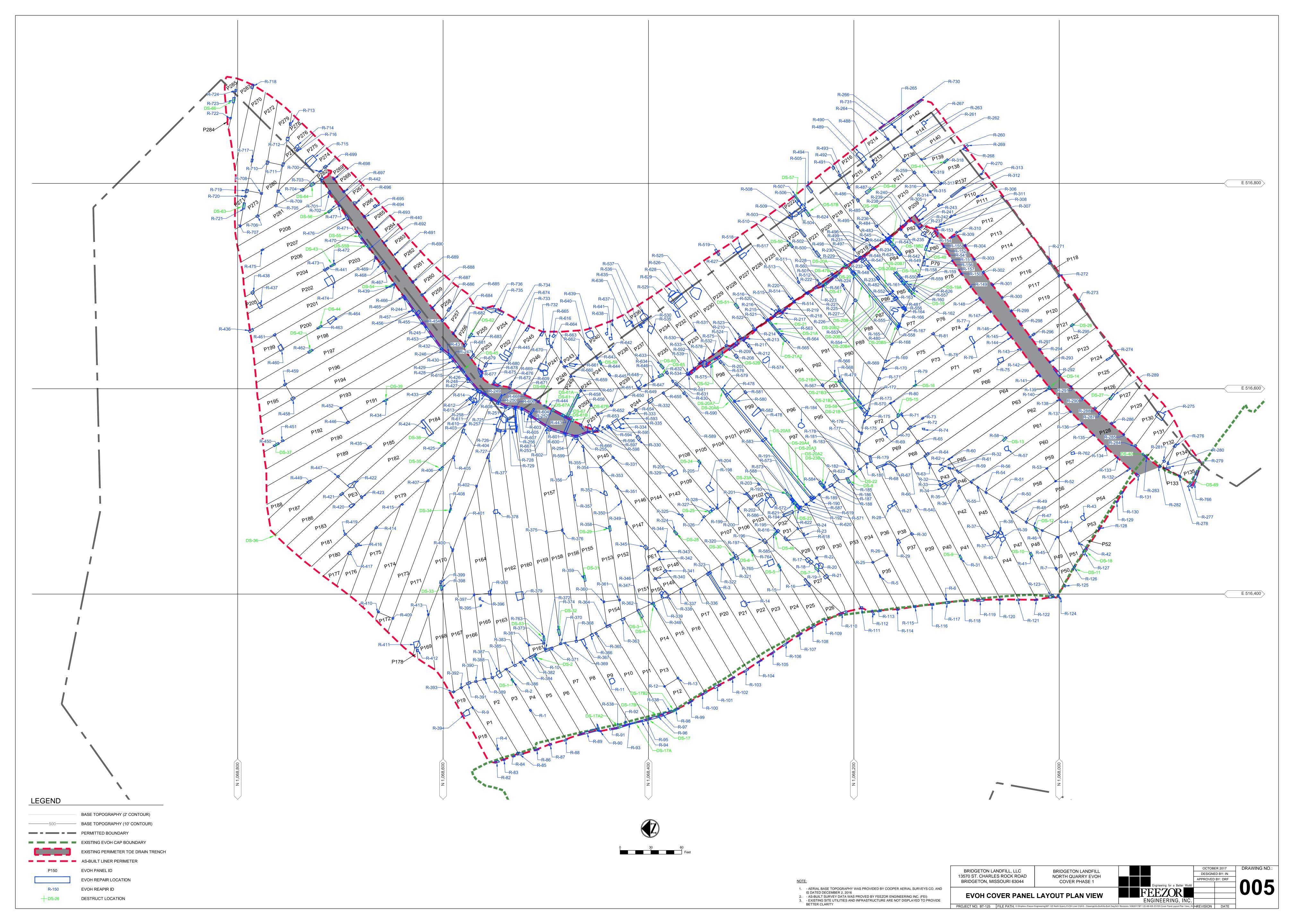
- 1. GAS AND LIQUID EXTRACTION POINTS THAT HAVE BEEN TEMPORARILY DECOMMISSIONED (PHYSICALLY DISCONNECTED FROM THE COLLECTION AND CONTROL SYSTEM DUE TO DECLINING GAS FLOWS), AND/OR ABANDONED, (PERMANENTLY AND PHYSICALLY REMOVED FROM THE COLLECTION AND CONTROL SYSTEM DUE TO INABILITY TO COLLECT GAS) HAVE BEEN REMOVED FROM THE SITE INFRASTRUCTURE UPDATE.
- 2. SEE DRAWING 002 FOR EXISTING UTILITIES LEGEND
- 3. AERIAL TOPOGRAPHY PROVIDED BY COOPER AERIAL SURVEYS, INC. AND IS DATED DECEMBER 2, 2016

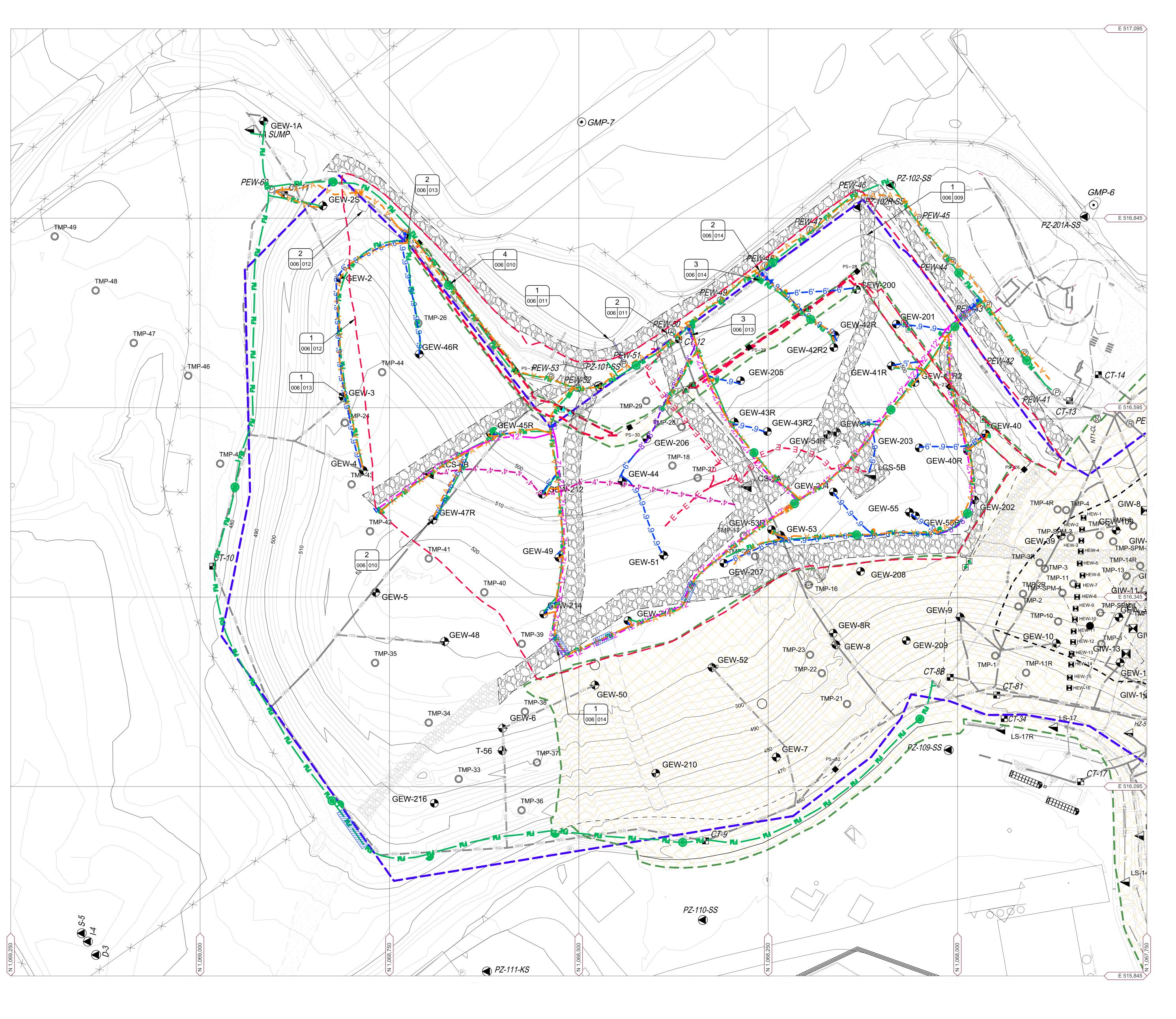
BRIDGETON LANDFILL, LLC
13570 ST. CHARLES ROCK ROAD
BRIDGETON, MISSOURI 63044

EVOH COVER UNDERCAP PLAN VIEW

BRIDGETON LANDFILL
NORTH QUARRY EVOH
COVER PHASE 1

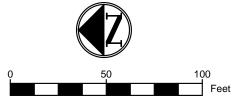
BRIDGETON LA





SOLID WASTE BOUNDARY **EXISTING GAS EXTRACTION WELL EXISTING PERIMETER GAS EXTRACTION WELL** PEW-20 **■** CT-1 EXISTING CONDENSATE SUMP EXISTING CONDENSATE TRAP/HEADER CONNECTION SUMP **■** *CT/HC-1* EXISTING LEACHATE COLLECTION SUMP LCS-2D EXISTING TEMPERATURE MONITORING PROBE AERIAL TOPOGRAPHY (2' CONTOUR) AERIAL TOPOGRAPHY (10' CONTOUR) AS-BUILT GRADING (2' CONTOUR) - AS-BUILT GRADING (10' CONTOUR) AS-BUILT HAUL ROAD EXISTING PERIMETER COLLECTION DRAIN EXISTING PERIMETER COLLECTION DRAIN SUMP EXISTING EVOH GEOMEMBRANE AS-BUILT EVOH GEOMEMBRANE LIMITS ── ► AS-BUILT DUAL-CONTAINED FORCEMAIN —4'—4'—4'—4'—4'— AS-BUILT LANDFILL GAS HEADER - 4 INCH -6'-6'-6'-6'-6'-6'-6'- AS-BUILT LANDFILL GAS HEADER - 6 INCH -8'-8'-8'-8'-8'-8'-8'-8'- AS-BUILT LANDFILL GAS HEADER - 8 INCH - 18' - 18' - 18' - 18' - 18' - AS-BUILT LANDFILL GAS HEADER - 18 INCH — A — A — A — A — A — AS-BUILT AIRLINE — E — E — E — E — E — AS-BUILT ELECTRICAL LINES AS-BUILT HEADER ACCESS RISER AS-BUILT BLIND FLANGE AS-BUILT ROAD CROSSING AS-BUILT ISOLATION VALVE AS-BUILT AIRLINE ISOLATION VALVE AS-BUILT FORCEMAIN ISOLATION VALVE VAULT AS-BUILT FORCEMAIN CLEANOUT RISER AS-BUILT END CAP AS-BUILT DUAL CONTAINED TEE & END CAP AS-BUILT 6 IN GAS STICKUP AS-BUILT 6 IN FORCEMAIN STICKUP AS-BUILT 8 IN CLEANOUT STICKUP AS-BUILT 6 IN CLEANOUT STICKUP

LEGEND



1. - GAS AND LIQUID EXTRACTION POINTS THAT HAVE BEEN TEMPORARILY DECOMMISSIONED (PHYSICALLY DISCONNECTED FROM THE COLLECTION AND CONTROL SYSTEM DUE TO DECLINING GAS FLOWS), AND/OR ABANDONED, (PERMANENTLY AND PHYSICALLY REMOVED FROM THE COLLECTION AND CONTROL SYSTEM DUE TO INABILITY TO COLLECT GAS) HAVE BEEN REMOVED FROM THE SITE INFRASTRUCTURE UPDATE.

- 2. SEE DRAWING 002 FOR EXISTING UTILITIES LEGEND
- SOME OF THE INFRASTRUCTURE ARE TURNED OFF FOR CLEARER REPRESENTATION
- AERIAL TOPOGRAPHY PROVIDED BY COOPER AERIAL SURVEYS, INC. AND IS DATED DECEMBER 2, 2016

BRIDGETON LANDFILL, LLC
13570 ST. CHARLES ROCK ROAD
BRIDGETON, MISSOURI 63044

BRIDGETON LANDFILL
NORTH QUARRY EVOH
COVER PHASE 1

BRIDGETON LANDFILL
NORTH QUARRY EVOH
FEEZOR
ENGINEERING, INC.

PROJECT NO: BT-125

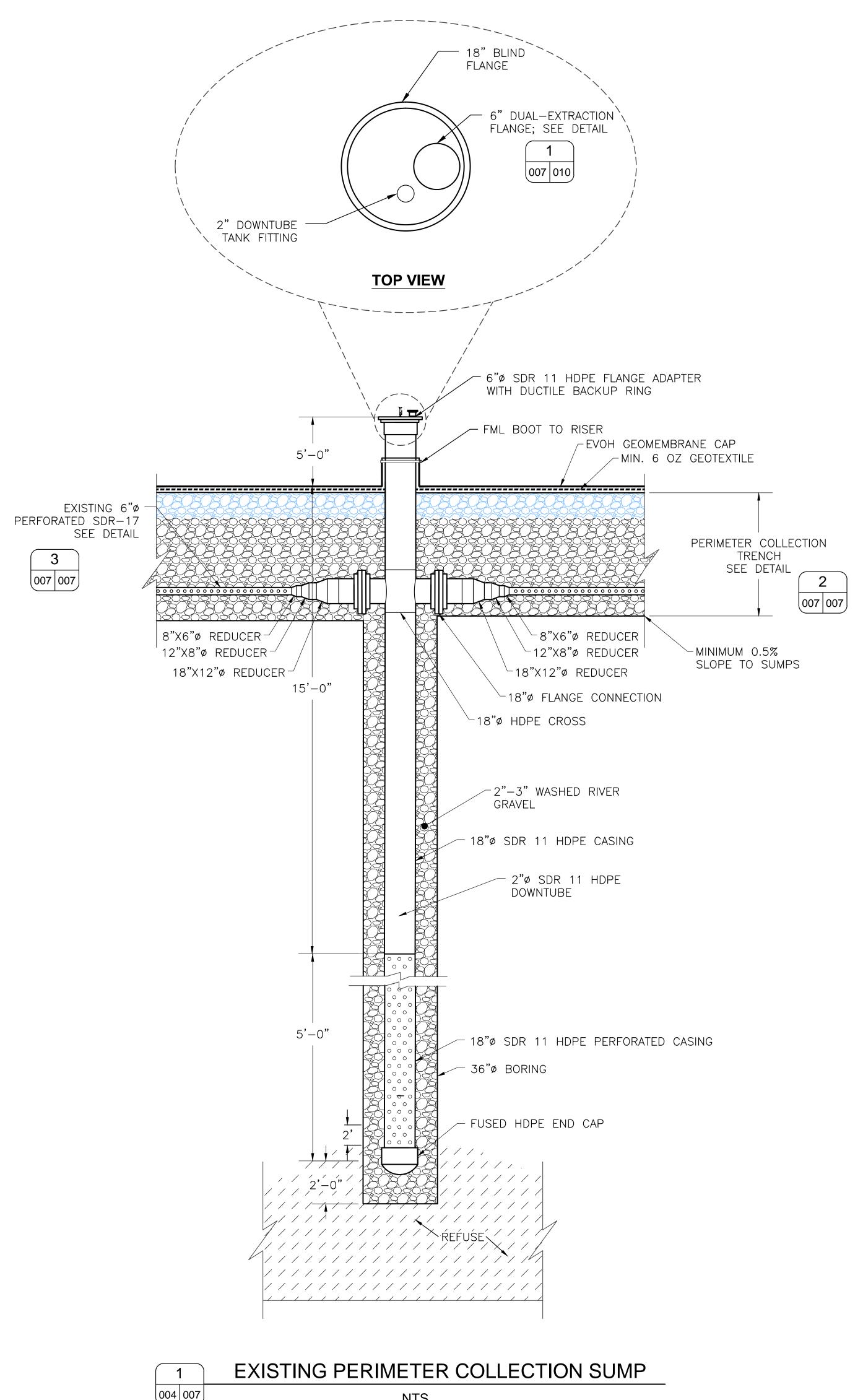
FILE PATH: D\Divopbox (Feezor Engineering)\BT-125 North Quarry EVOH Liner CQA\S- Drawings\As-Built\As-Built\Dwg BJV Revisions 10062017

DRAWING NO.:

DRAWING NO.:

DRAWING NO.:

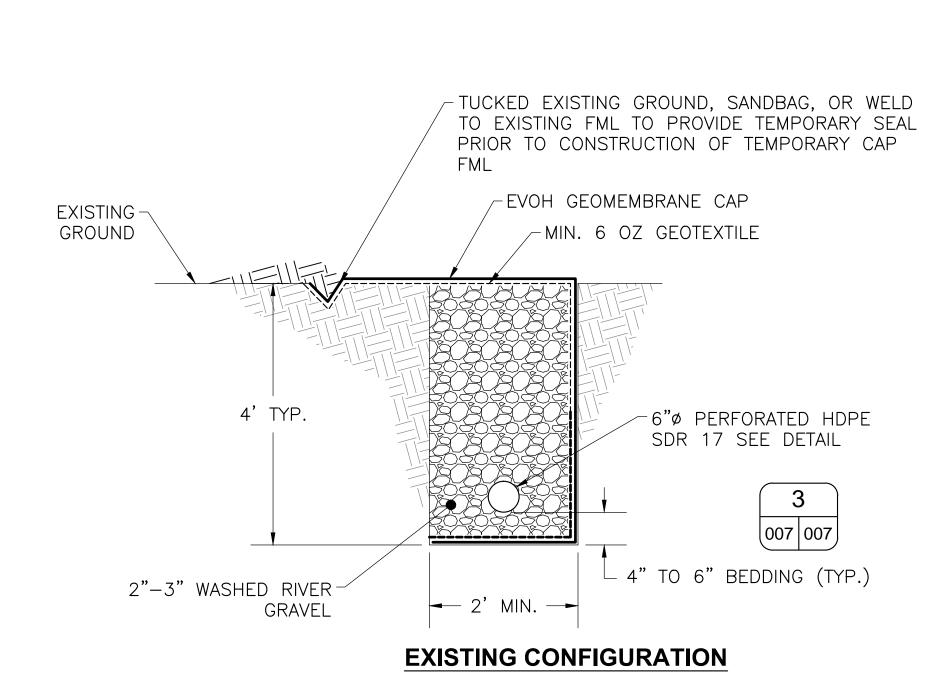
REVISION DATE

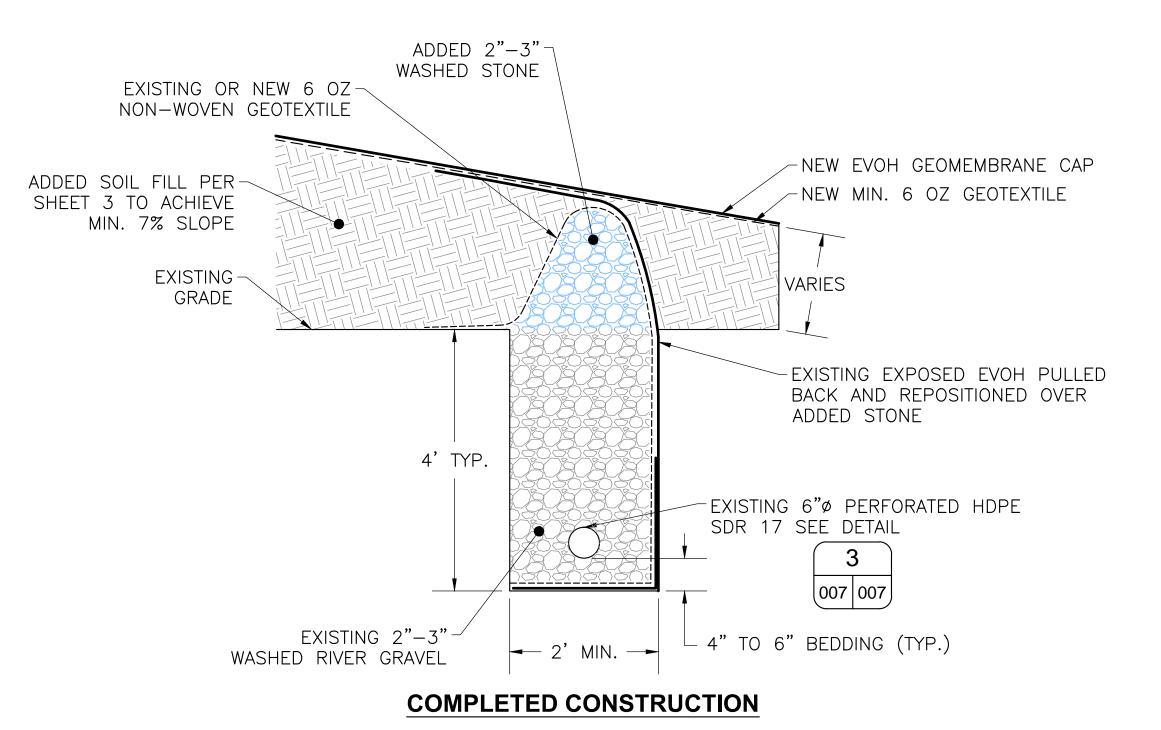


## NTS

NOTE:

1. INSTALLED PRIOR TO INITIATION OF NORTH QUARRY PHASE 1 EVOH COVER SYSTEM PROJECT.

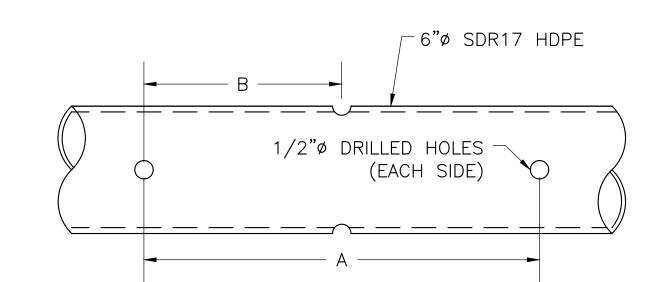




## PERIMETER COLLECTION TRENCH 004 007 NTS

NOTE:

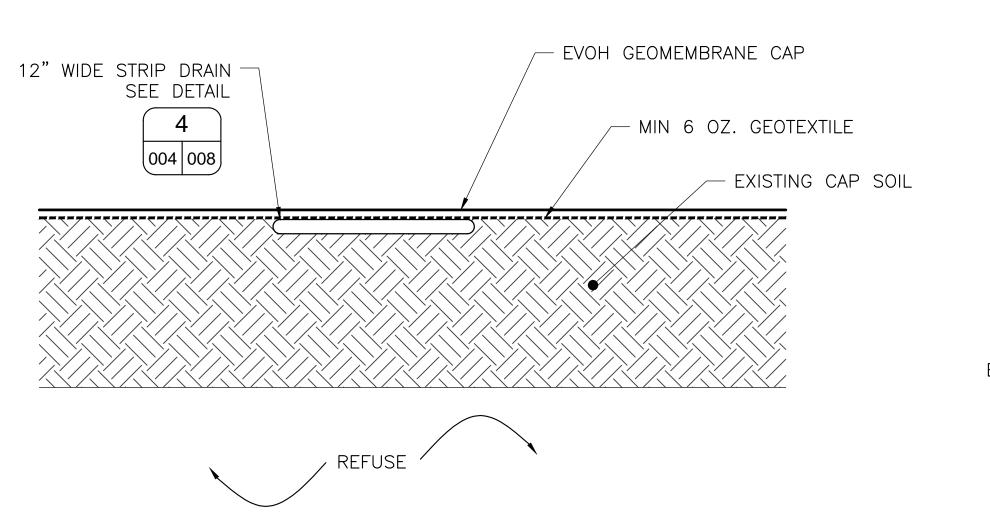
1. INSTALLED PRIOR TO INITIATION OF NORTH QUARRY PHASE 1 EVOH COVER SYSTEM PROJECT.

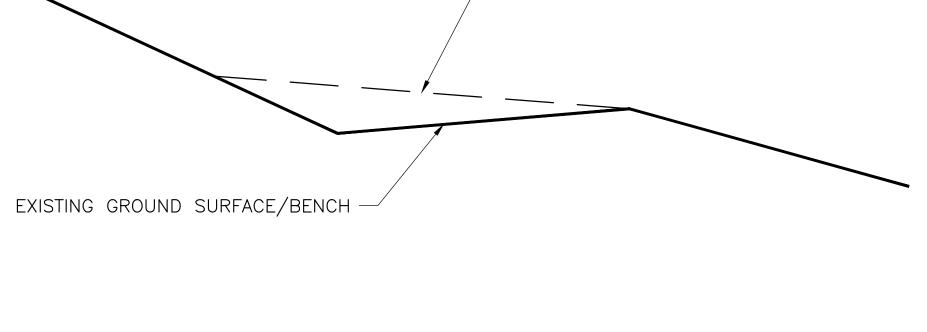


## EXISTING PERIMETER COLLECTION PIPE 007 007 NTS

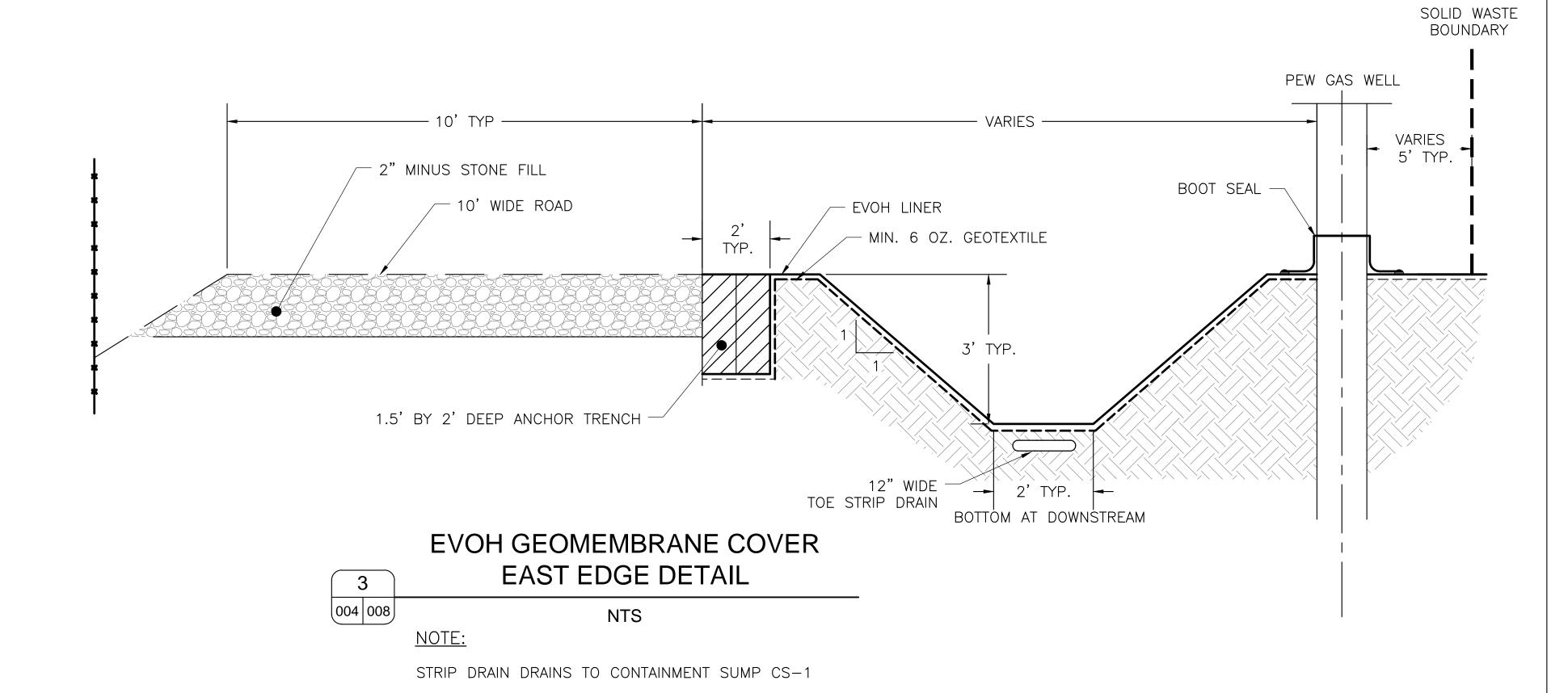
NOTE:

- 1. A=20"
- B=10" 90° ROTATION BETWEEN ROWS
- 2. INSTALLED PRIOR TO INITIATION OF NORTH QUARRY PHASE 1 EVOH COVER SYSTEM PROJECT.



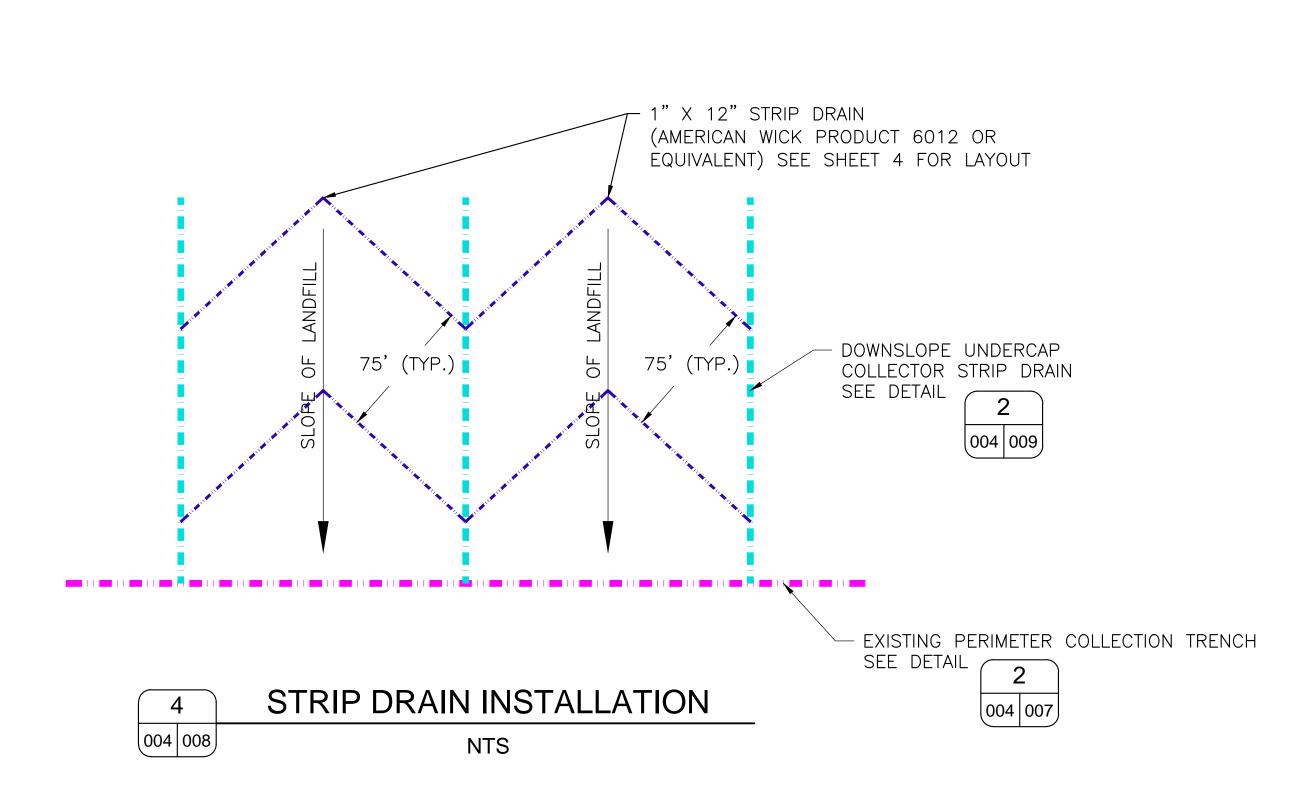


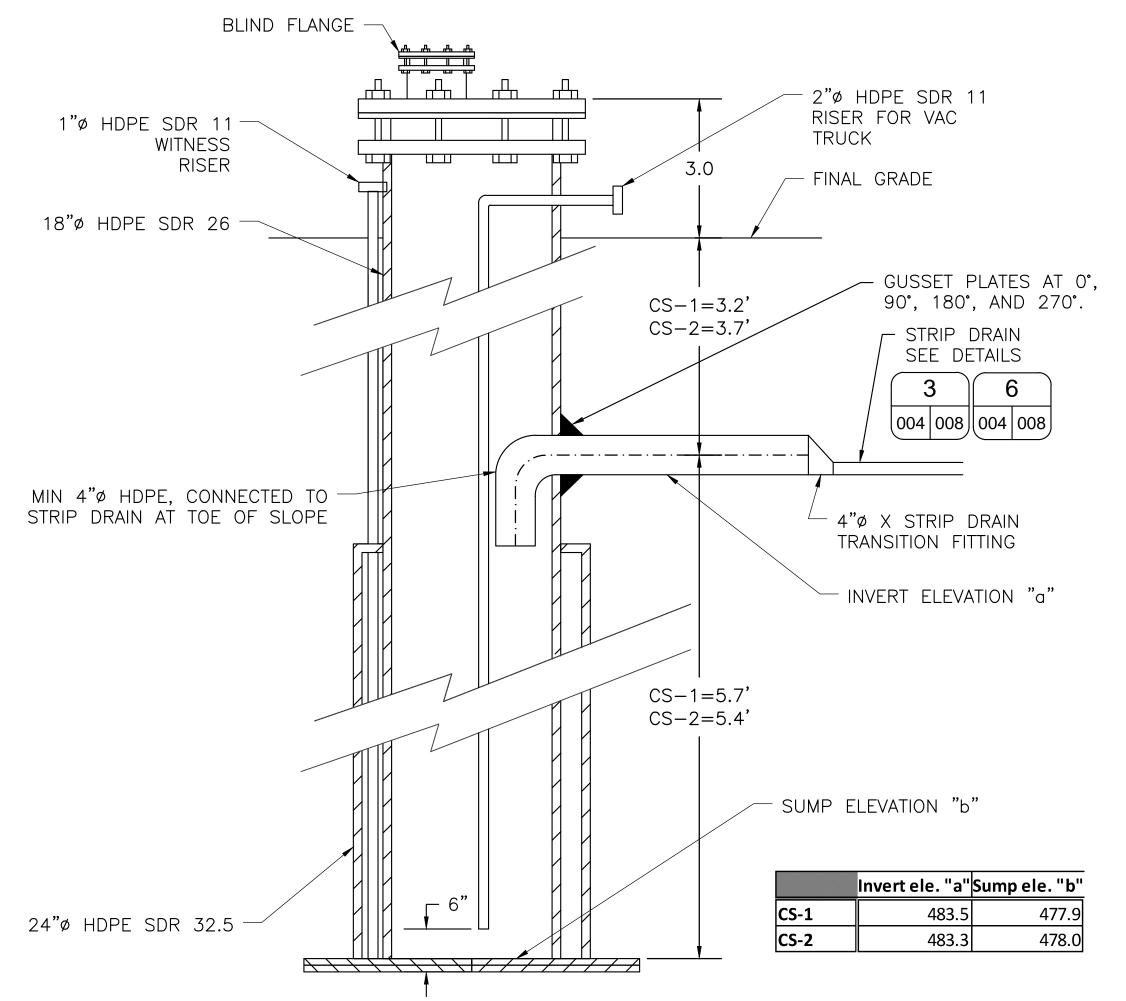
RE-GRADED EXISTING BENCH WITH POSITIVE SLOPE TO PROMOTE FLOW FOR STORM WATER RUNOFF

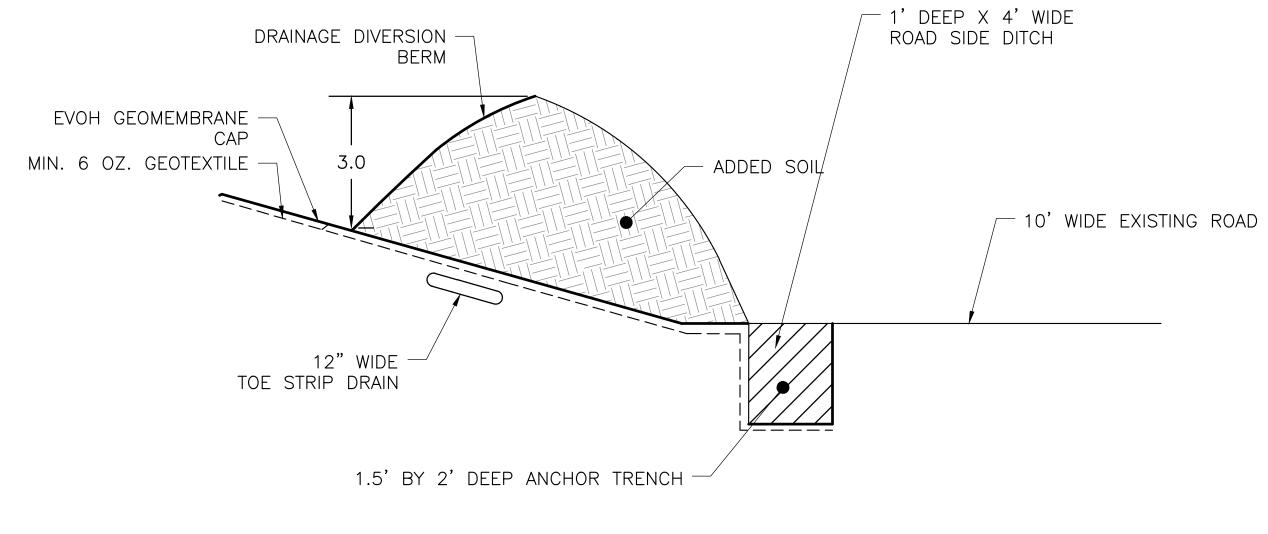


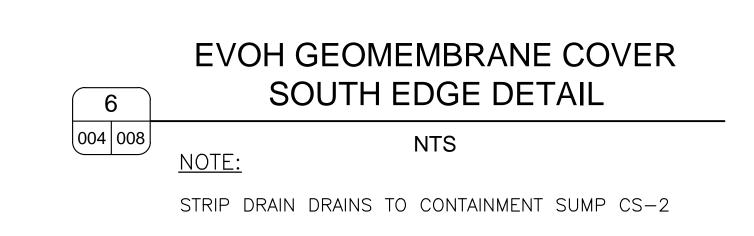








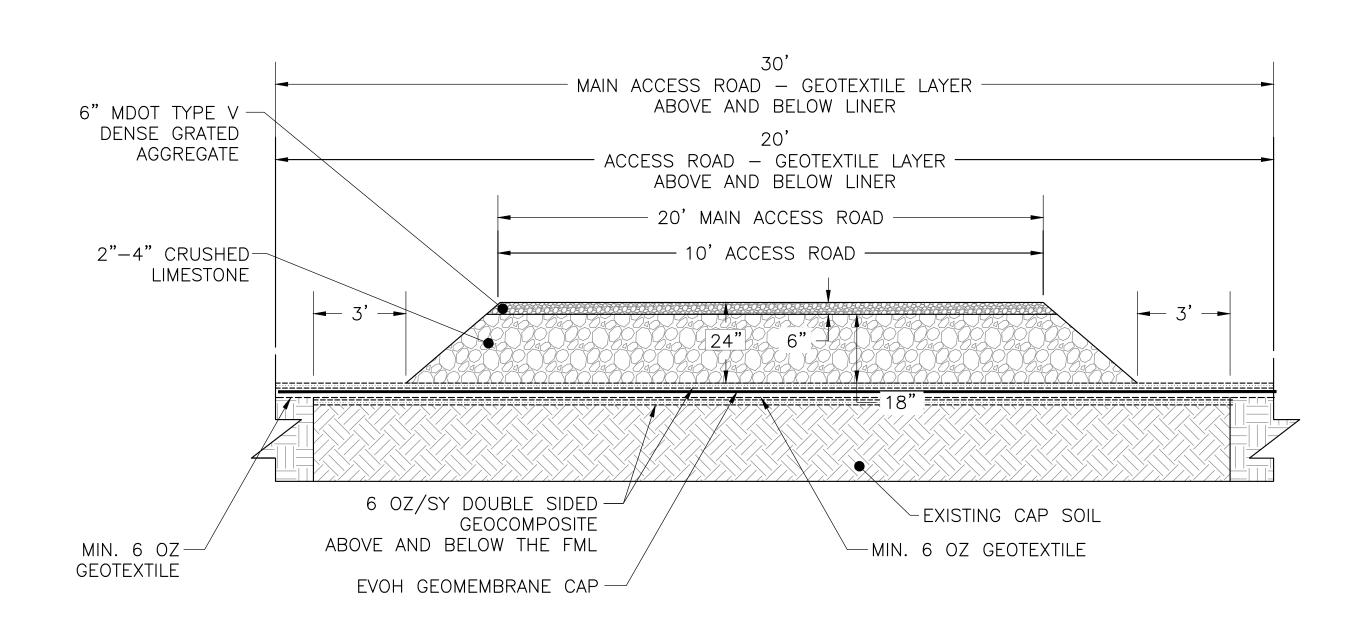


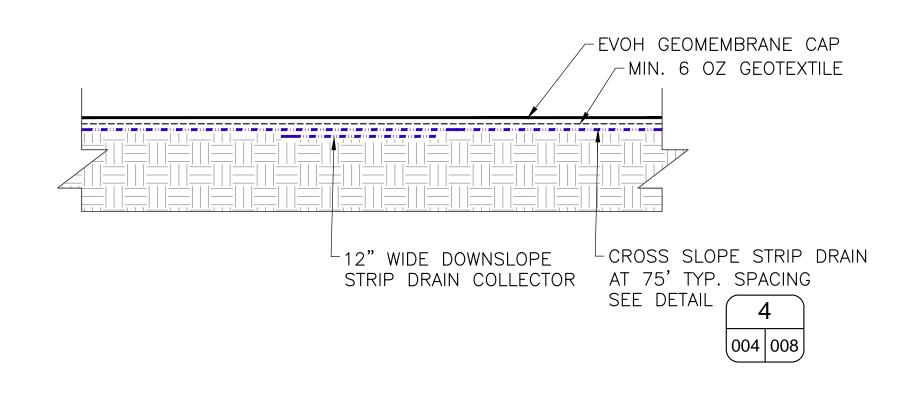


## CONTAINMENT SUMP PUMP STATION

5 FOR TOE STRIP DRAIN

004 008 NTS

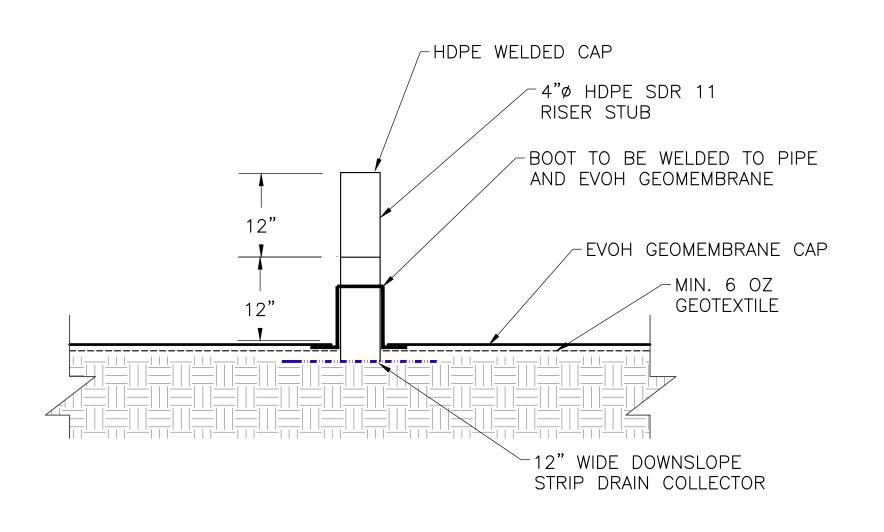






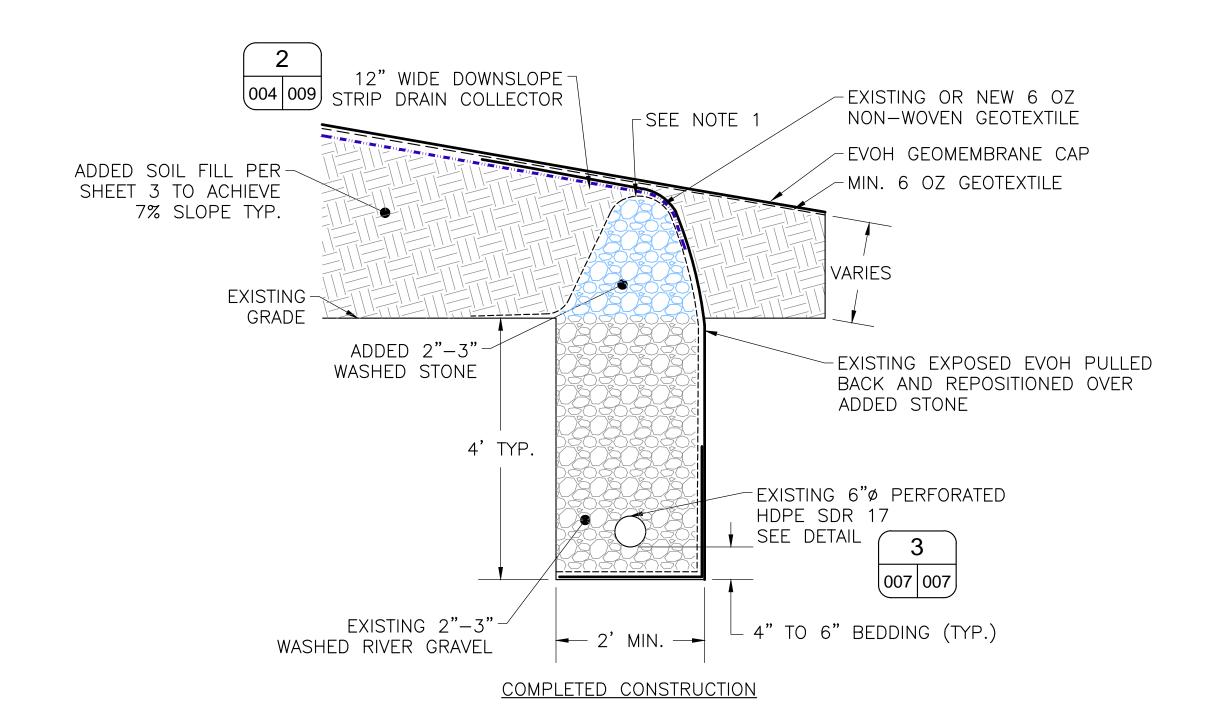
2 12" WIDE DOWNSLOPE STRIP DRAIN COLLECTOR

OO4 009 NTS

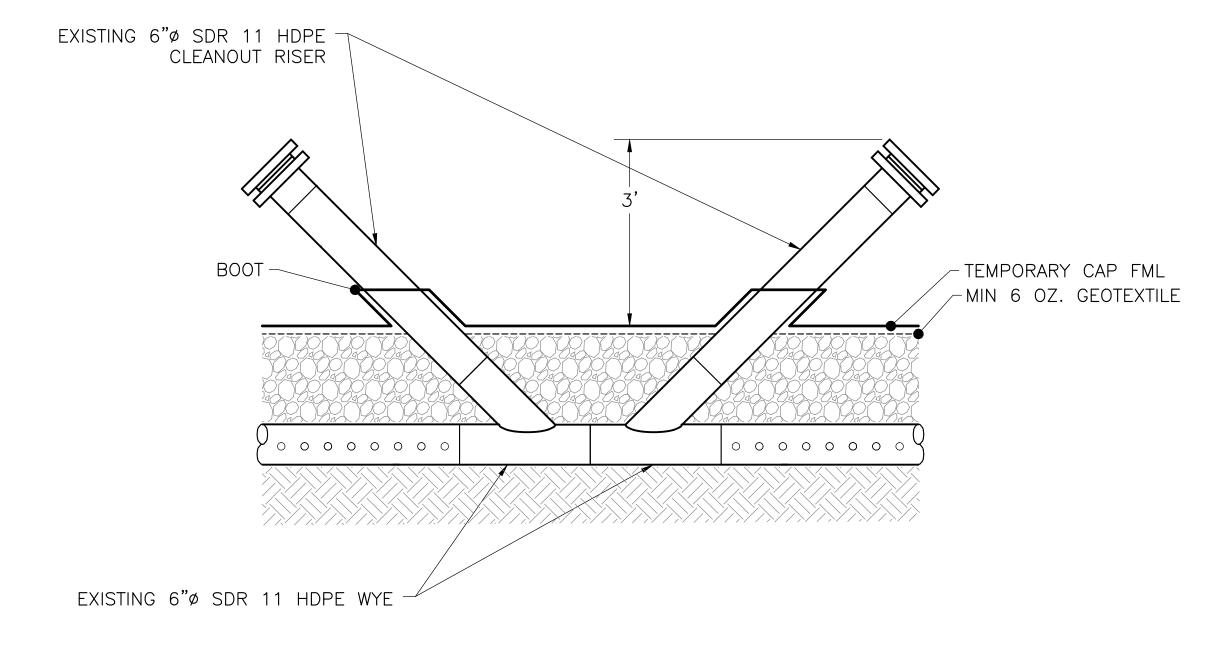


## 3 DOWNSLOPE STRIP DRAIN COLLECTOR RISER STUB NTS NOTES:

1. SEE SHEET 4 FOR RISER STUB LOCATIONS.







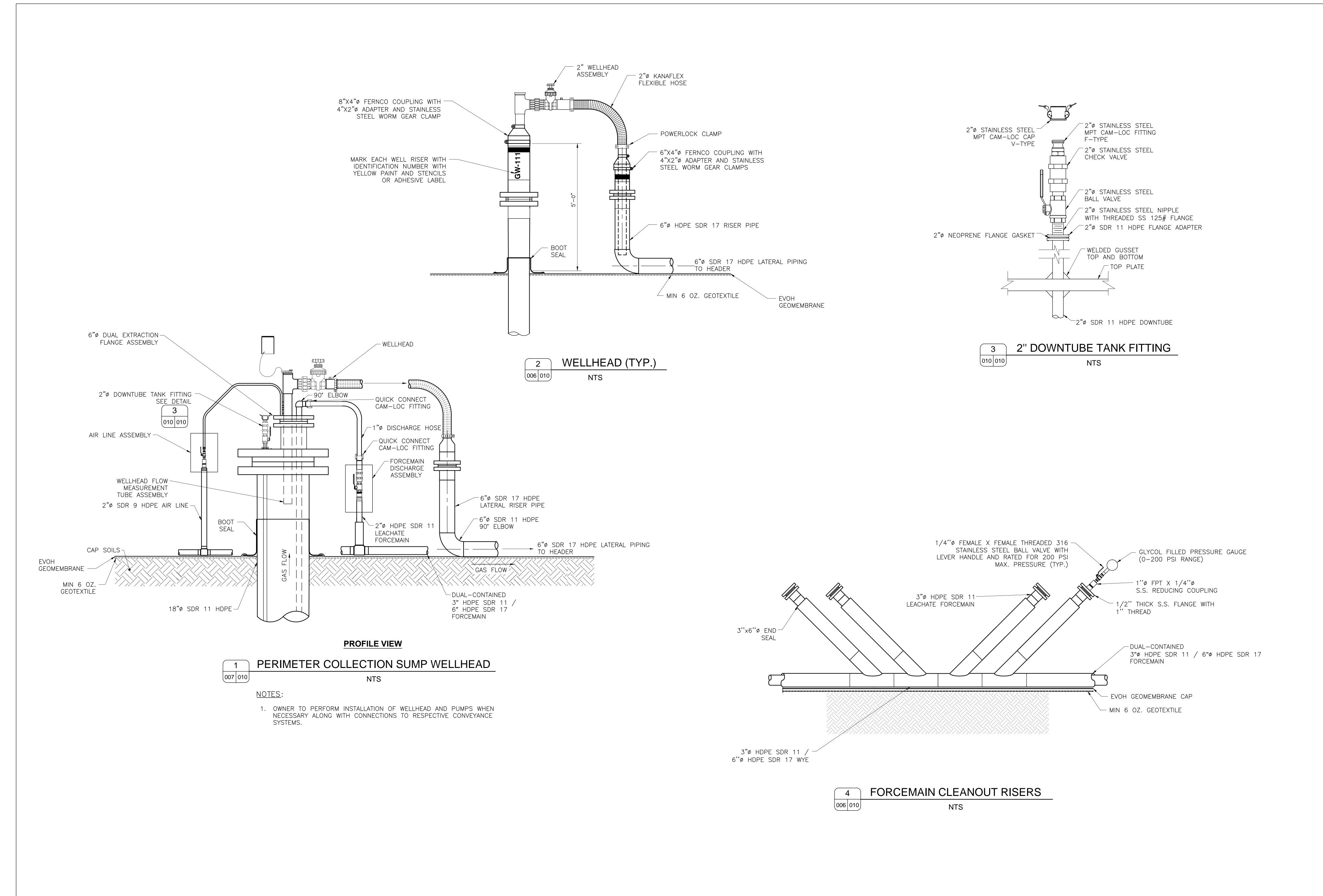
# PERIMETER COLLECTOR TRENCH CLEANOUT RISERS NTS NOTE: 1. INSTALLED PRIOR TO INITIATION OF NORTH QUARRY PHASE 1 EVOH COVER SYSTEM PROJECT.

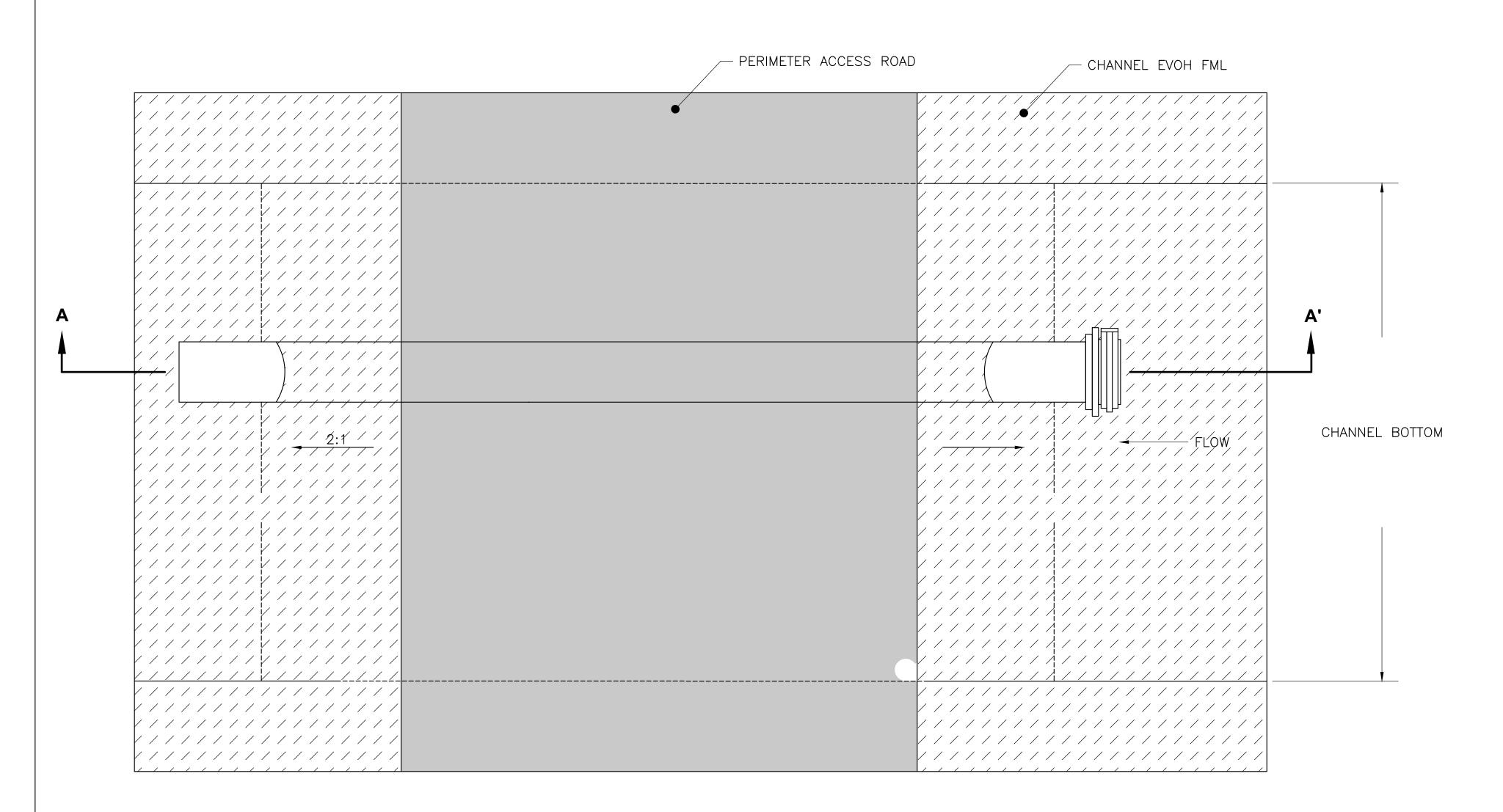
<u>)TE</u>:

1. CUT GEOTEXTILE AND TIED—IN DOWNSLOPE COLLECTOR STRIP DRAIN INTO ADDED STONE.

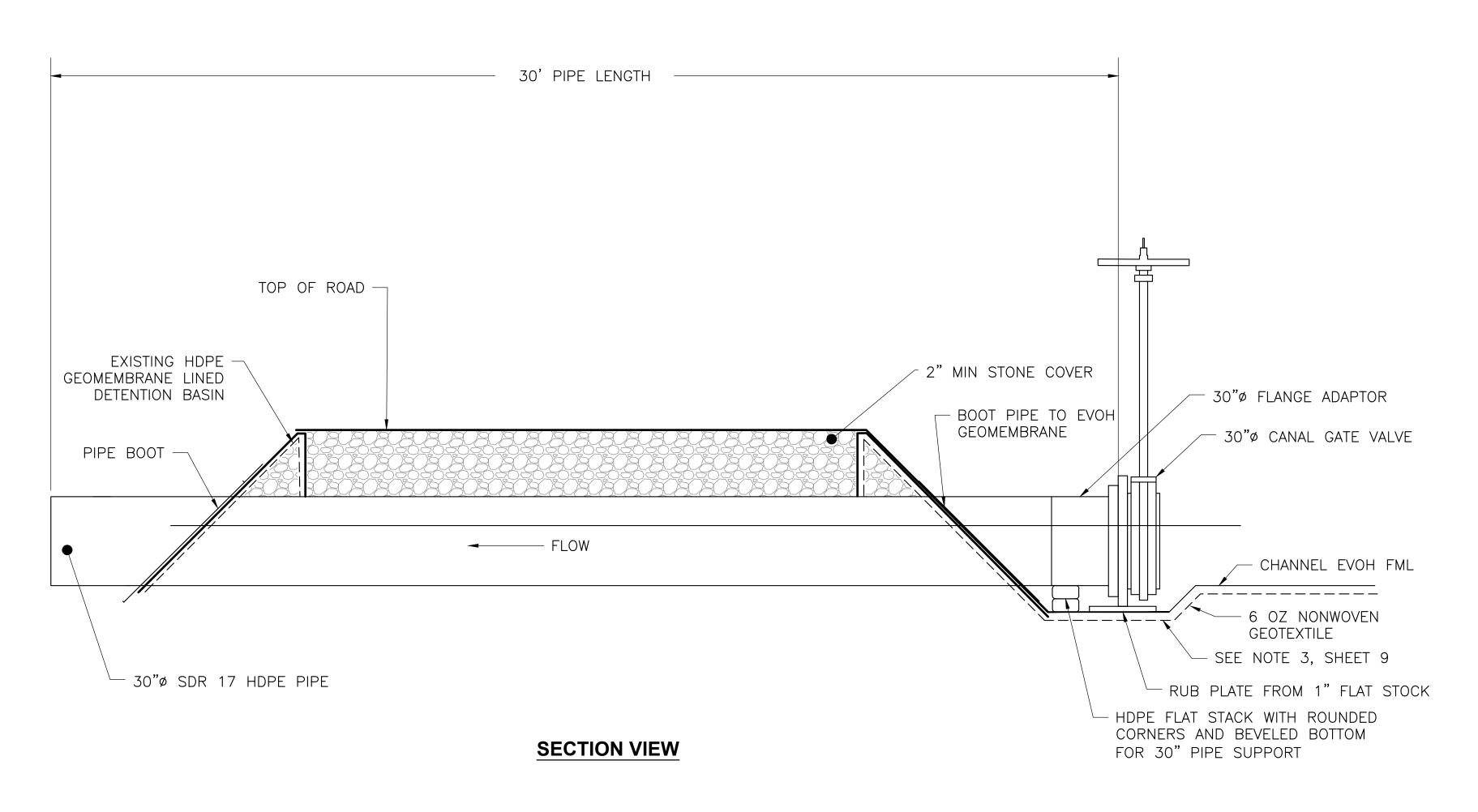
DOWNSLOPE STRIP DRAIN COLLECTOR TERMINATION

PROJECT NO: BT-125 FILE PATH: D:\Dropbox (Feezor Engineering)\BT-125 North Quarry EVOH Liner CQA\5 - Drawings\As-Built\As-Built\Dwg BJV Revisions 10062017\BT-125-AB-007-014 (Details).dwg

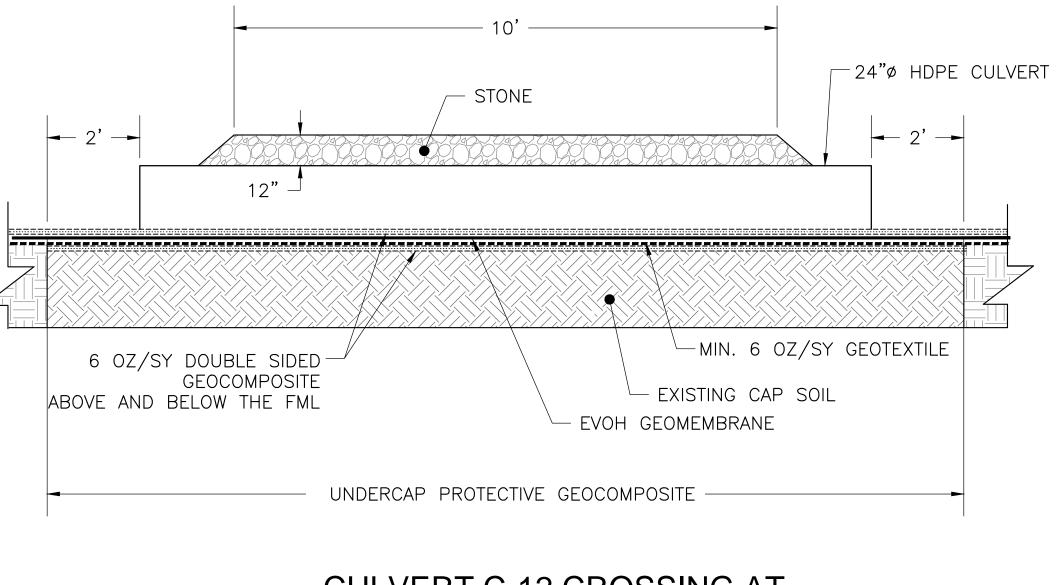




## **PLAN VIEW**

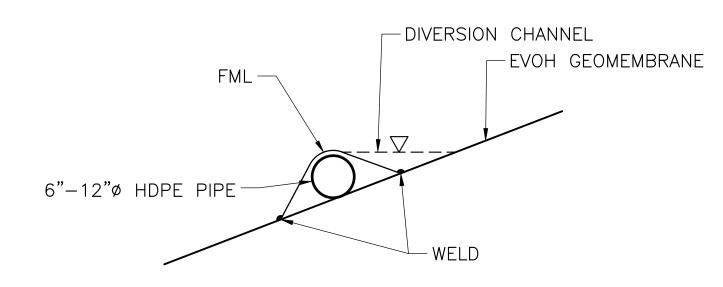




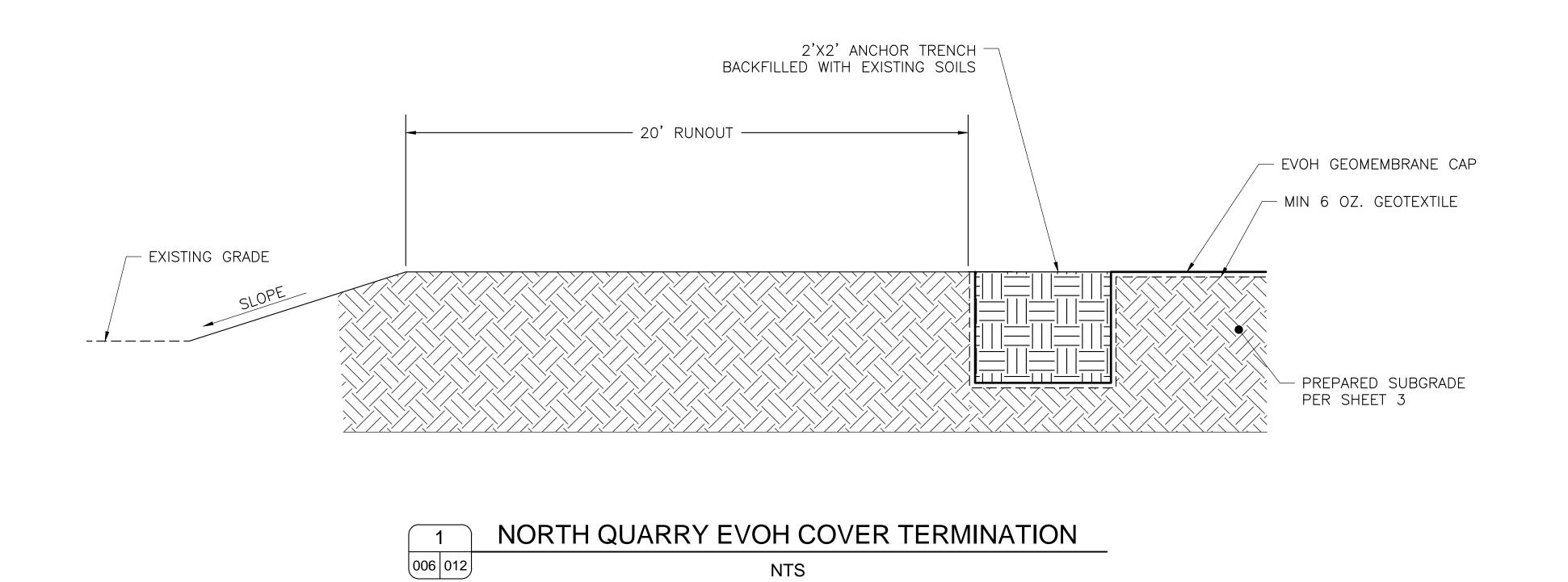


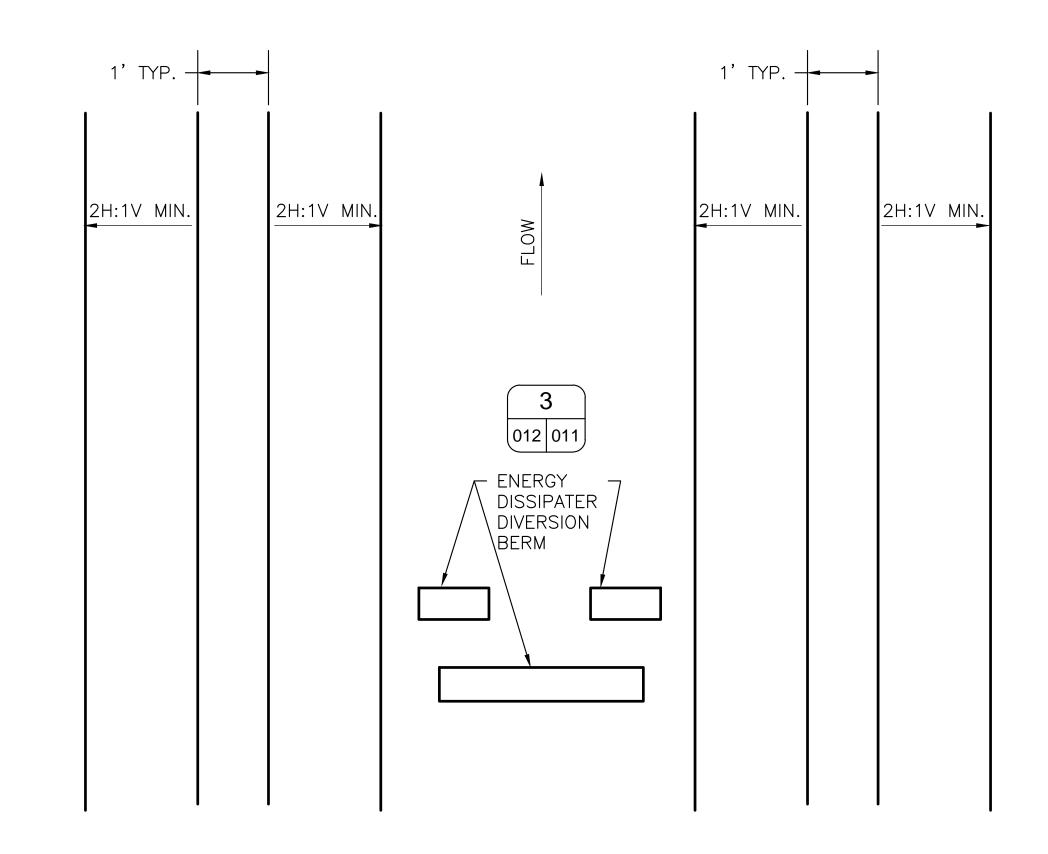
CULVERT C-12 CROSSING AT LIGHT-DUTY ACCESS ROAD

NTS

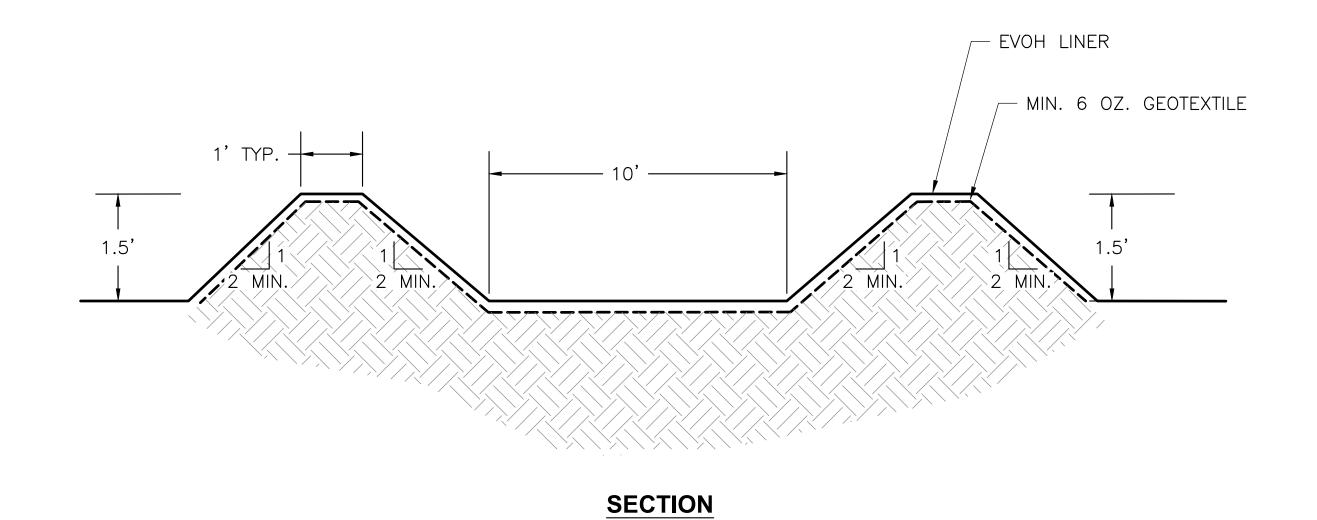




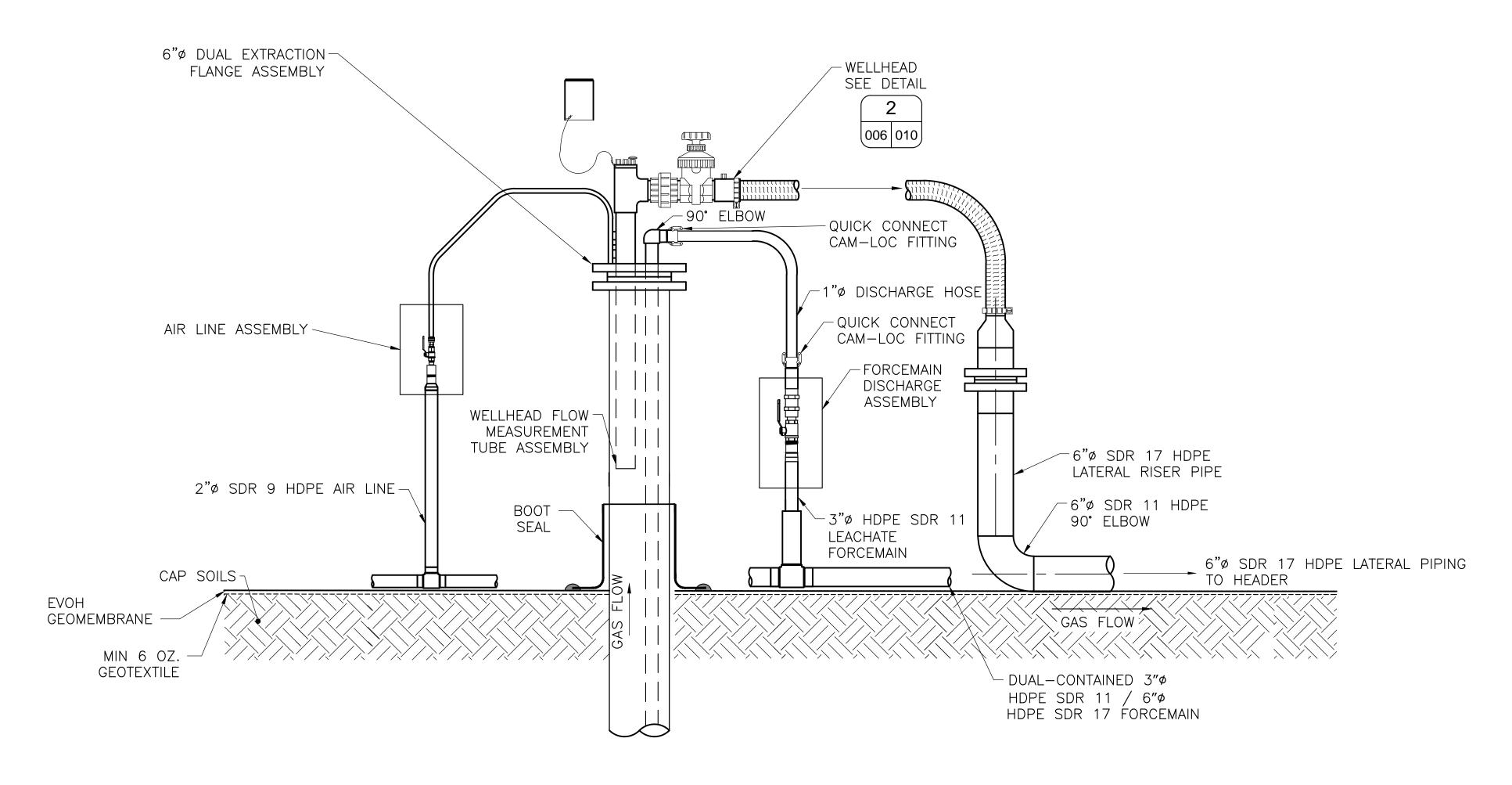




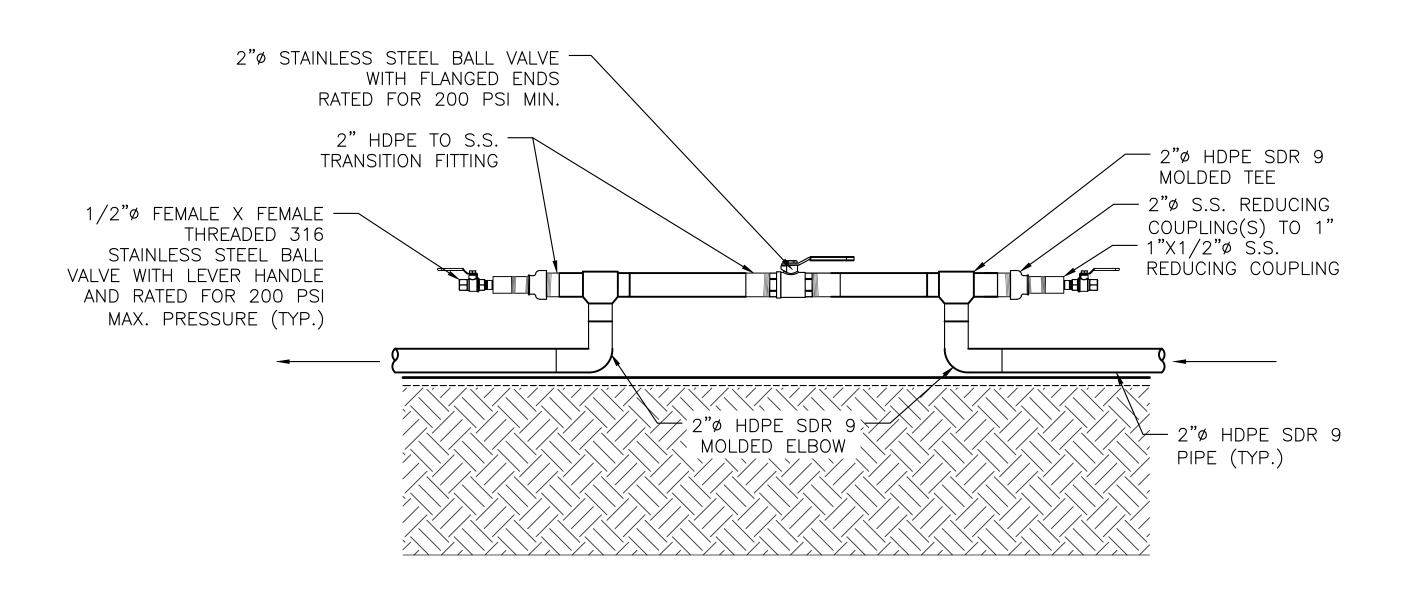
**PLAN** 



2 LINED DOWNCHUTE
006 012 NTS



1 DUAL EXTRACTION WELLHEAD (TYP)
006 013 NTS



006 013

AIRLINE ISOLATION AND BLOWOFF VALVE

NTS

